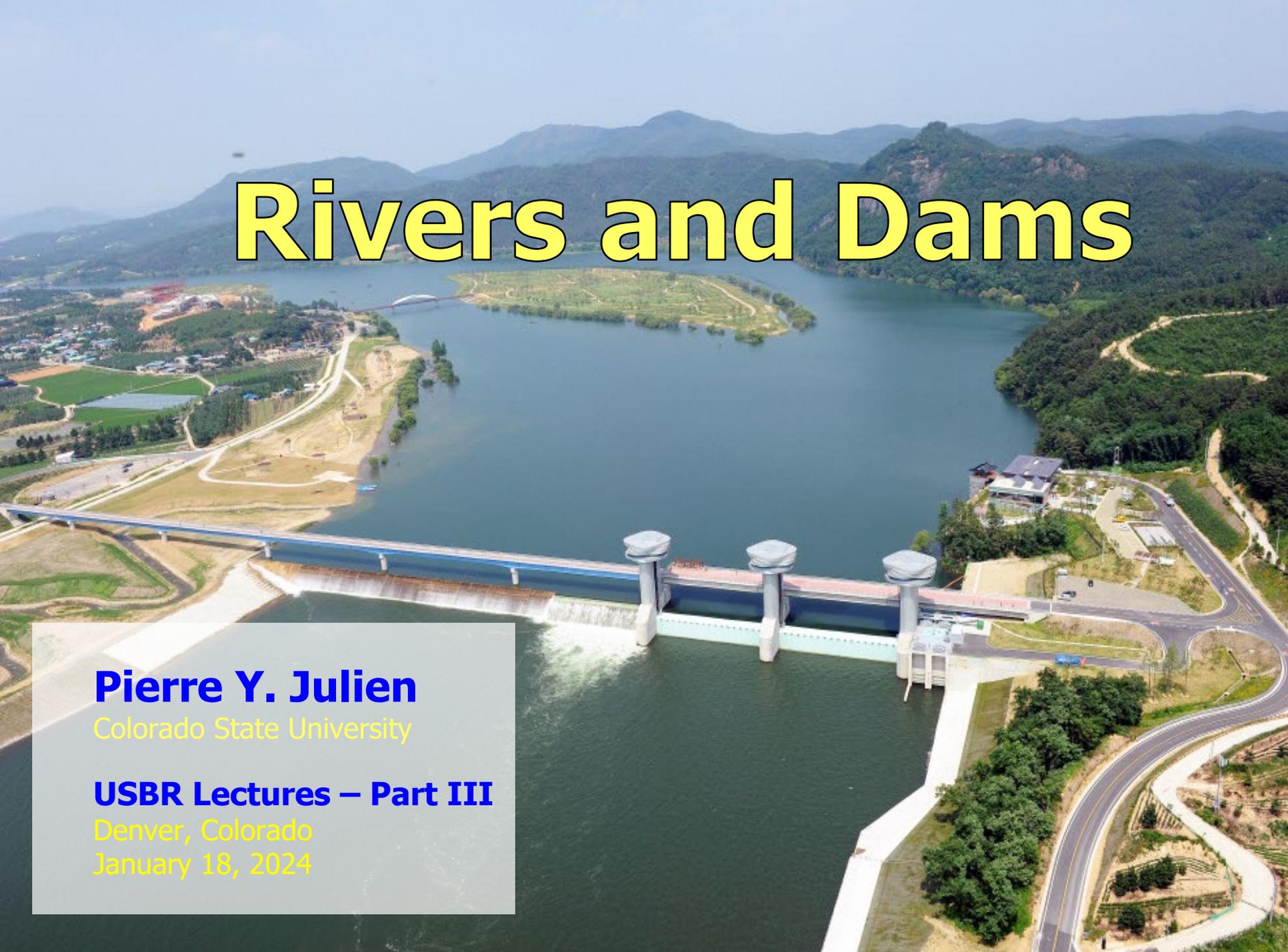


Rivers and Dams

An aerial photograph of a large dam and reservoir. The dam is a long concrete structure with several spillways and a central gate structure. The reservoir is a large body of water that fills a valley, with a small island in the middle. The surrounding landscape is mountainous and forested. In the foreground, there are roads, buildings, and some agricultural fields.

Pierre Y. Julien

Colorado State University

USBR Lectures – Part III

Denver, Colorado

January 18, 2024

USBR Short Course

1. Watersheds and Climate
2. Sedimentation Engineering
3. **Rivers and Dams**
4. River Environment



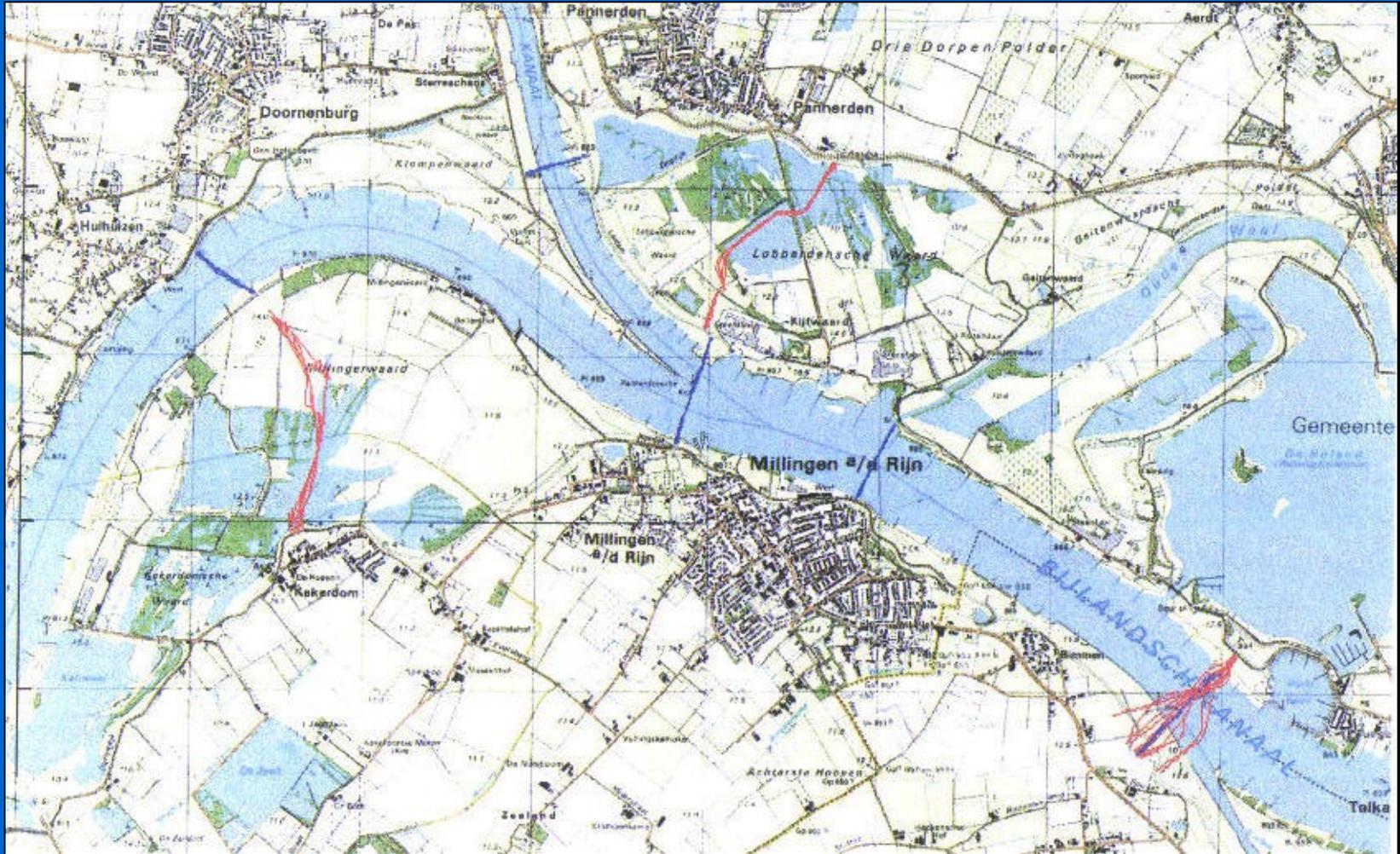
Rivers and Dams

- 1. River Equilibrium**
- 2. Aggradation**
- 3. Degradation below Dams**
- 4. Case Study Gupo Bridge**
- 5. Case Study Dam Break**

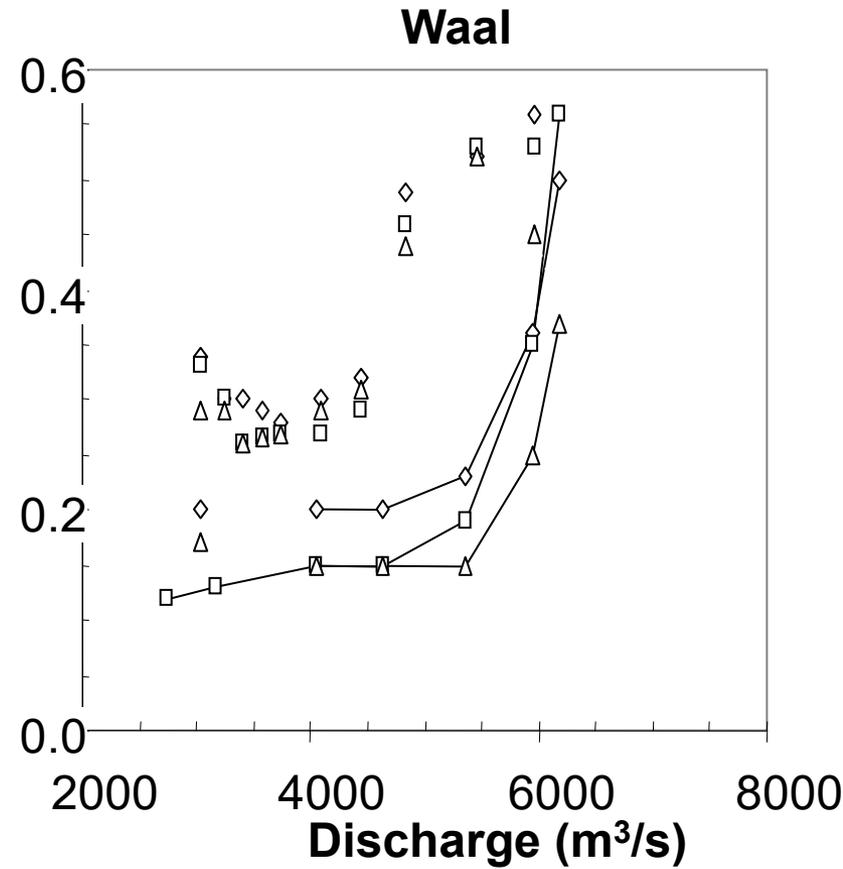
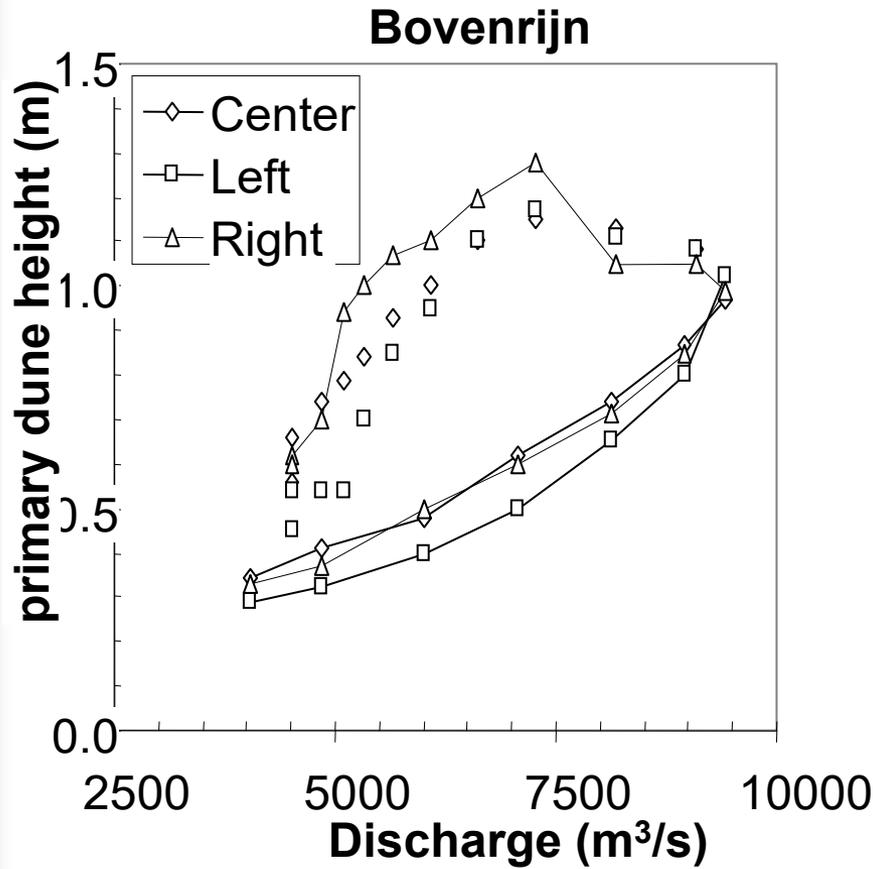


1a. Manning n

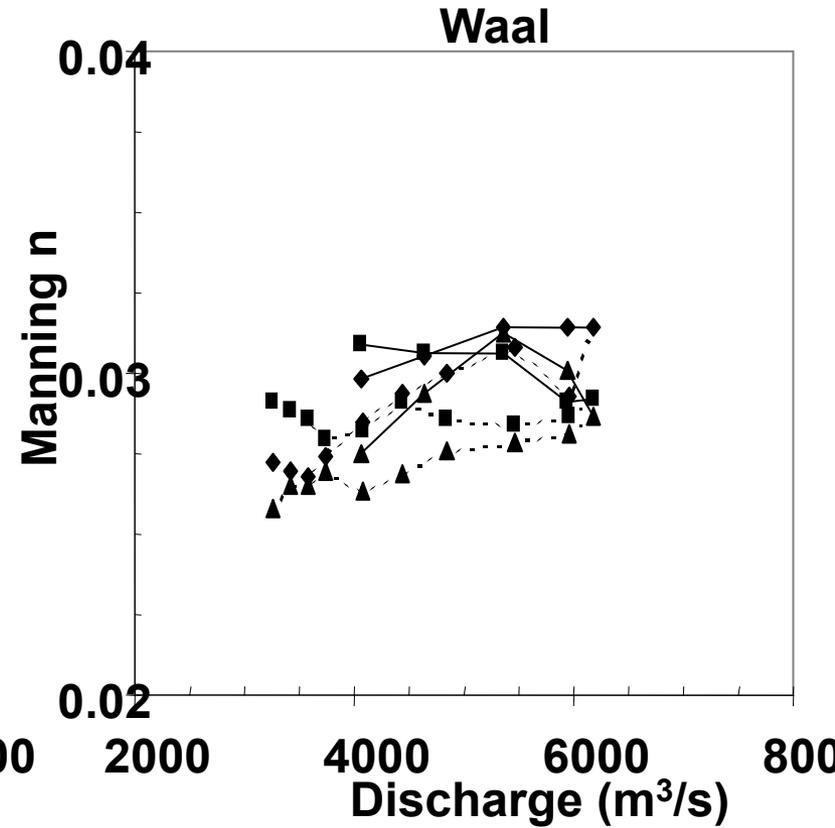
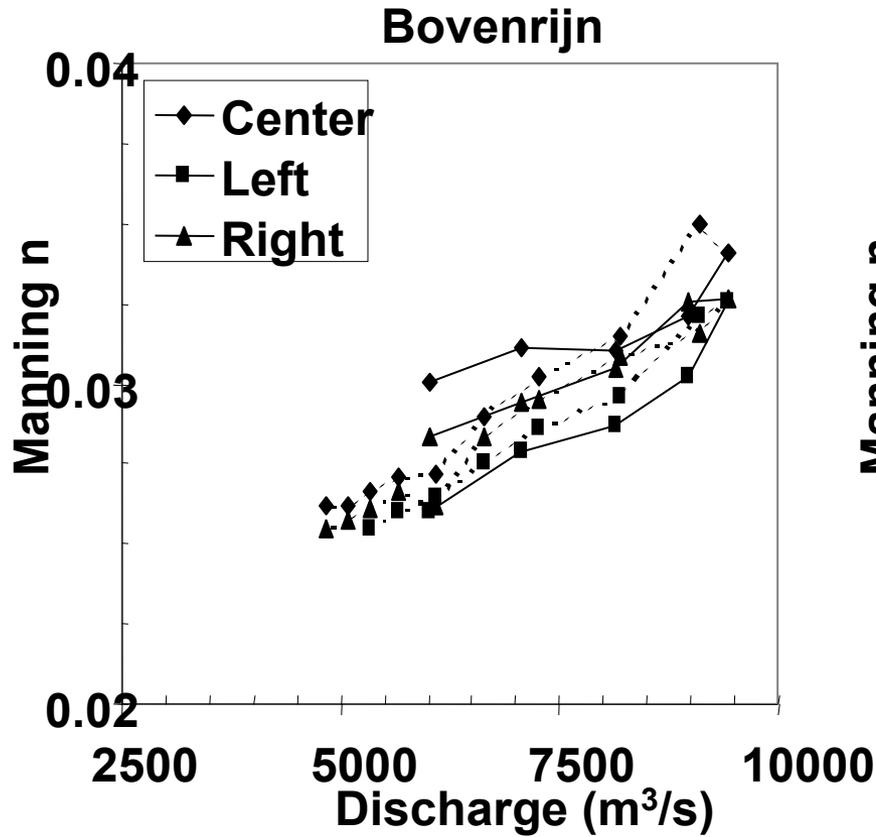
Rhine River flood in 1998



Primary dune height vs discharge

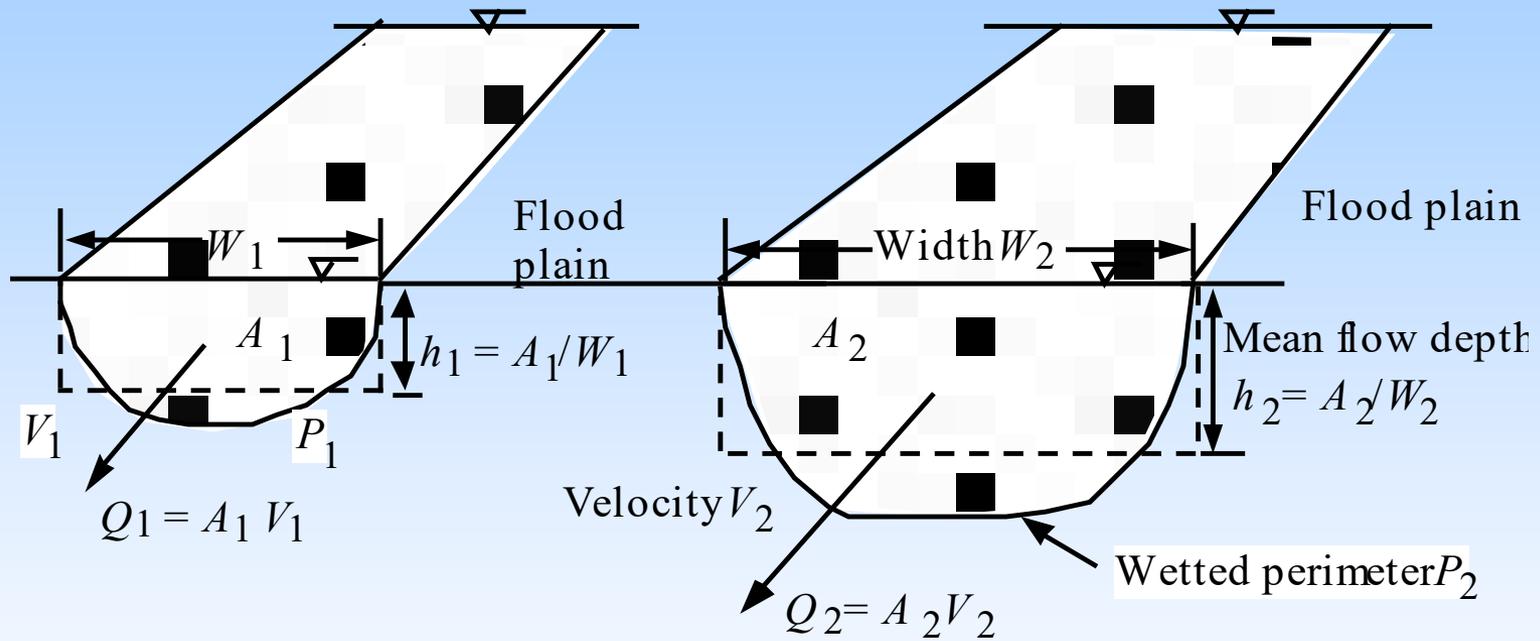


Manning n vs discharge



1b. Downstream Hydraulic Geometry

Downstream Hydraulic Geometry



Julien-Wargadalam (J-W) Equations

When the Manning-Strickler approximation is applicable, i.e. $m = 1/6$, a simplified form of Eqs. (10.19) is obtained in SI as

$$h \approx 0.133 Q^{0.4} \tau_*^{-0.2} \quad (10.20a) \blacklozenge$$

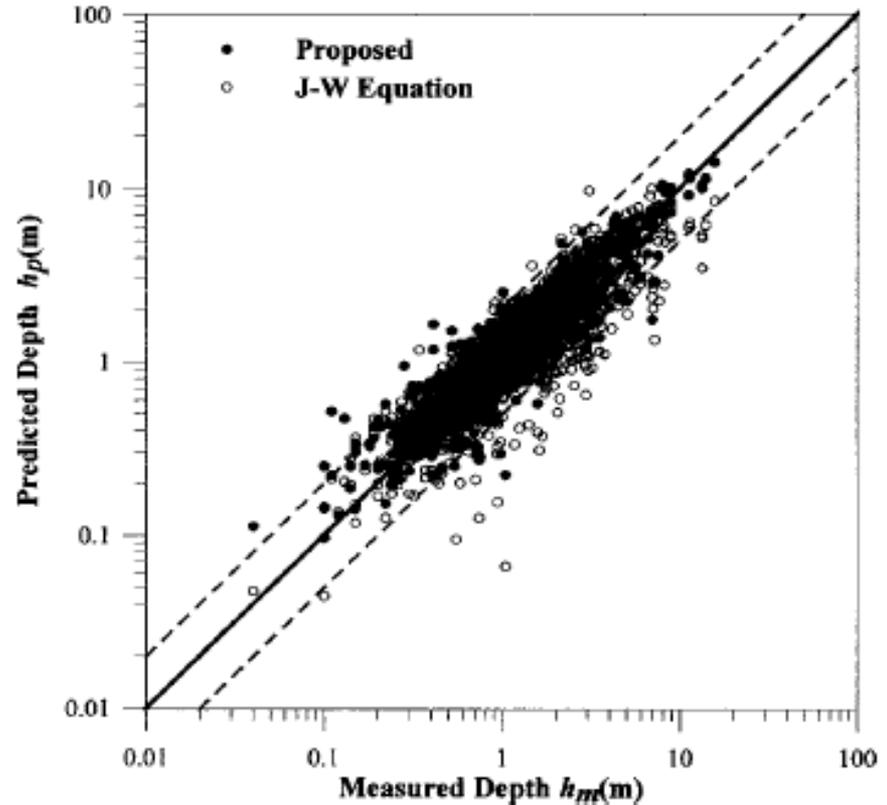
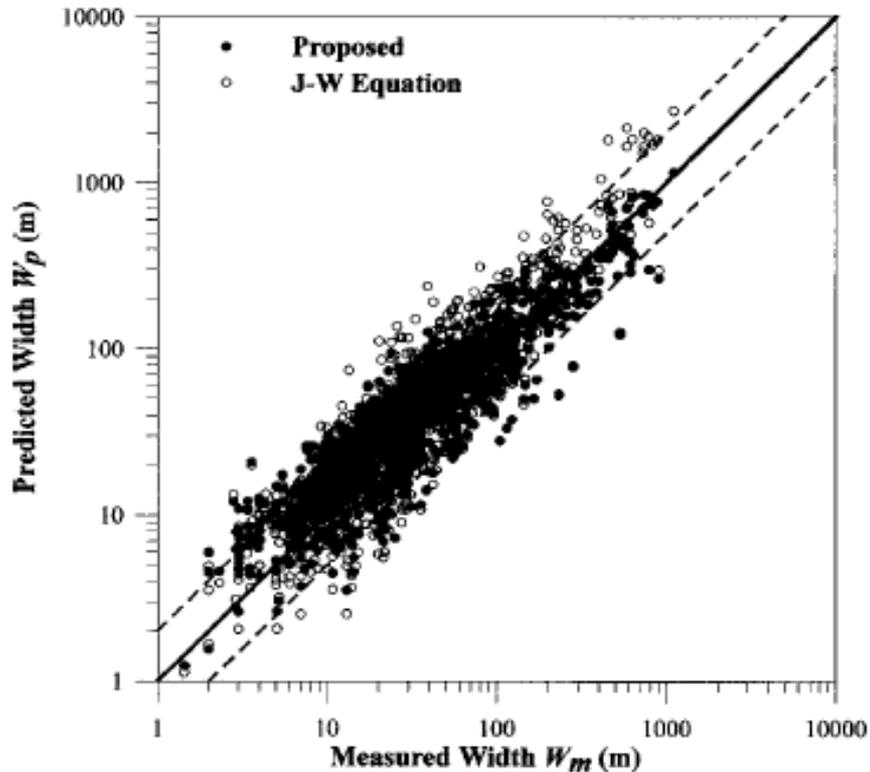
$$W \approx 0.512 Q^{0.53} d_s^{-0.33} \tau_*^{-0.27} \quad (10.20b) \blacklozenge$$

$$V \approx 14.7 Q^{0.07} d_s^{0.33} \tau_*^{0.47} \quad (10.20c) \blacklozenge$$

$$S \approx 12.4 Q^{-0.4} d_s \tau_*^{1.2} \quad (10.20d) \blacklozenge$$

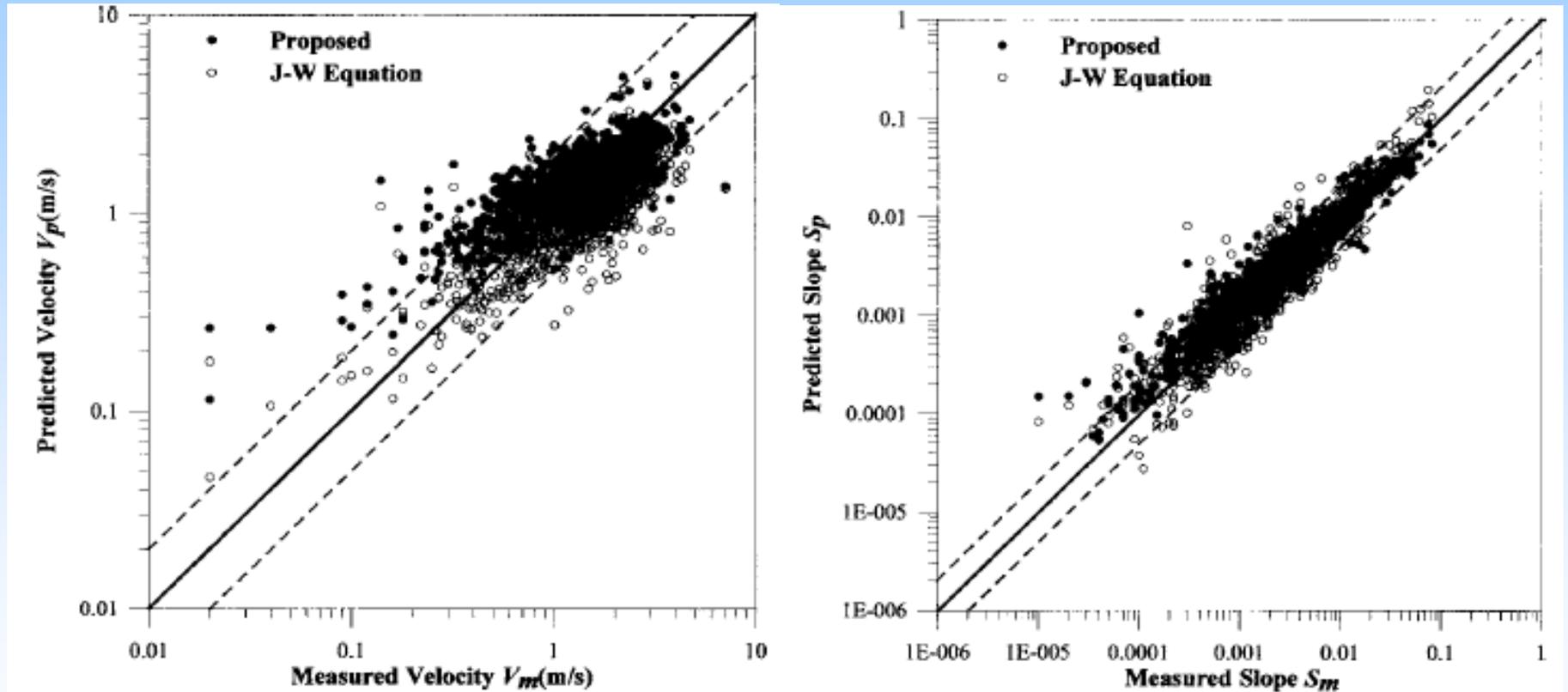
The hydraulic geometry of stable channels is obtained from Eqs. (10.20) when $\tau_* \cong 0.047$. Higher sediment transport rates require higher velocity and slope, and reduced width and depth.

Bankfull width and depth



from Julien and Wargadalam (ASCE-JHE, 1996)

Bankfull velocity and slope



from Julien and Wargadalam (ASCE-JHE, 1996)

1c. Meandering

Sediment Transport in Sharp Bends

Laboratory experiments show that fine sand can deposit where coarse sand cannot, i.e. point bars

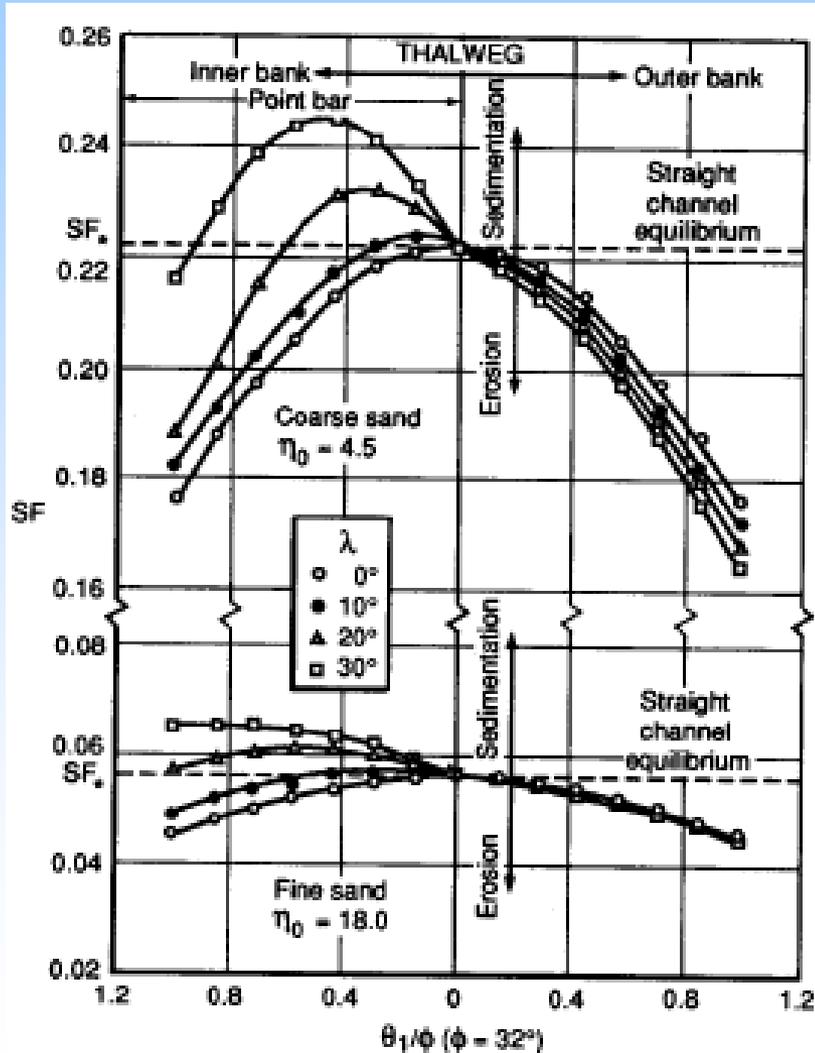
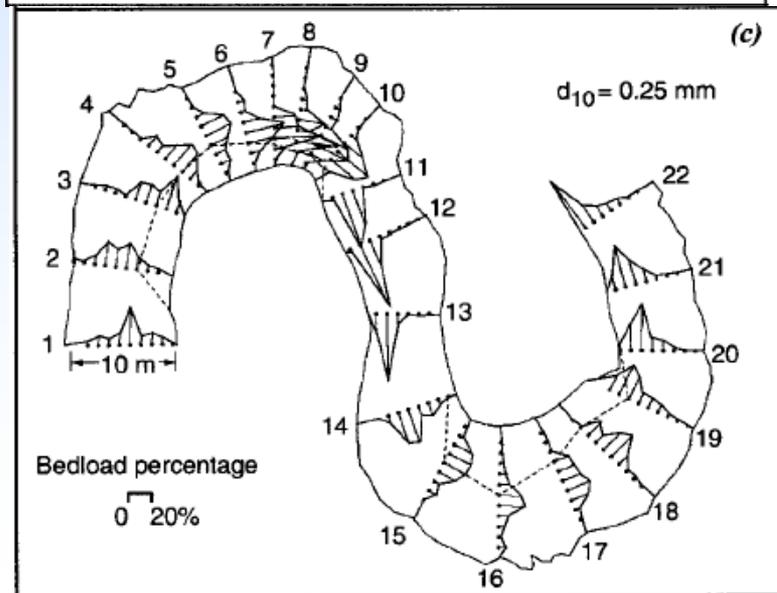
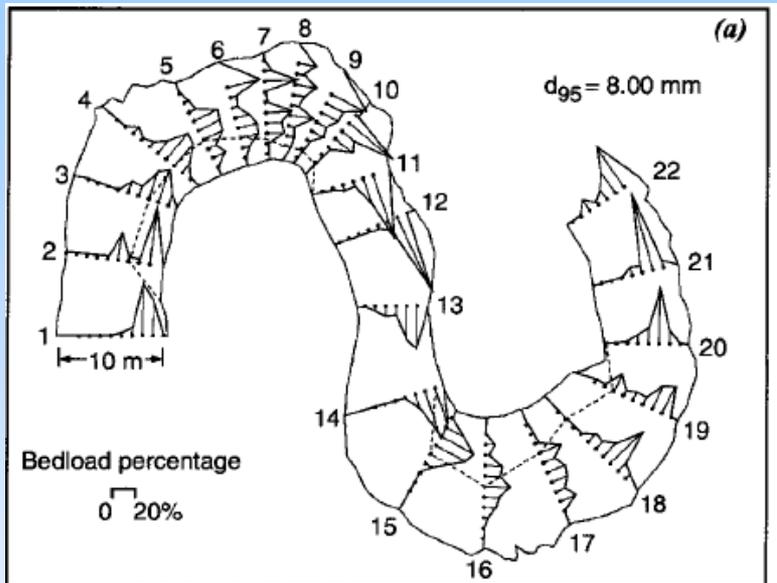


Fig. 3. Relation between SF and θ_1/ϕ ($M/N = 1$).

from Kawai and Julien (JHR-IAHR, 1996)

Sediment Transport in Sharp Bends



Field measurements in the sharp bends of the Fall River, Colorado demonstrate that particles of different sizes move in different directions.

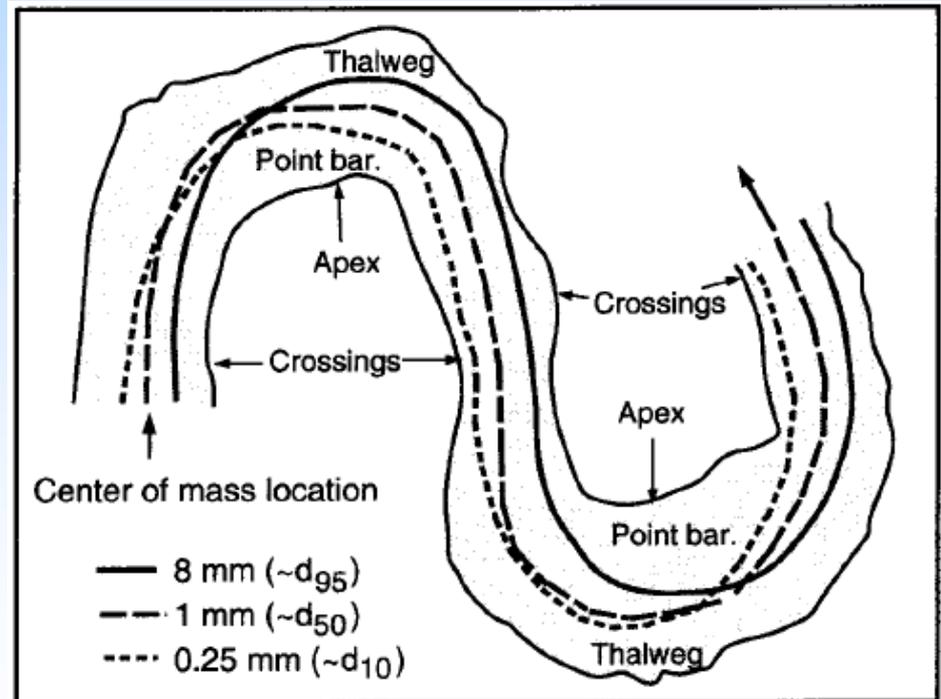


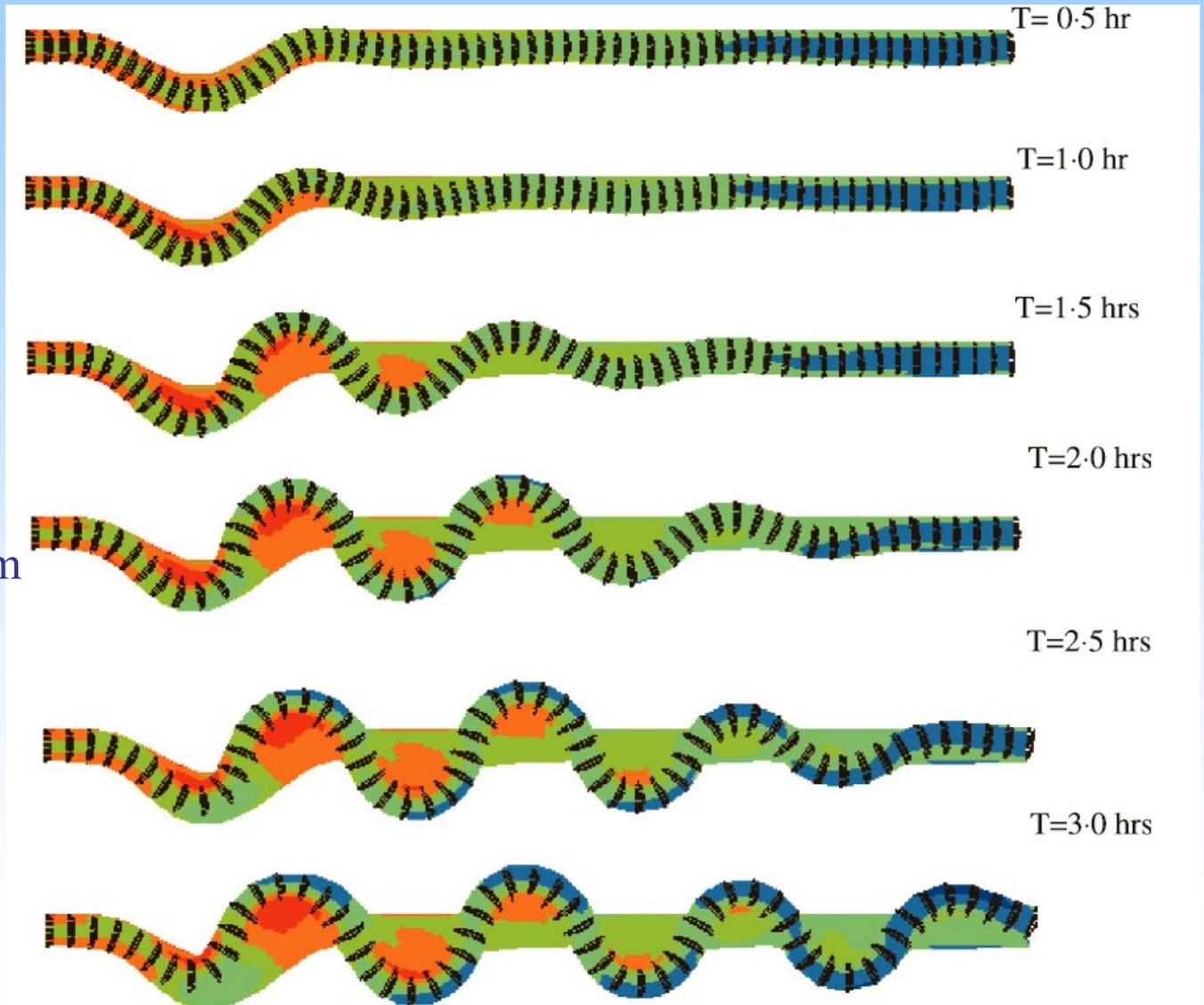
Fig. 5 Center of mass curves for three bedload size fractions

from Julien and Anthony (JHR-IAHR, 2002)

Meandering Simulations

Initial Conditions

- sine-generated
- deflection angle 30°
- discharge 2.1 l/s
- width 0.4 m
- length 13.2 m
- sediment size 0.45 mm



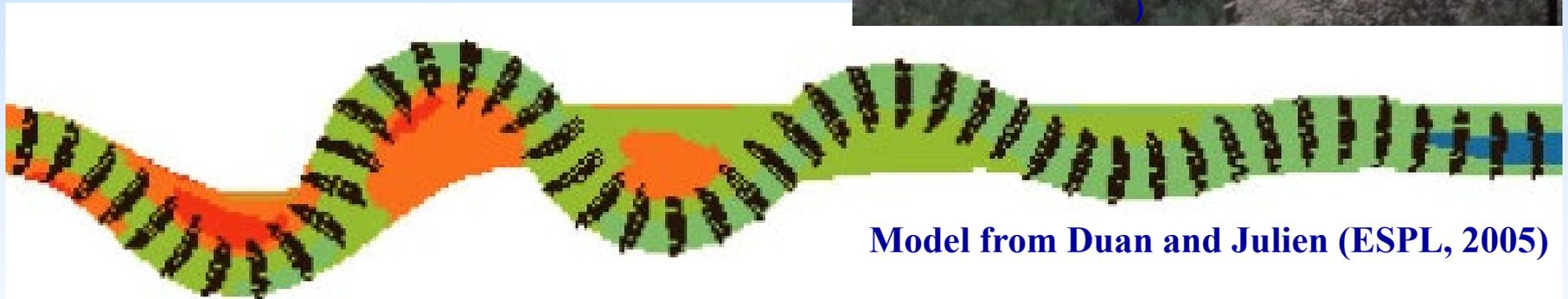
Model from Duan and Julien (ESPL, 2005)

Meandering Evolution

Example starting from a straight channel
on the Rio Puerco, New Mexico



Rio Puerco, New Mexico

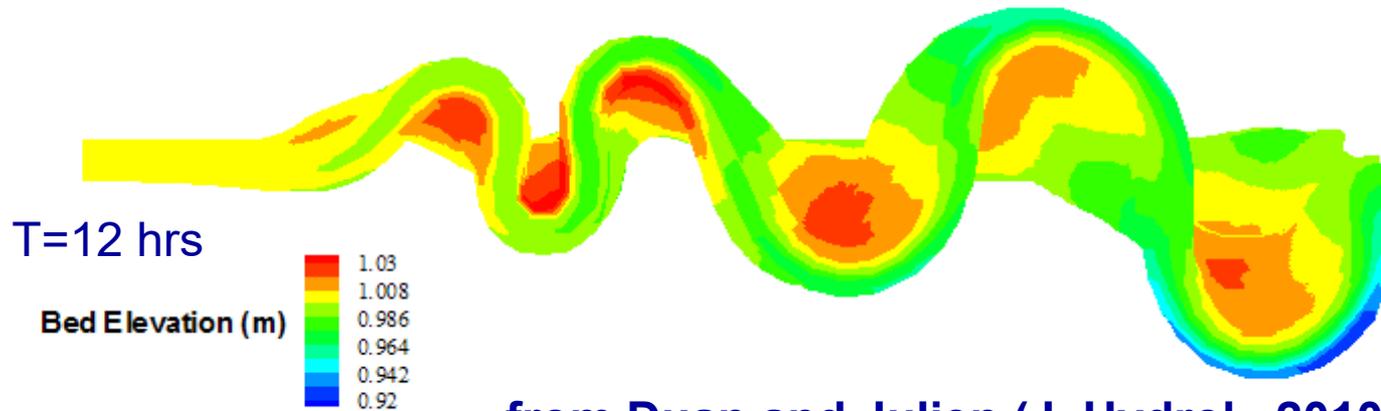
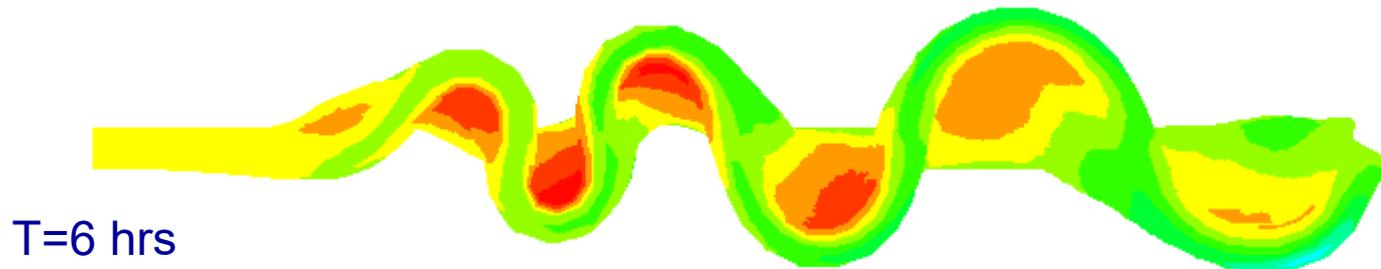
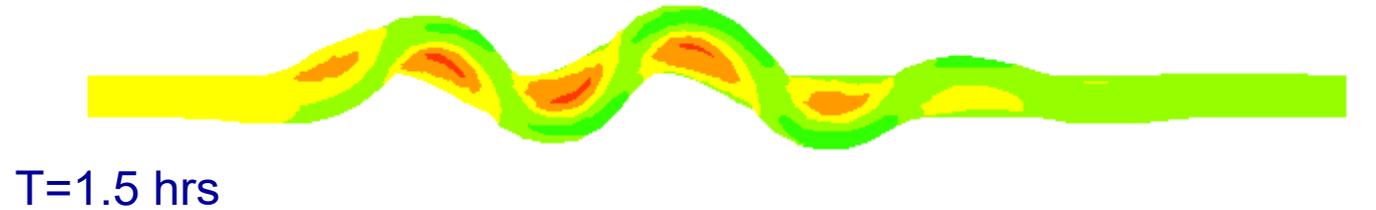


Model from Duan and Julien (ESPL, 2005)



Rio Puerco, New Mexico

Meandering Simulations



from Duan and Julien (J. Hydrol., 2010)

Lateral Migration in a Meandering Channel

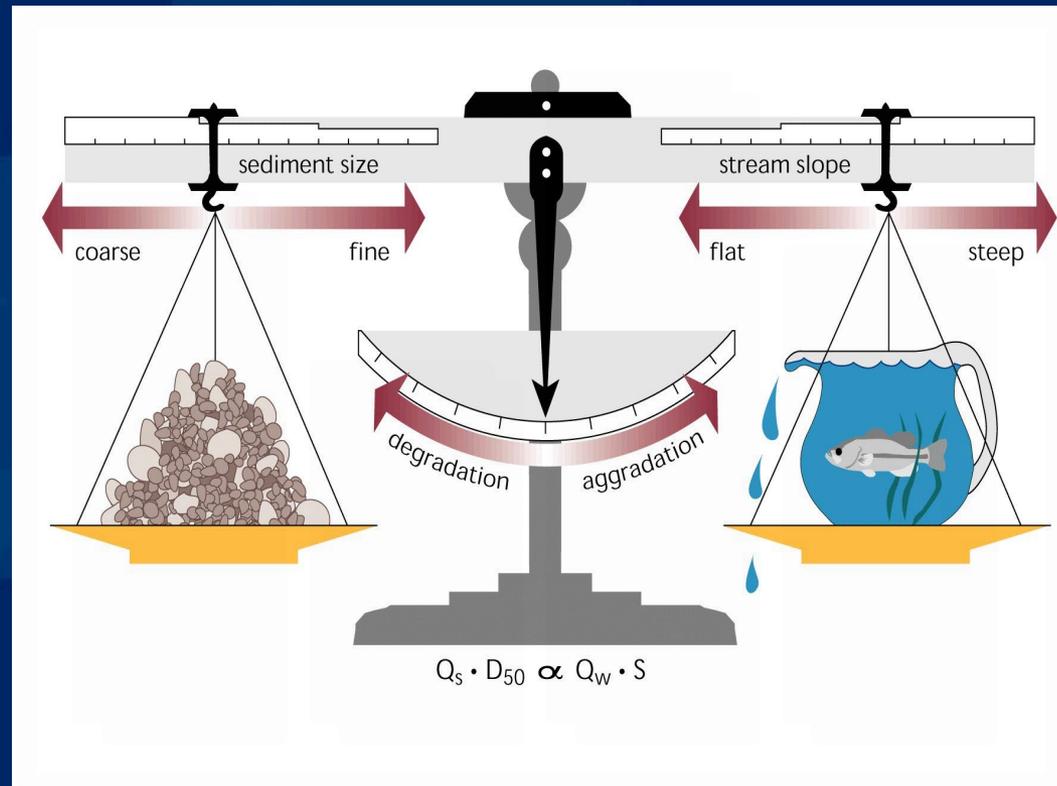


Rivers and Dams

1. River Equilibrium
2. **Aggradation**
3. Degradation below Dams
4. Case Study Gupo Bridge
5. Case Study Dam Break



2a. Meandering to Braiding (sediment overload)



Natural Chute Cutoffs

- Often in response to an increase in sediment load



- Chute cutoffs on Williams River, AK
(Photo by N.D. Smith)



Oxbow Lake

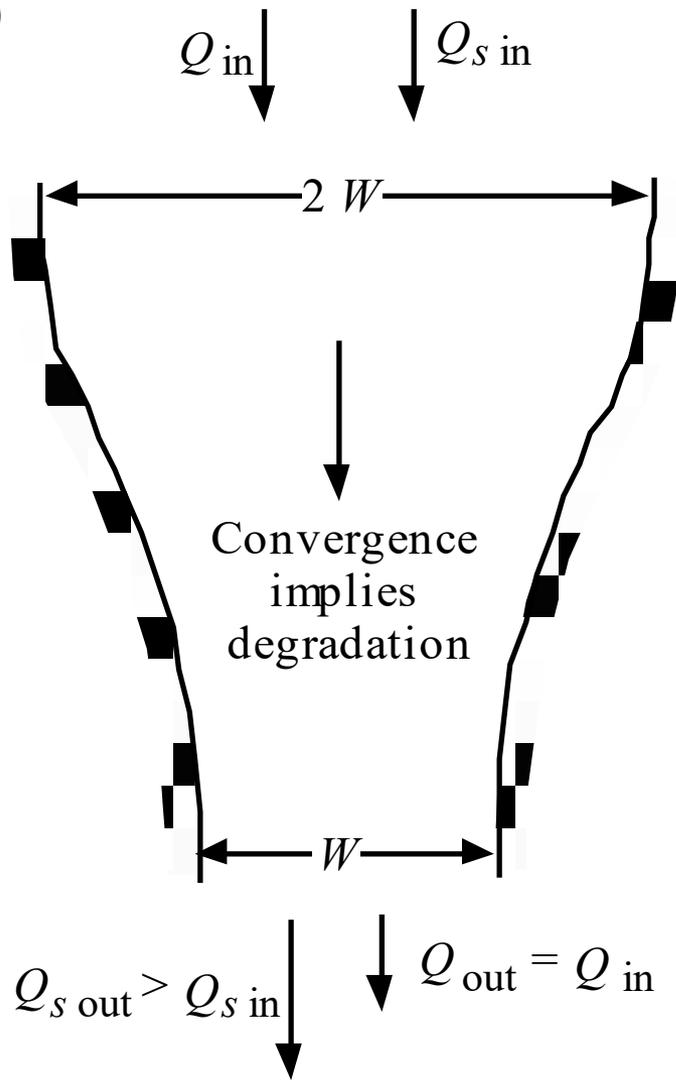


Riverbed rising forces
river overbank

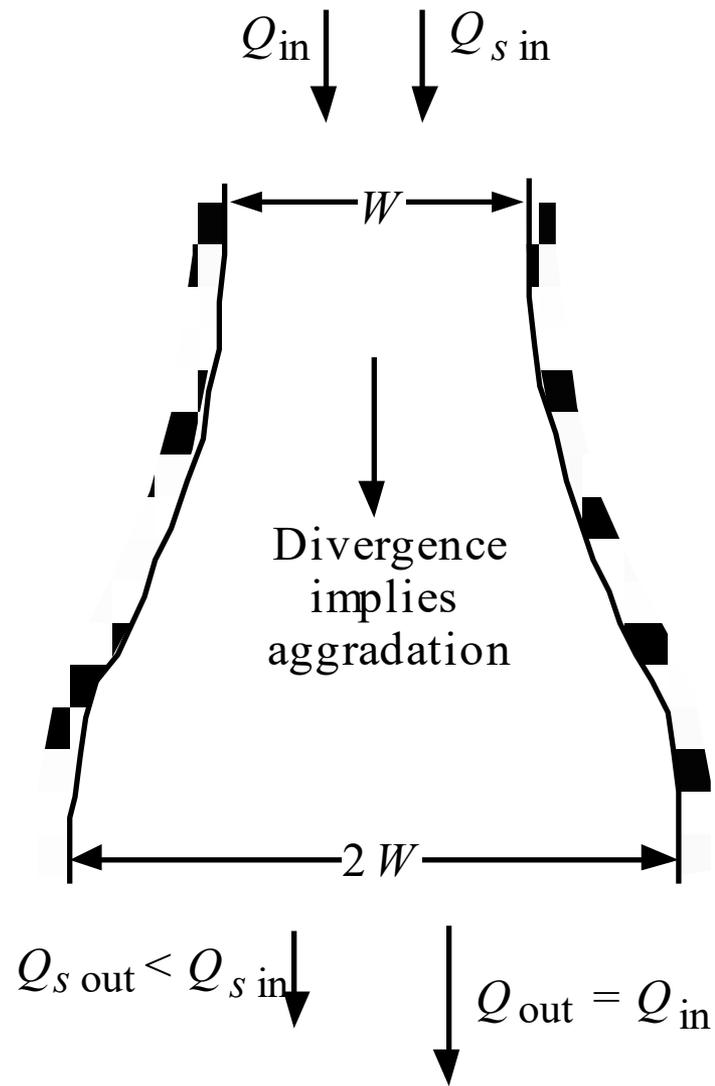


2b. Channel width variability

a)



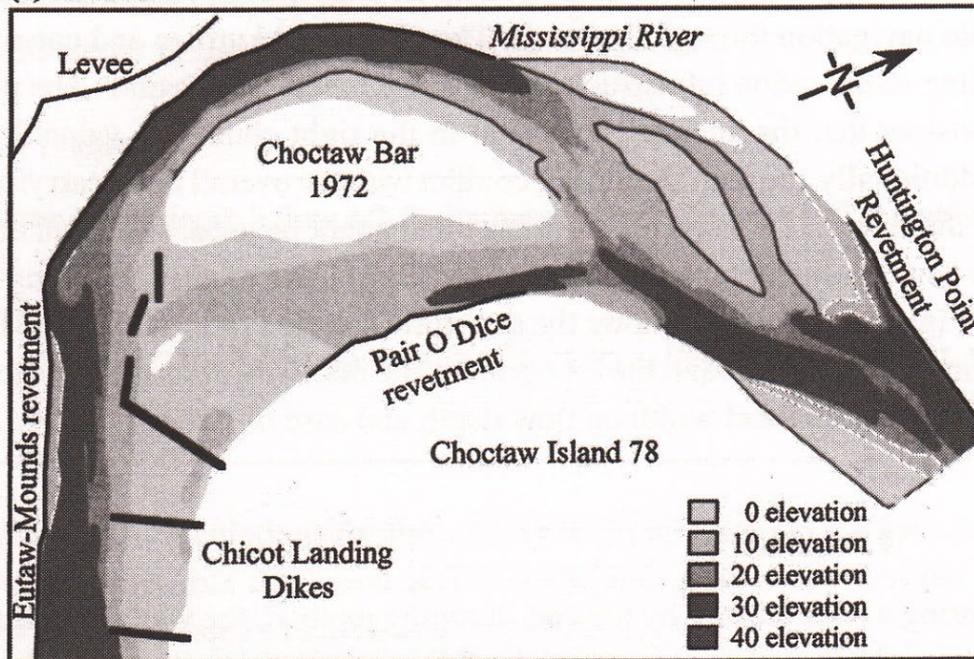
b)



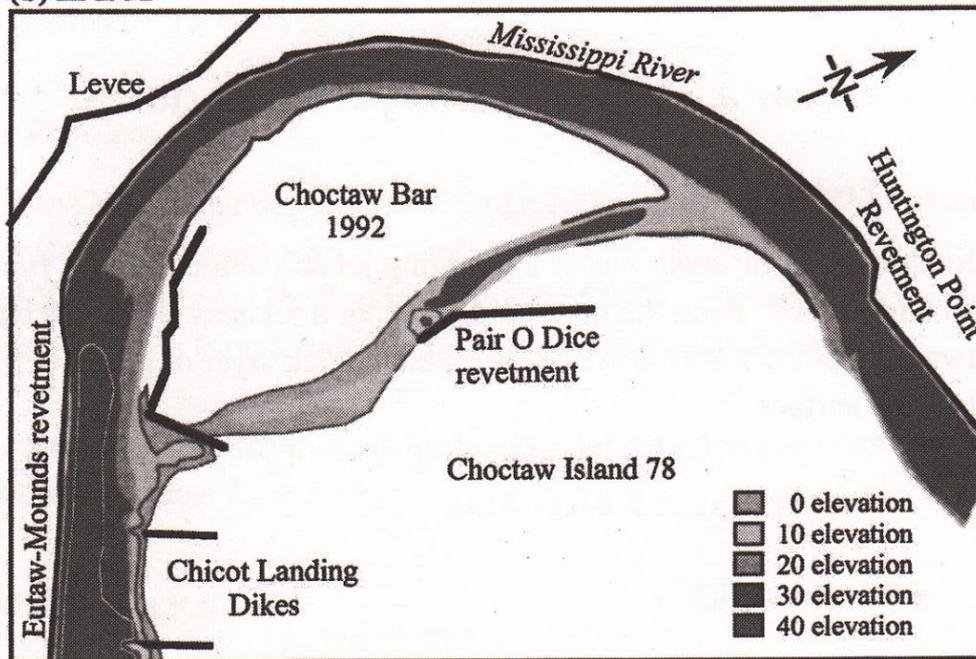
Dykes



(a) In 1972

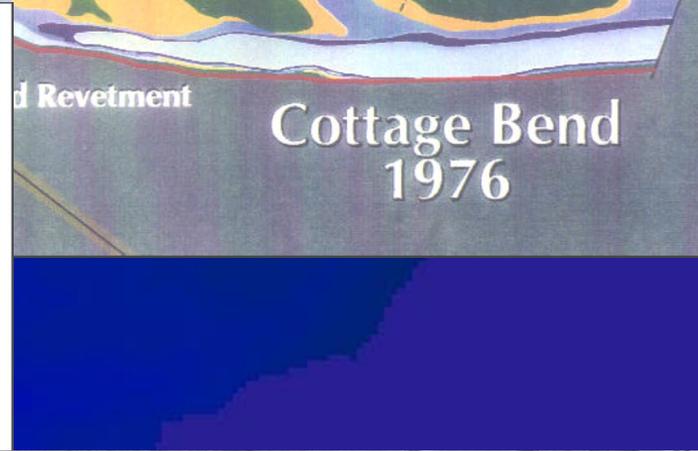
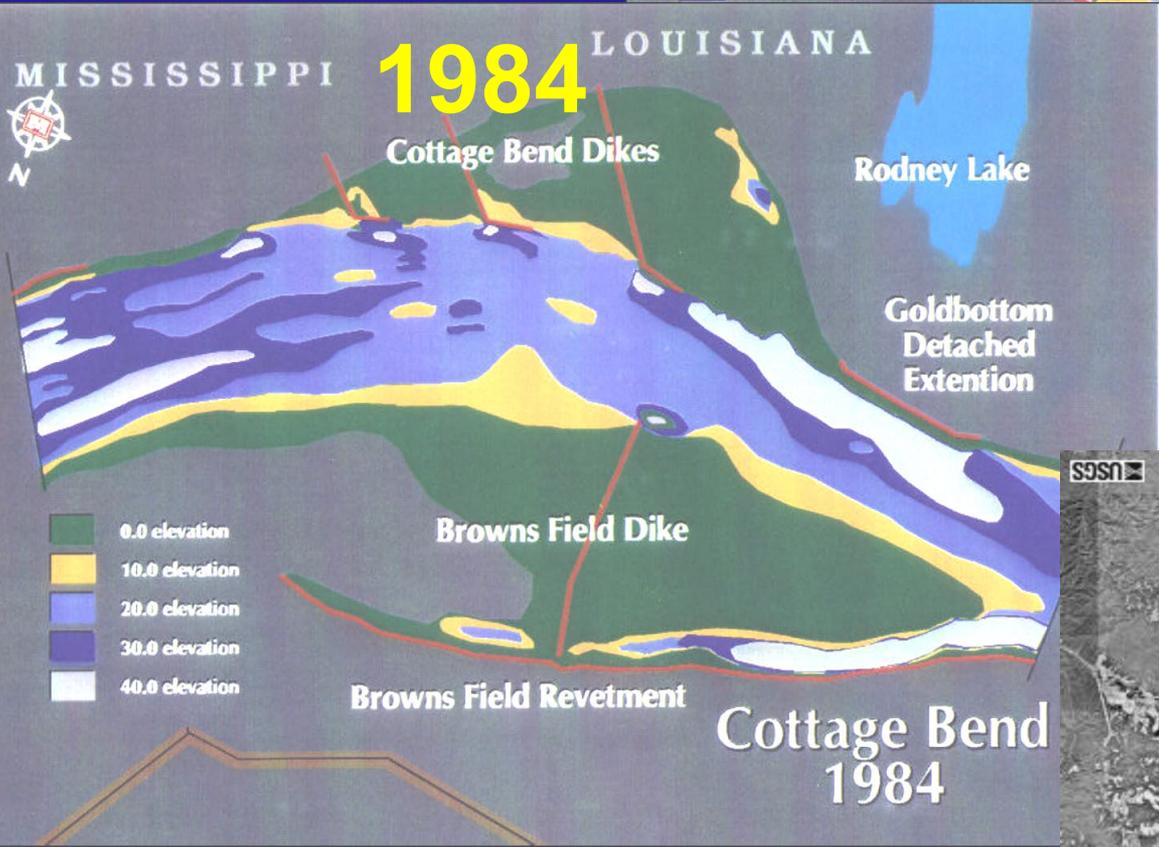


(b) In 1992



From Julien
River Mechanics
CUP 2018

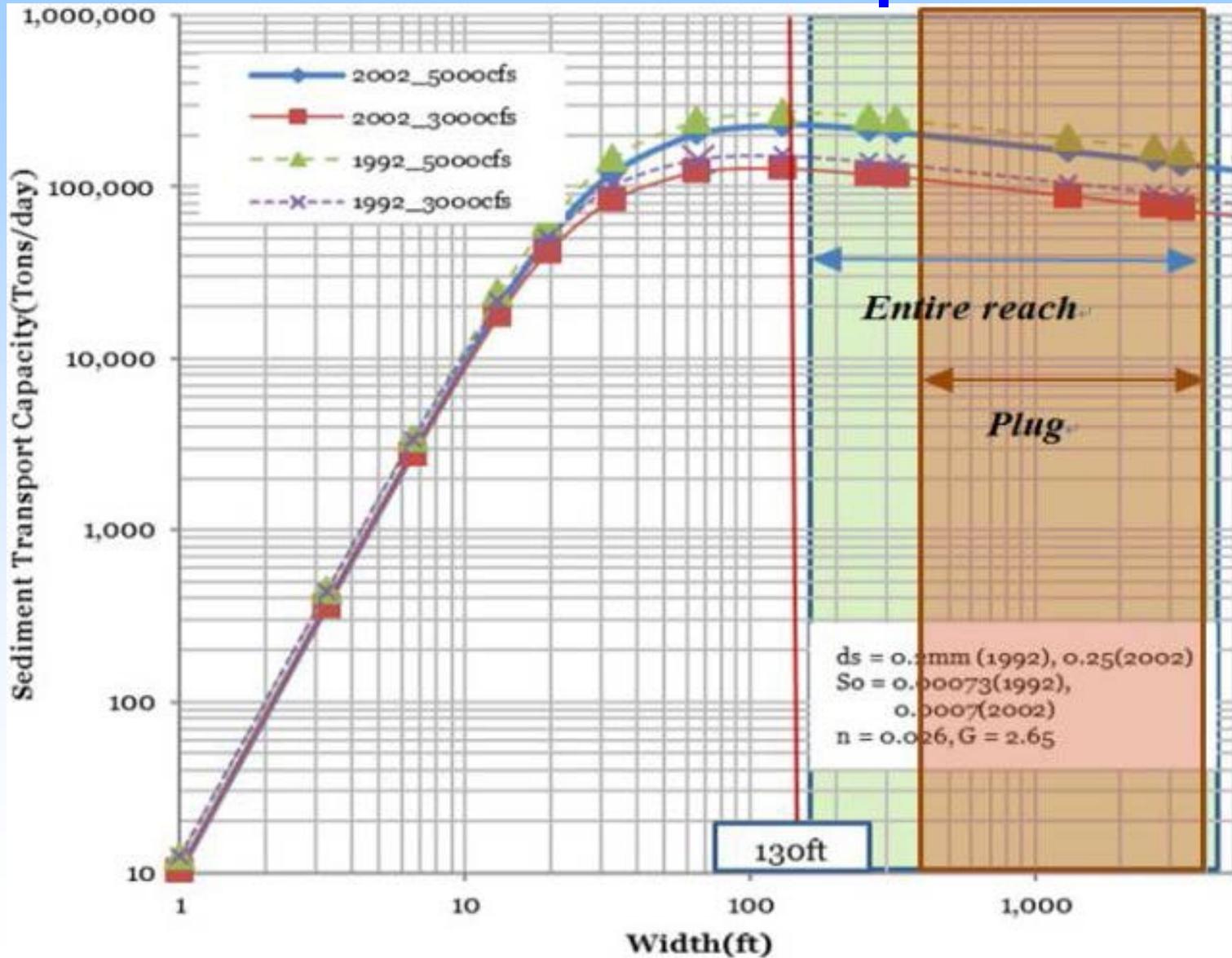
Cottage Bend



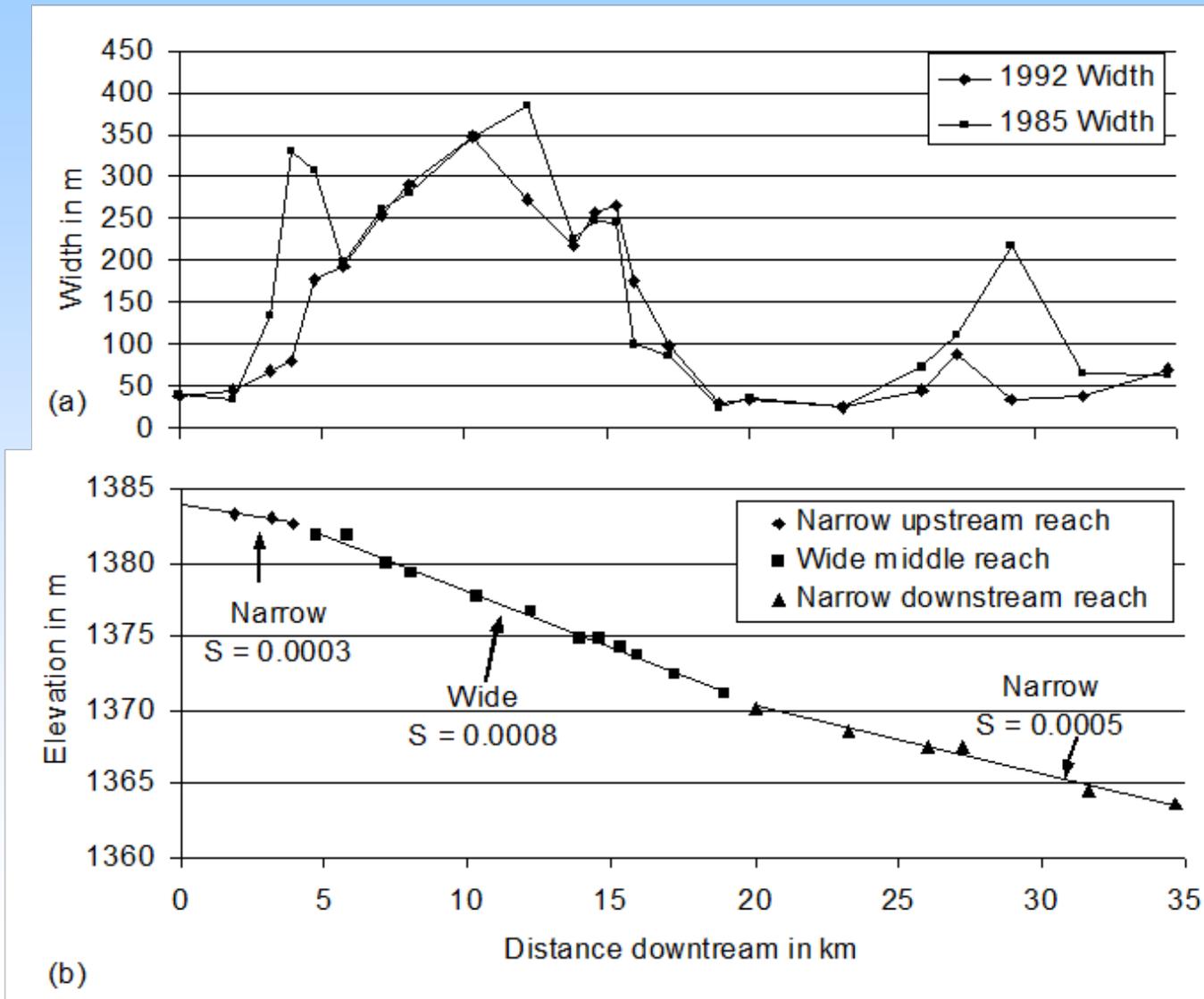
2c. Width-slope trade-offs



Relationship between channel width and sediment transport



Wider reaches are steeper!



Rivers and Dams

1. River Equilibrium
2. Aggradation
3. **Degradation below Dams**
4. Case Study Gupo Bridge
5. Case Study Dam Break



3a. Degradation Problems





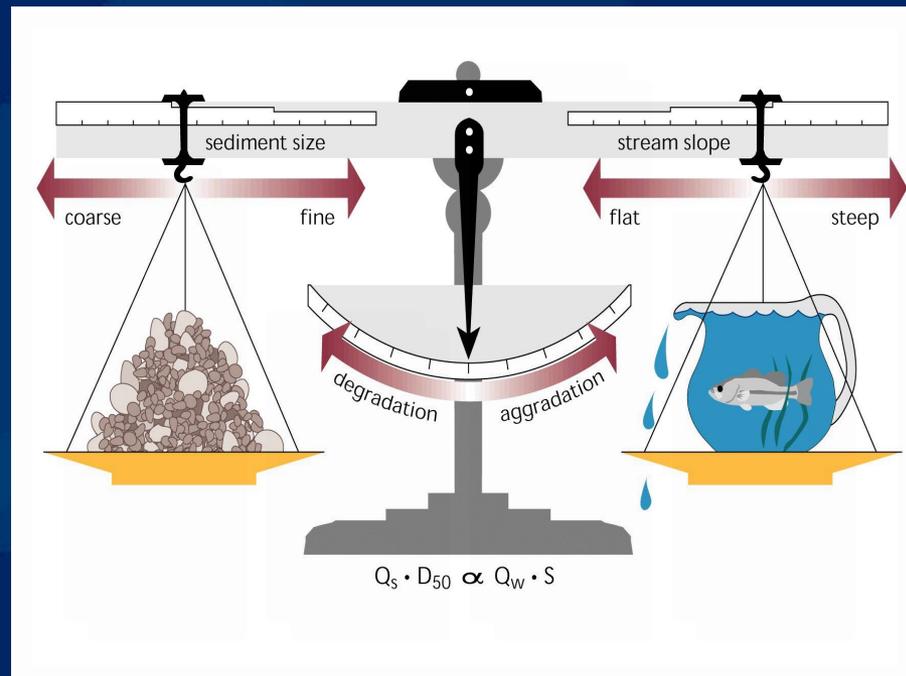








3b. Braiding to meandering (sediment starved)





**Cochiti
Dam**

Rio Grande

Santa Fe River

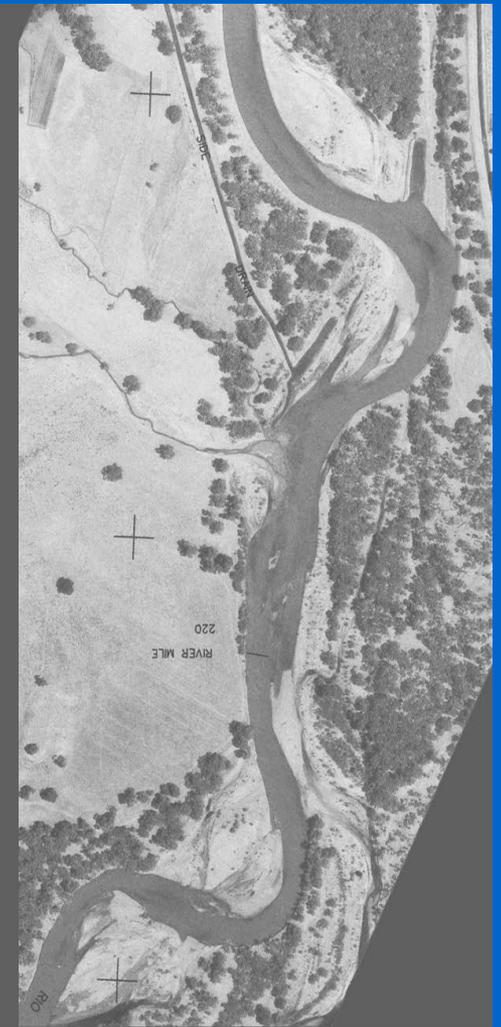
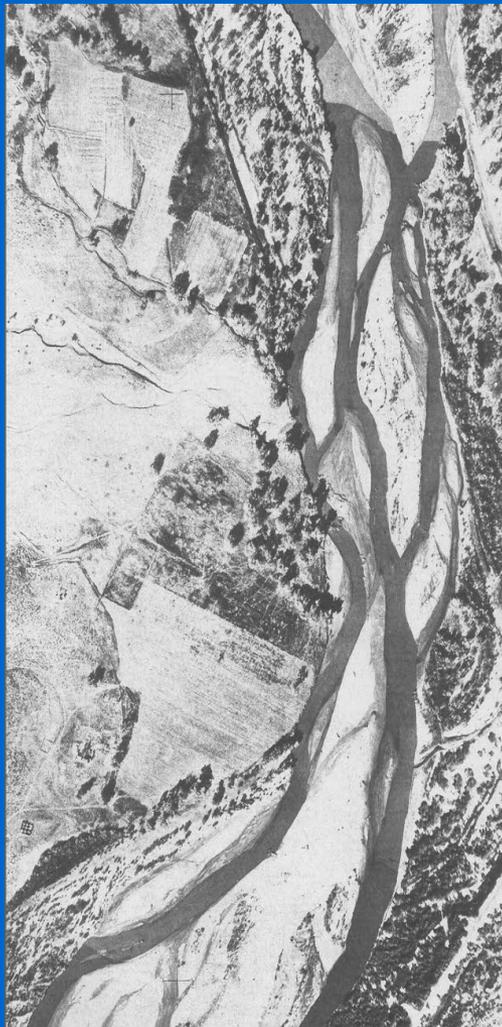


Planform geometry

1935

1972

1992



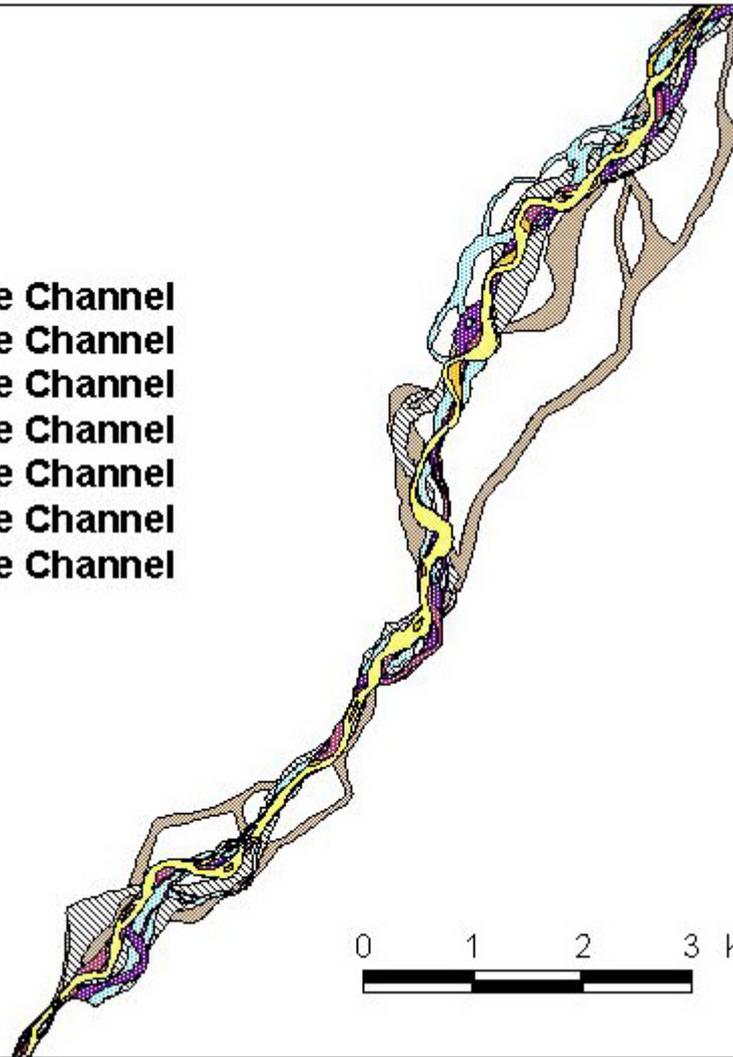
0 600 m

N

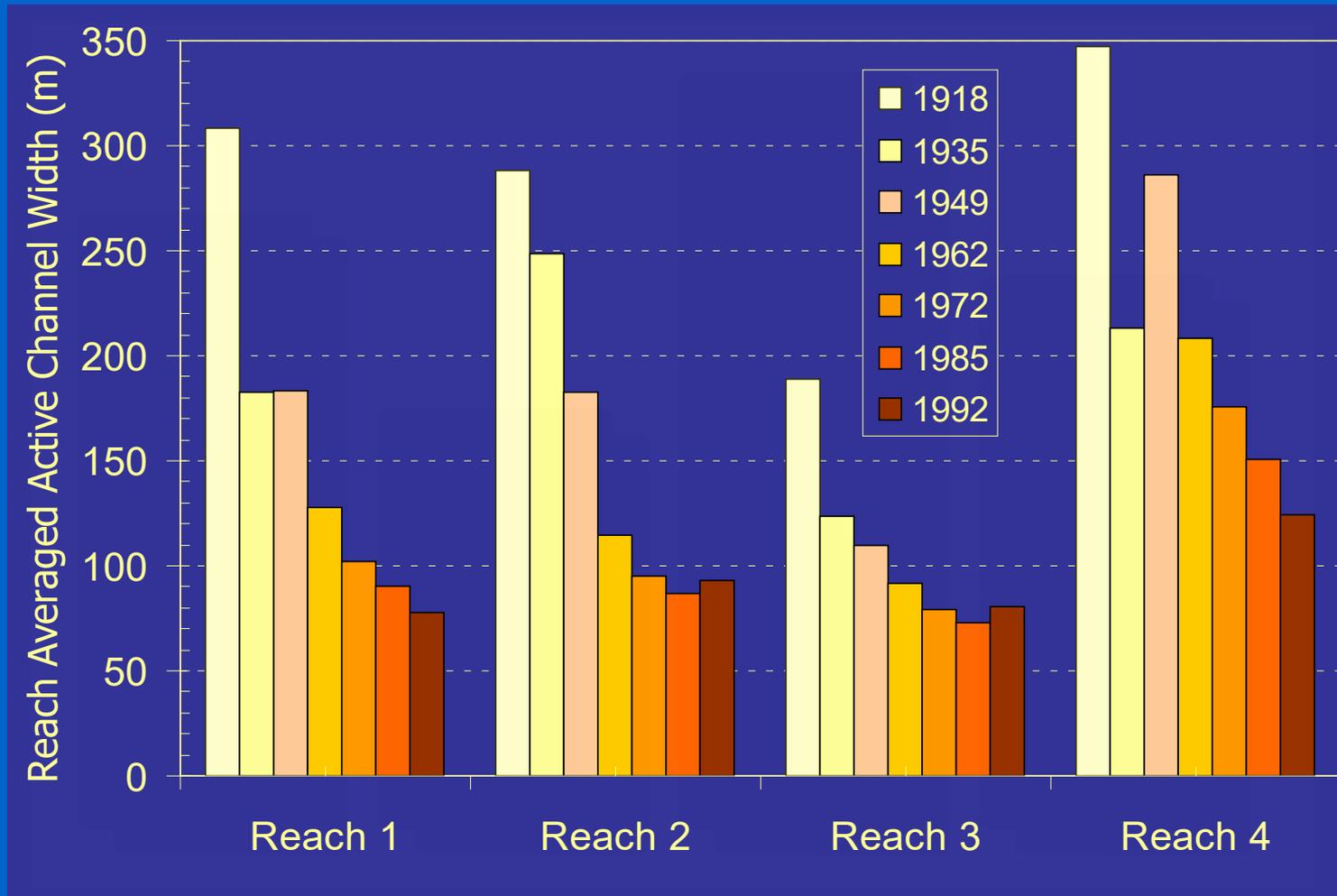
Lateral Adjustments

Reach 2

- 1992 Active Channel
- 1985 Active Channel
- 1972 Active Channel
- 1962 Active Channel
- 1949 Active Channel
- 1935 Active Channel
- 1918 Active Channel

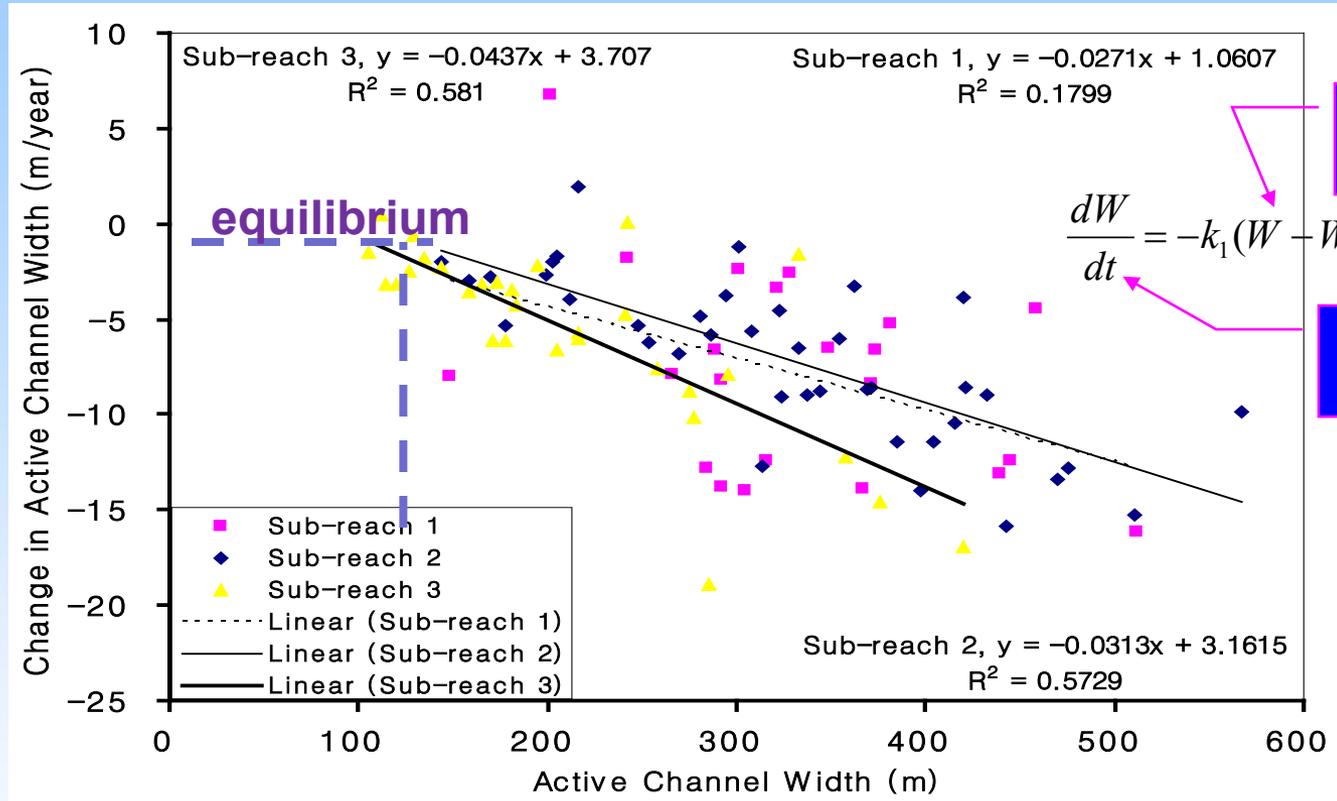


Active channel width



Changes in active channel width

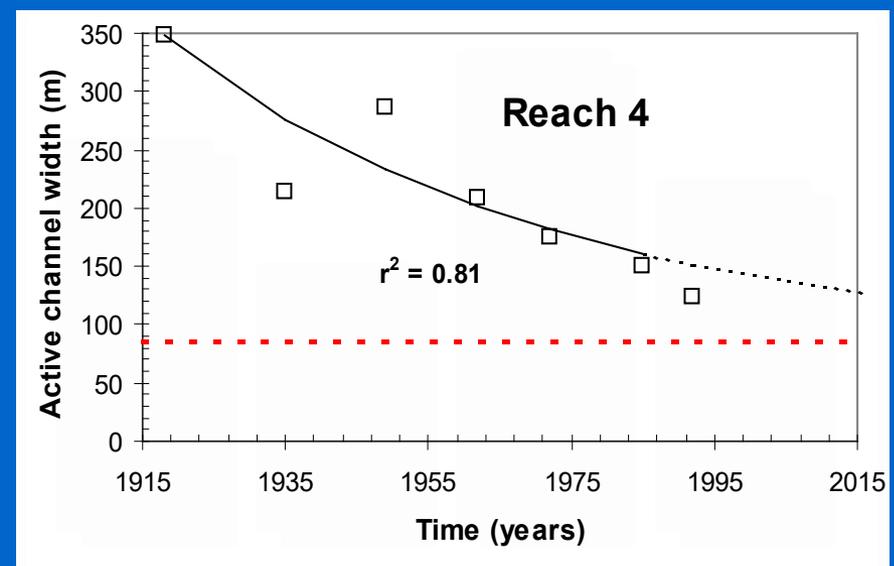
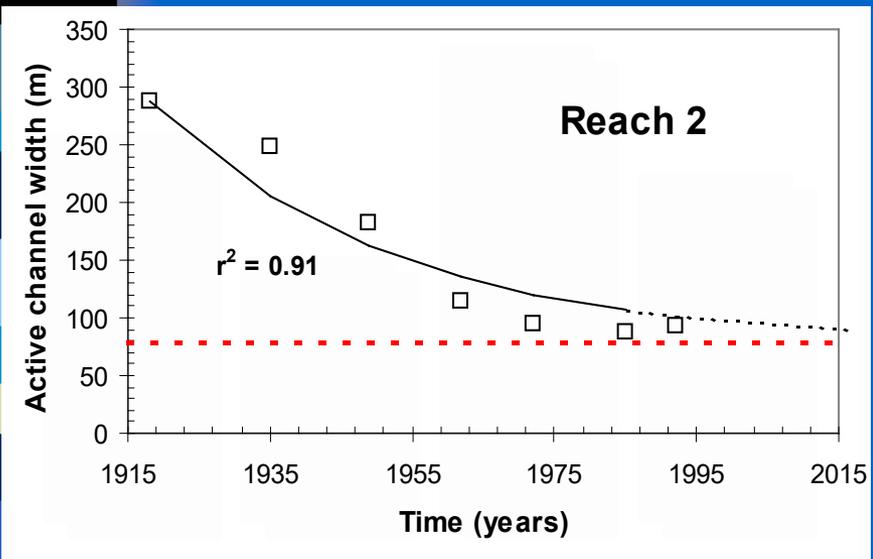
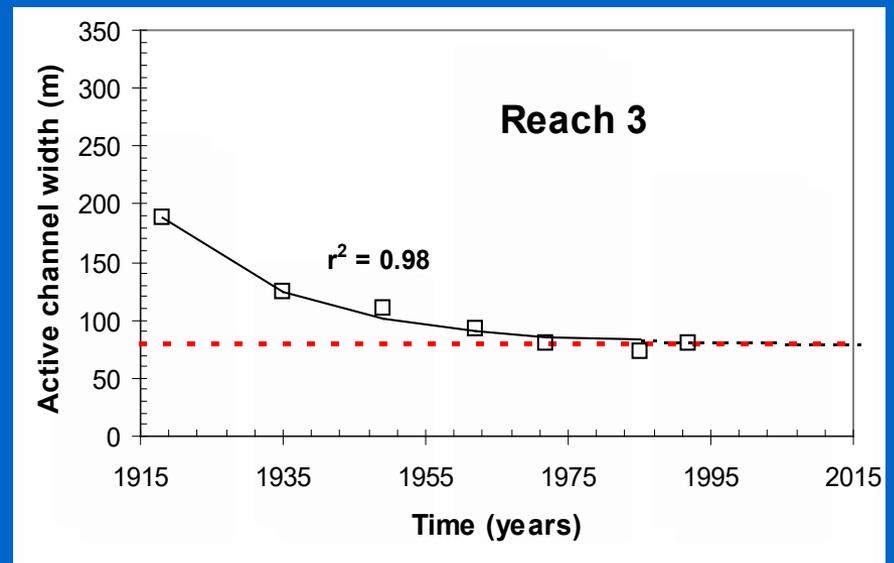
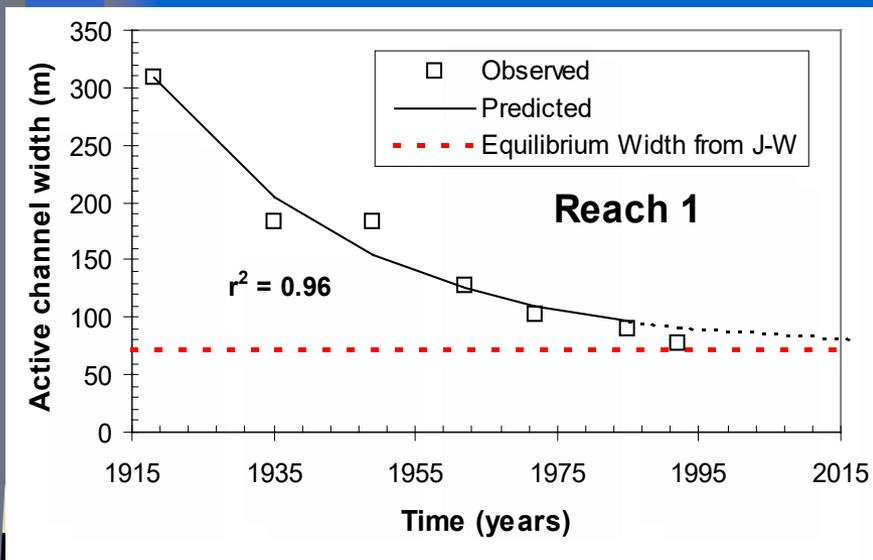
Rio Grande, NM (after Richard et al., 2005)



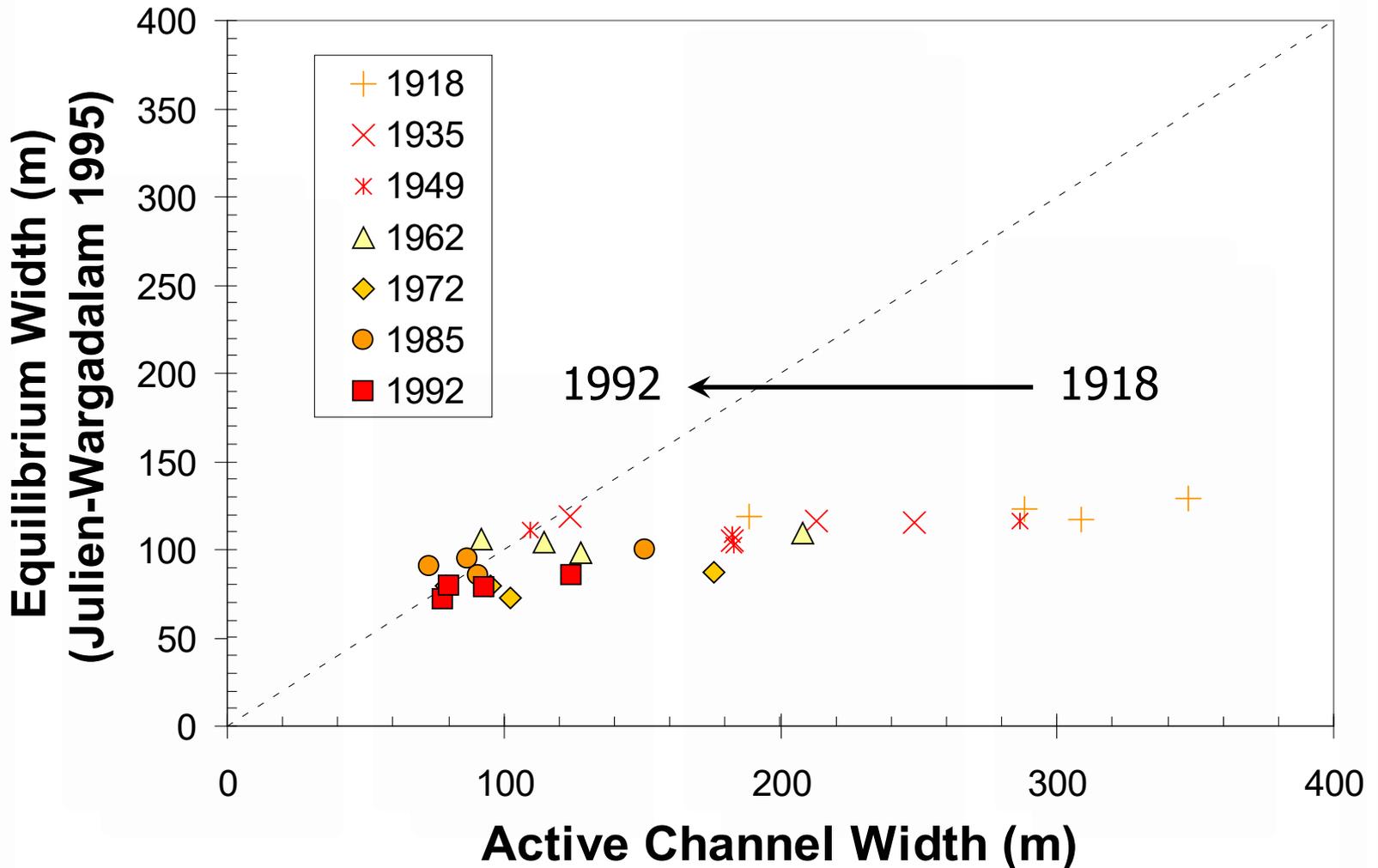
$$\frac{dW}{dt} = -k(W - W_e)$$

$$W = W_e + (W_o - W_e) \cdot e^{-kt}$$

Exponential Model Results



Hydraulic Geometry Equations (Julien & Wargadalam 1995)



3c. River Problems in Estuaries

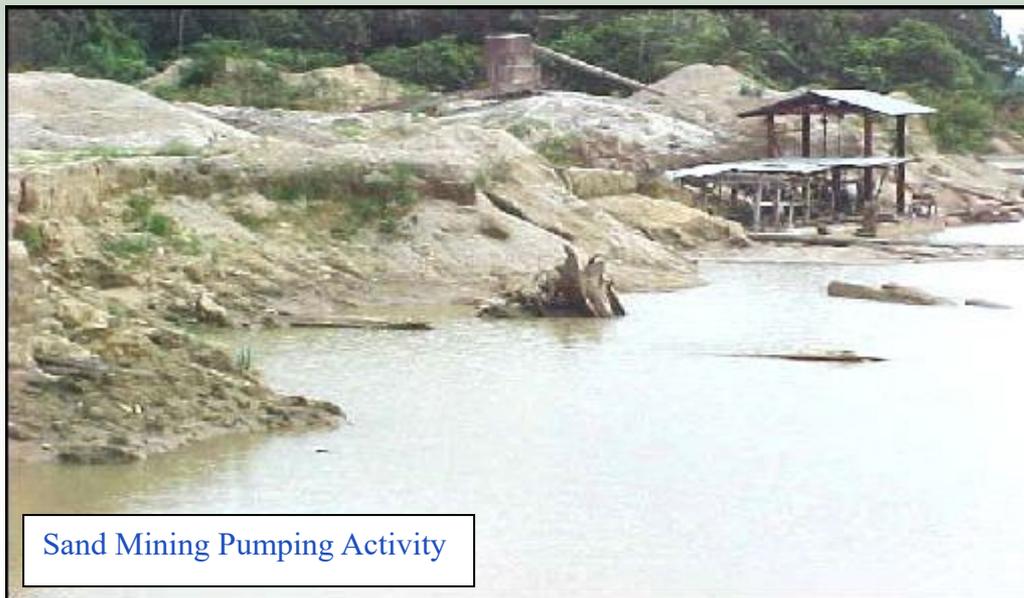
Sand and Gravel Mining



Kampong Kubang Bedengong



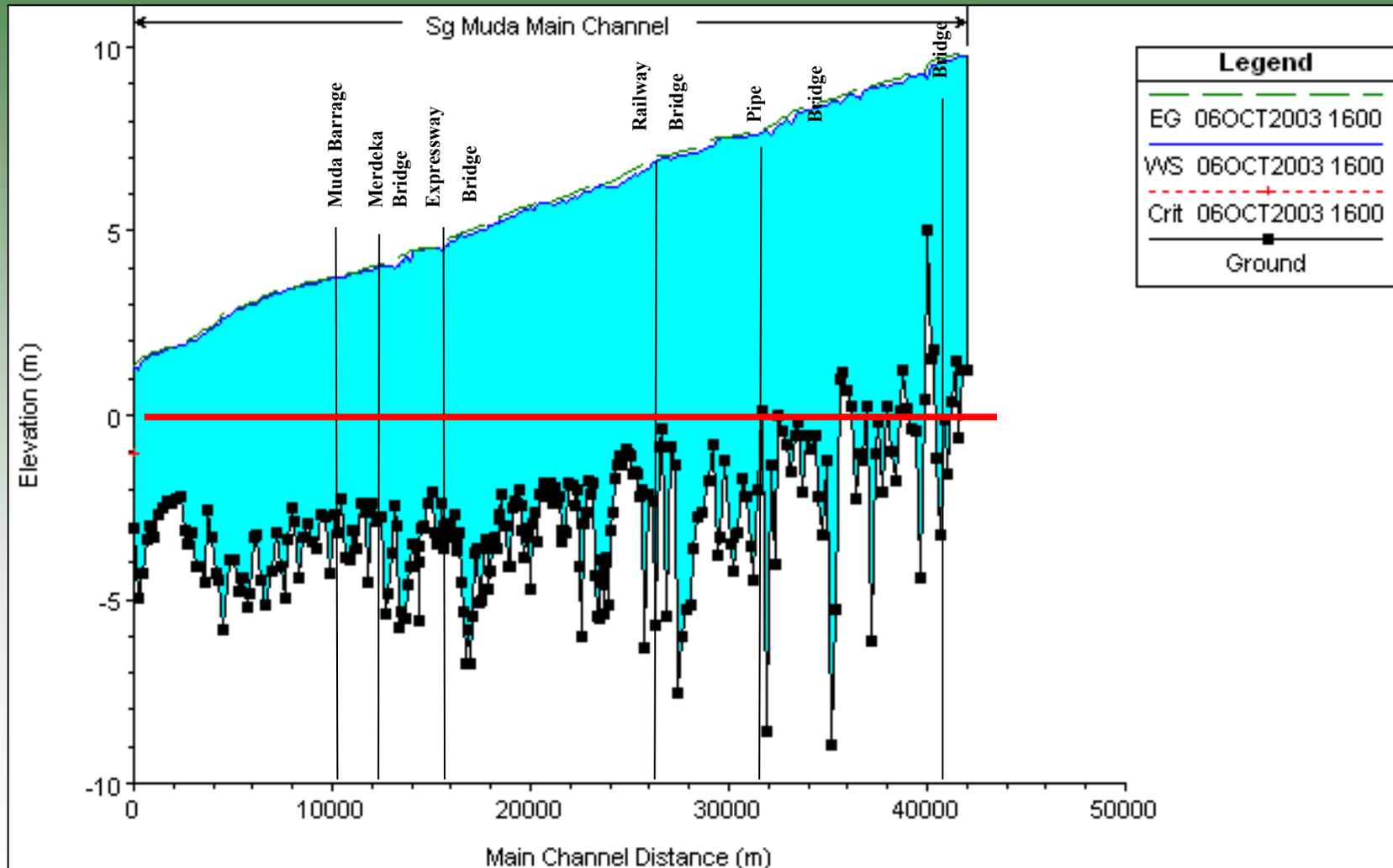
Kampong Lubok Segintah



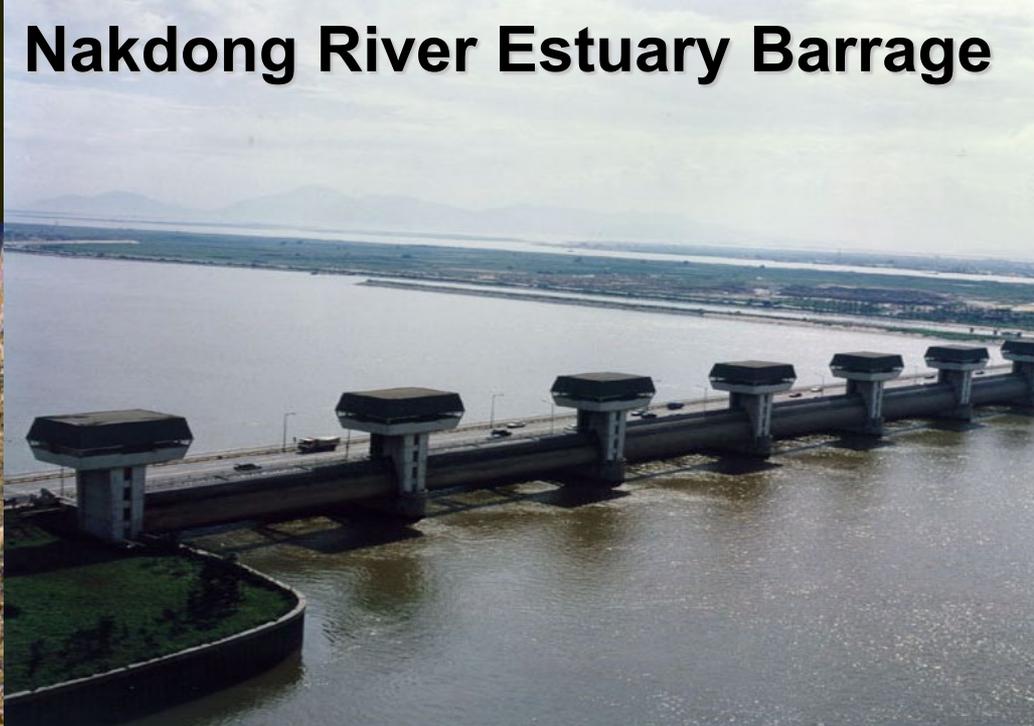
Sand Mining Pumping Activity

River Sand
Mining

Longitudinal Flood Profile for Sg Muda ($Q=1340\text{m}^3/\text{s}$)



Nakdong River Estuary Barrage



•from Ji et al. ASCE-JHE, Nov. 2011

Rivers and Dams

1. River Equilibrium
2. Aggradation
3. Degradation below Dams
4. **Case Study Gupo Bridge**
5. Case Study Dam Break

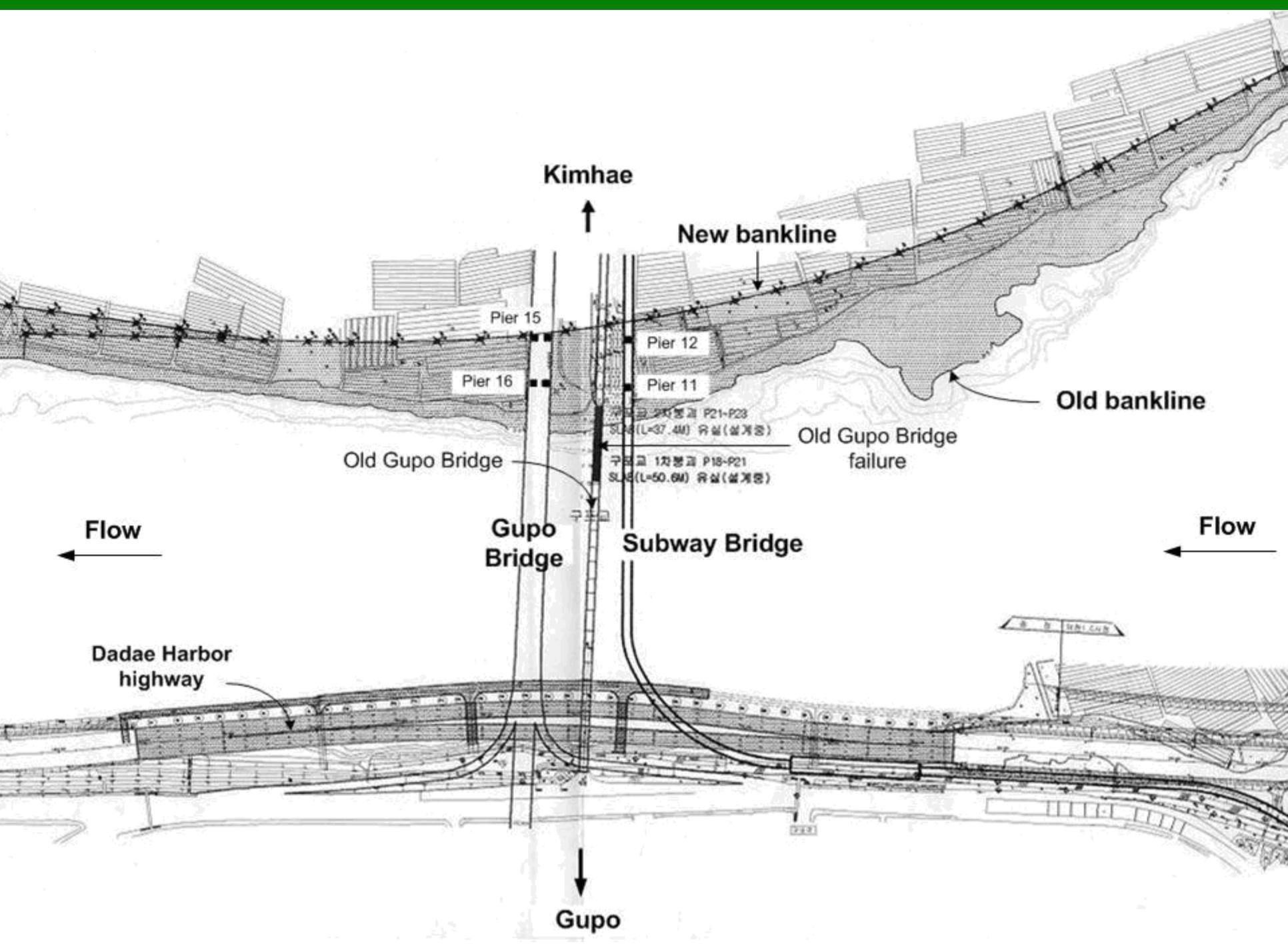


Case-Study: Gupo Bridge during Typhoon Maemi in 2003





P10



Kimhae

New bankline

Pier 15

Pier 12

Pier 16

Pier 11

Old bankline

Old Gupo Bridge

Old Gupo Bridge failure

Flow

Flow

Gupo Bridge

Subway Bridge

Dadae Harbor highway

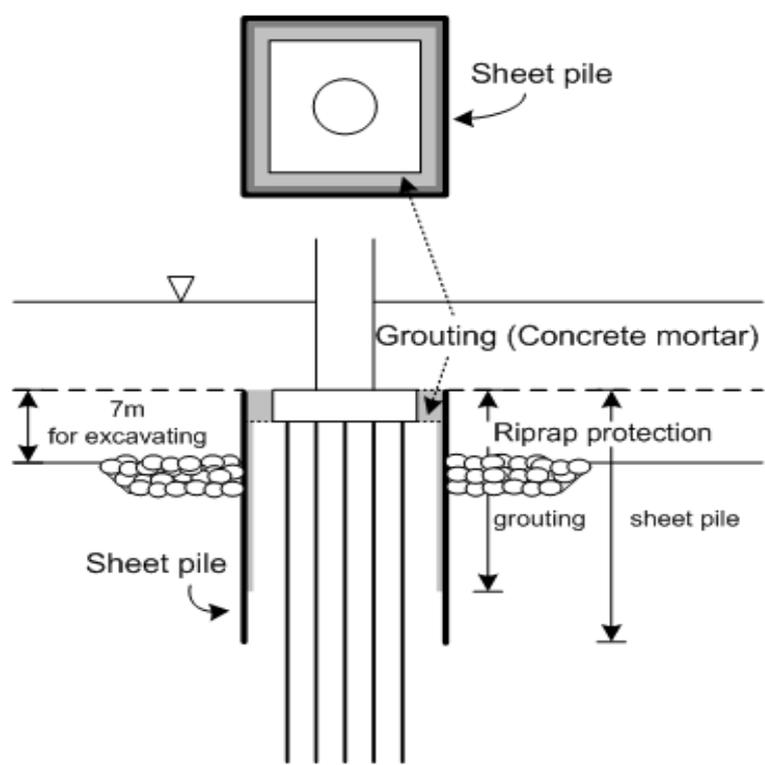
Gupo

구포교 2차정교 P21-P23
SL4 (L=37.4M) 유실(설계중)
구포교 1차정교 P19-P21
SL6 (L=50.6M) 유실(설계중)

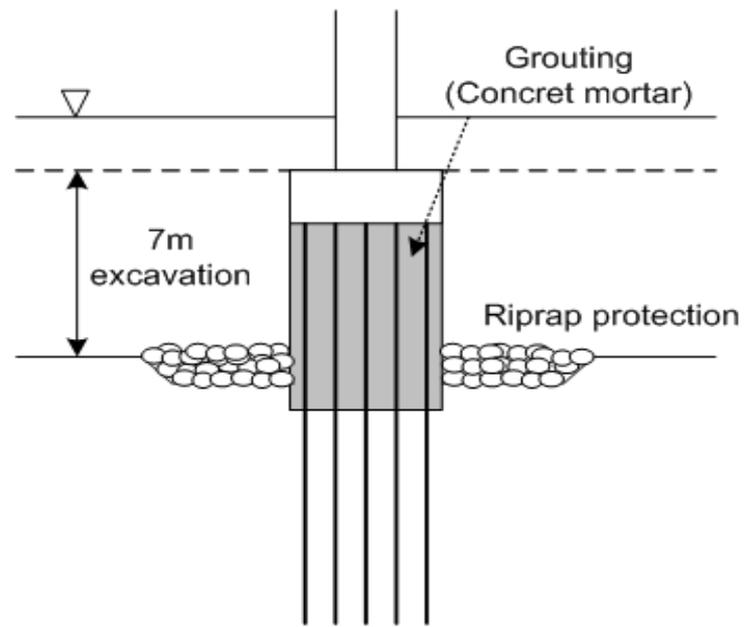
구포교



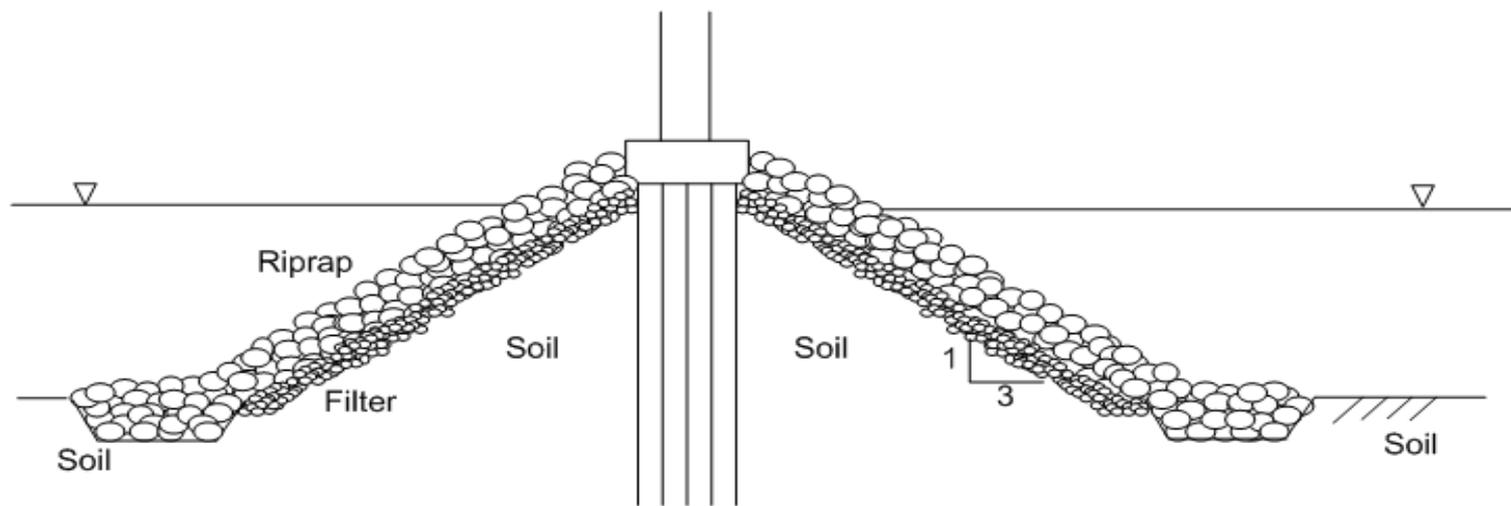
P15



Alternative plan I



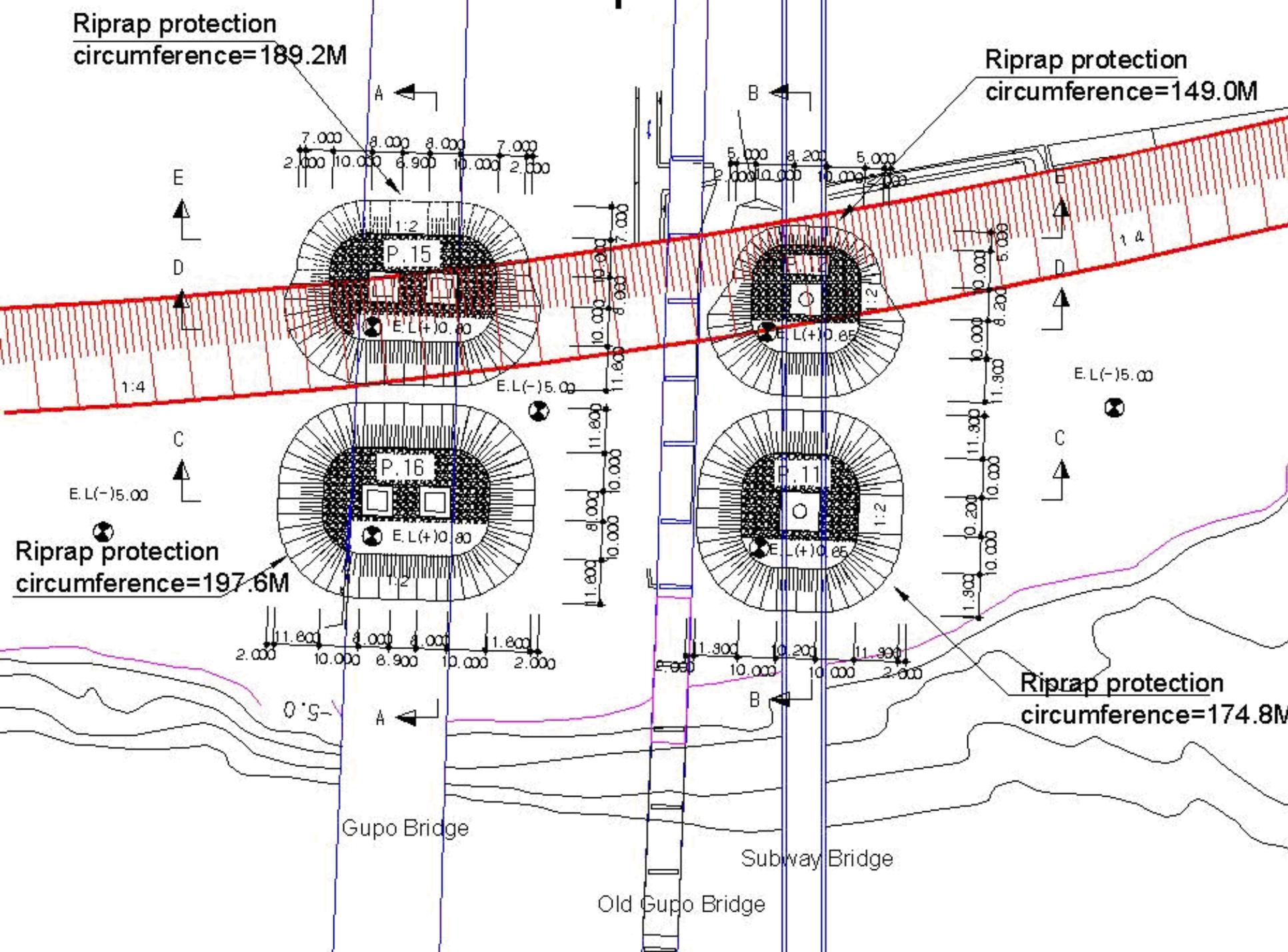
Alternative plan II



Alternative plan III

Riprap protection
circumference=189.2M

Riprap protection
circumference=149.0M



Riprap protection
circumference=197.6M

Riprap protection
circumference=174.8M

Gupo Bridge

Subway Bridge

Old Gupo Bridge

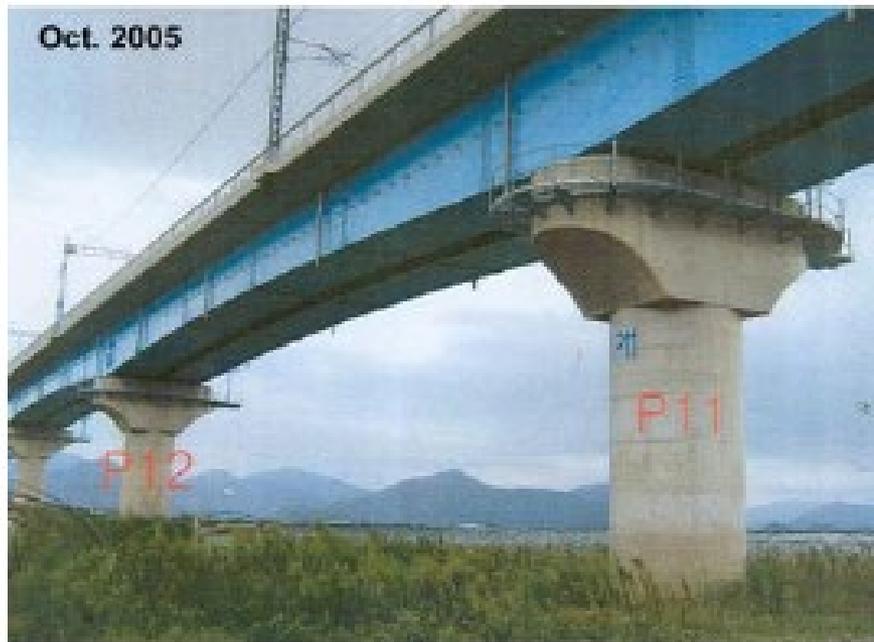
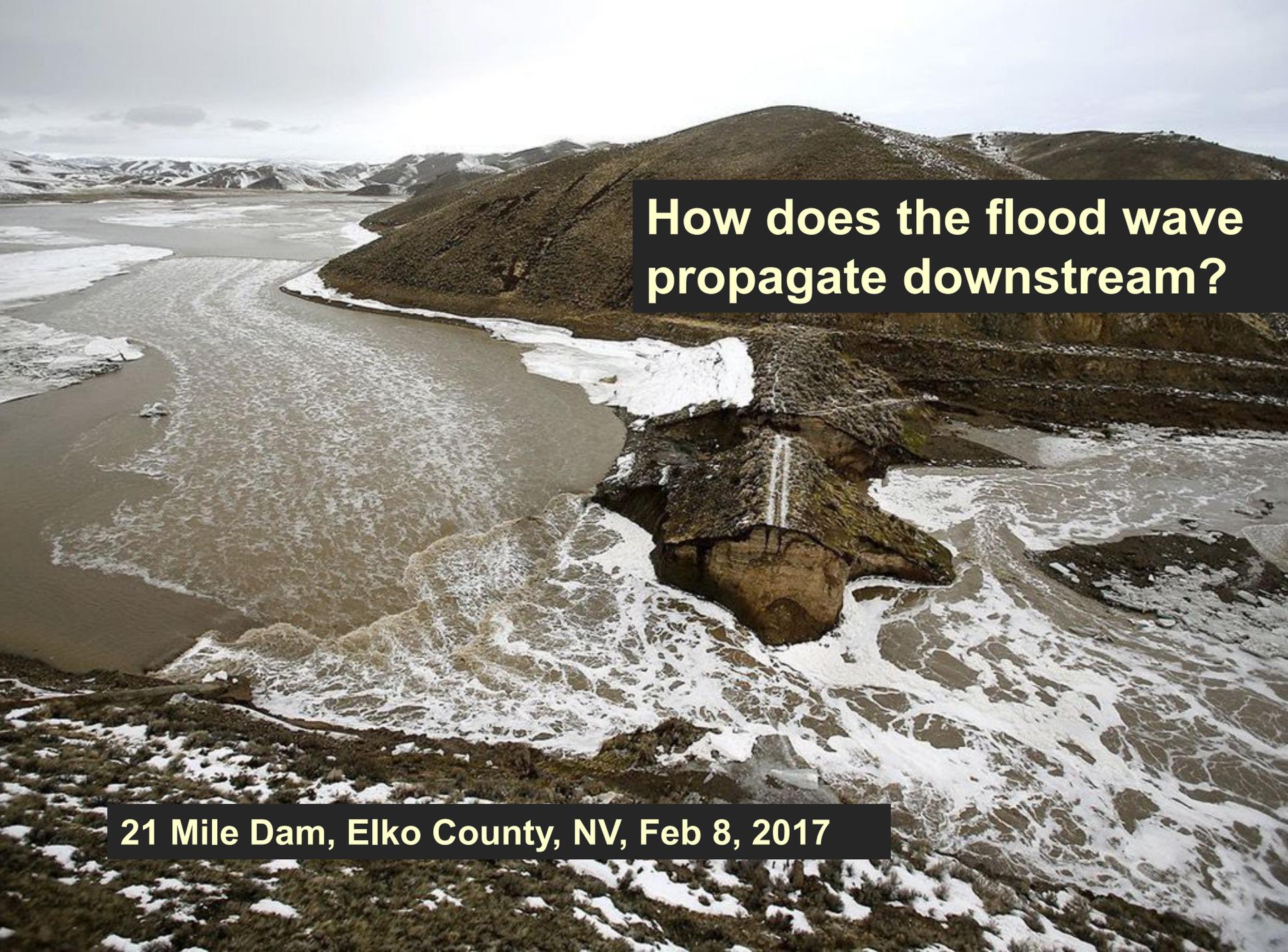


Figure 14. Gupo and Subway Bridge Piers before and after retrofitting construction

Rivers and Dams

1. River Equilibrium
2. Aggradation
3. Degradation below Dams
4. Case Study Gupo Bridge
5. Case Study Dam Break



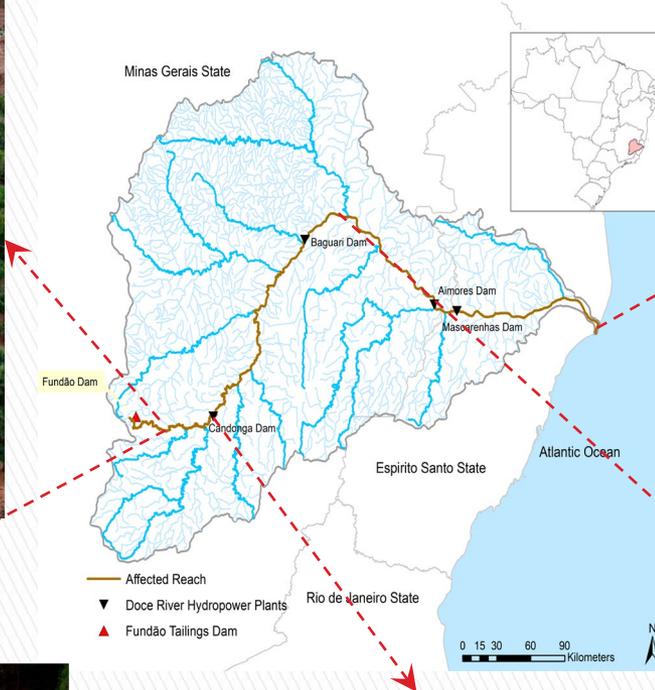


How does the flood wave propagate downstream?

21 Mile Dam, Elko County, NV, Feb 8, 2017

The Fundão Dam Collapse

**Bento Rodrigues Town,
6 November 2015**



**Coast, 21 November 2015
C ≈ 1,500 mg/l**



**Doce River at
Governador Valadares City
11 November 2015,
C ≈ 30,000 mg/l**

**Gesteira Town
6 November 2015**



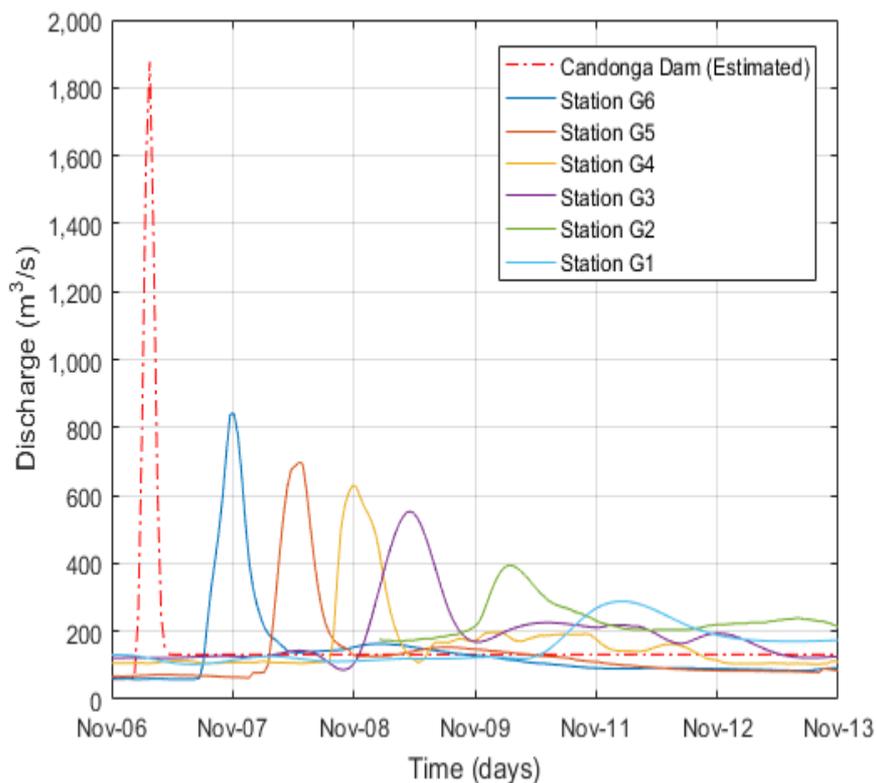
**Candonga Dam, 6 November 2015
C ≈ 700,000 mg/l**



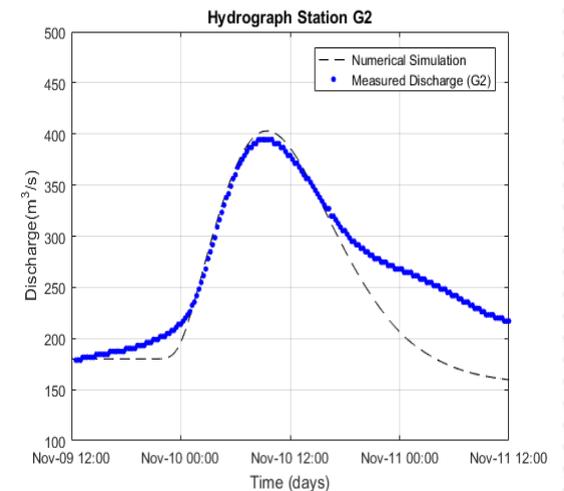
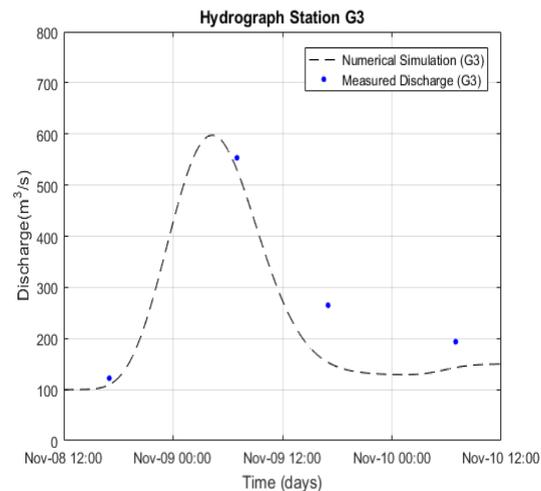
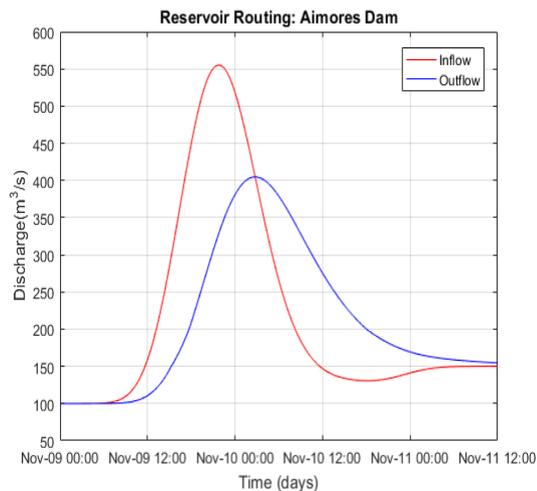
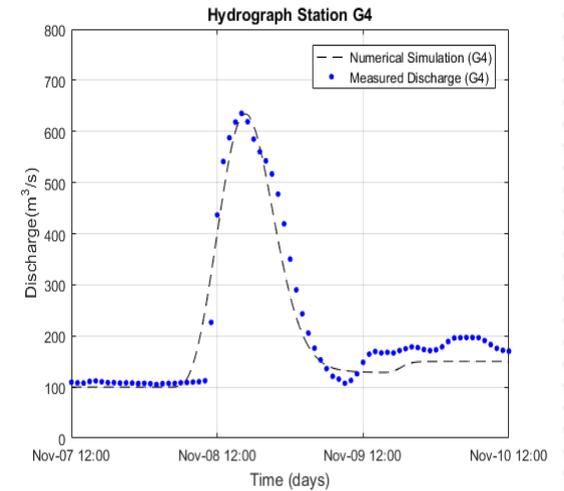
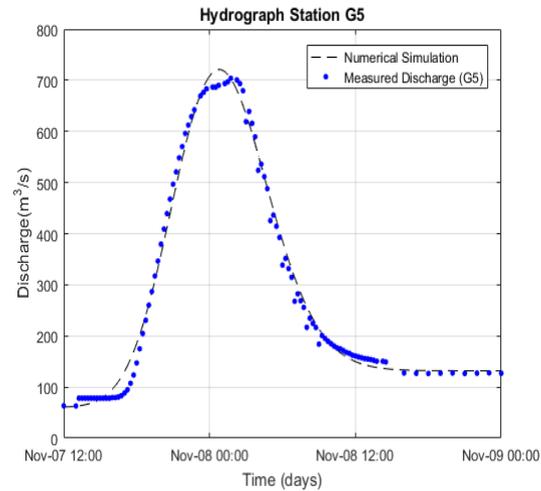
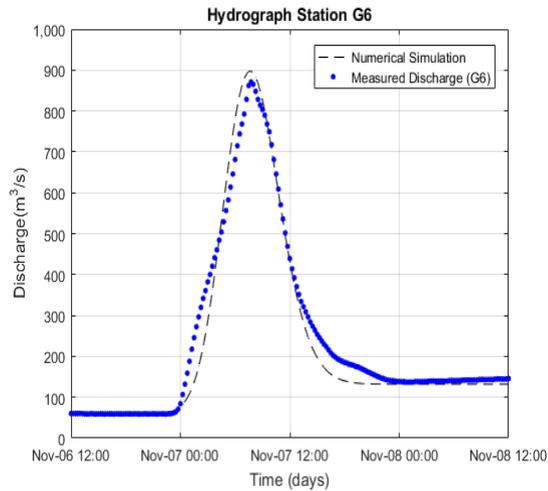
from Marcos Palu (2018)

Hydrographs

Observed hydrographs in Doce River after the Fundão Dam break (ANA, 2015).



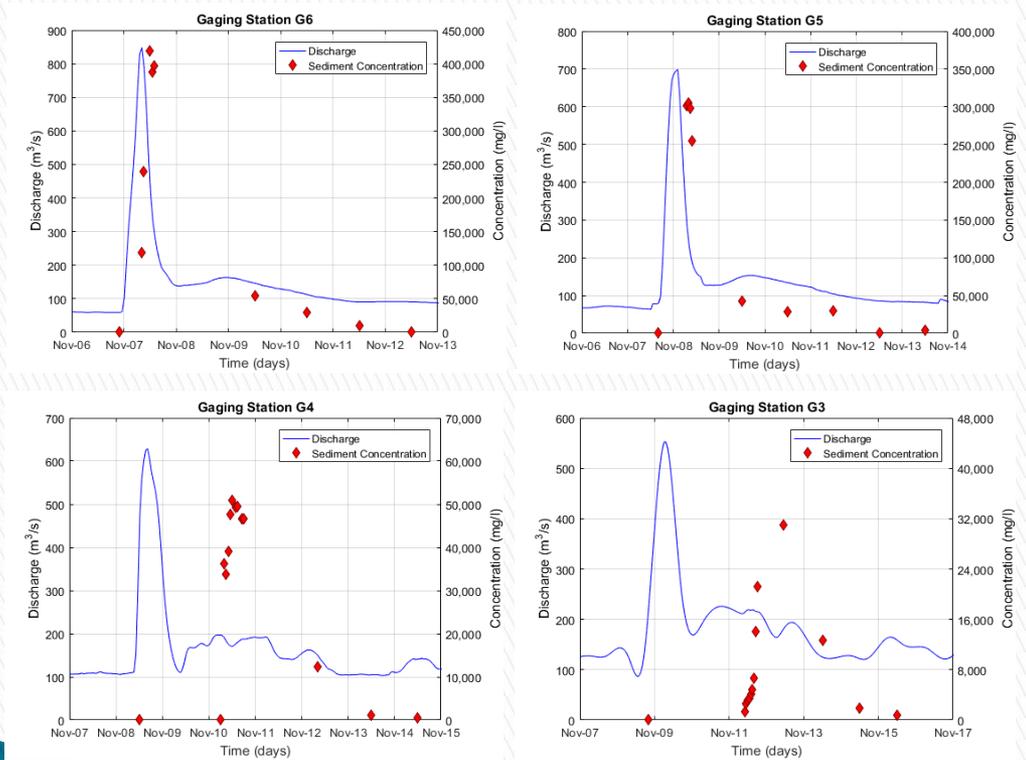
Floodwave Propagation Modeling



from Marcos Palu and Julien ASCE-JHE (2020)

Sediment Concentration Measurements

Observed suspended sediment concentration (CPRM & ANA, 2015)



Sediment Routing NEW Development!

The one-dimensional advection-dispersion equation with settling is applied on the evaluation of transport of suspended load in open channels (Fischer et al., 1979; Julien, 2010).

$$\frac{\partial C}{\partial t} + U \frac{\partial C}{\partial x} = K_d \frac{\partial^2 C}{\partial x^2} - kC$$

C is the concentration;
 U is the flow averaged velocity;
 K_d is the longitudinal dispersion coefficient;
 $k = \omega/h$ is the settling rate.

Analytical solution for a constant spill of finite duration τ is:

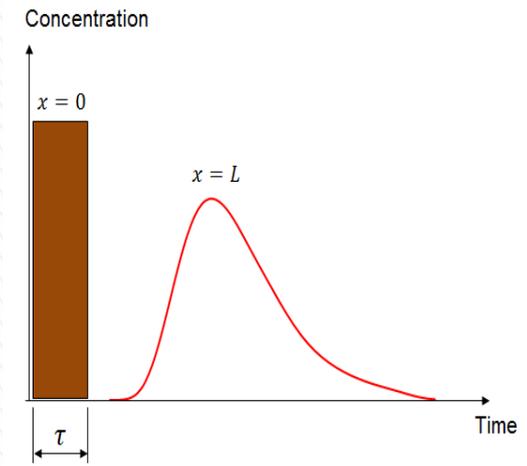
$$C(x, t) = \frac{C_0}{2} \left\{ \begin{aligned} & e^{\frac{Ux}{2K_d}(1-\Gamma)} \left[\operatorname{erfc} \left(\frac{x - Ut\Gamma}{2\sqrt{K_d t}} \right) - \operatorname{erfc} \left(\frac{x - U(t - \tau)\Gamma}{2\sqrt{K_d(t - \tau)}} \right) \right] \\ & + e^{\frac{Ux}{2K_d}(1+\Gamma)} \left[\operatorname{erfc} \left(\frac{x + Ut\Gamma}{2\sqrt{K_d t}} \right) - \operatorname{erfc} \left(\frac{x + U(t - \tau)\Gamma}{2\sqrt{K_d(t - \tau)}} \right) \right] \end{aligned} \right\}$$

Where: $\Gamma = \sqrt{1 + 4\eta}$ and $\eta = \frac{kK_d}{U^2}$

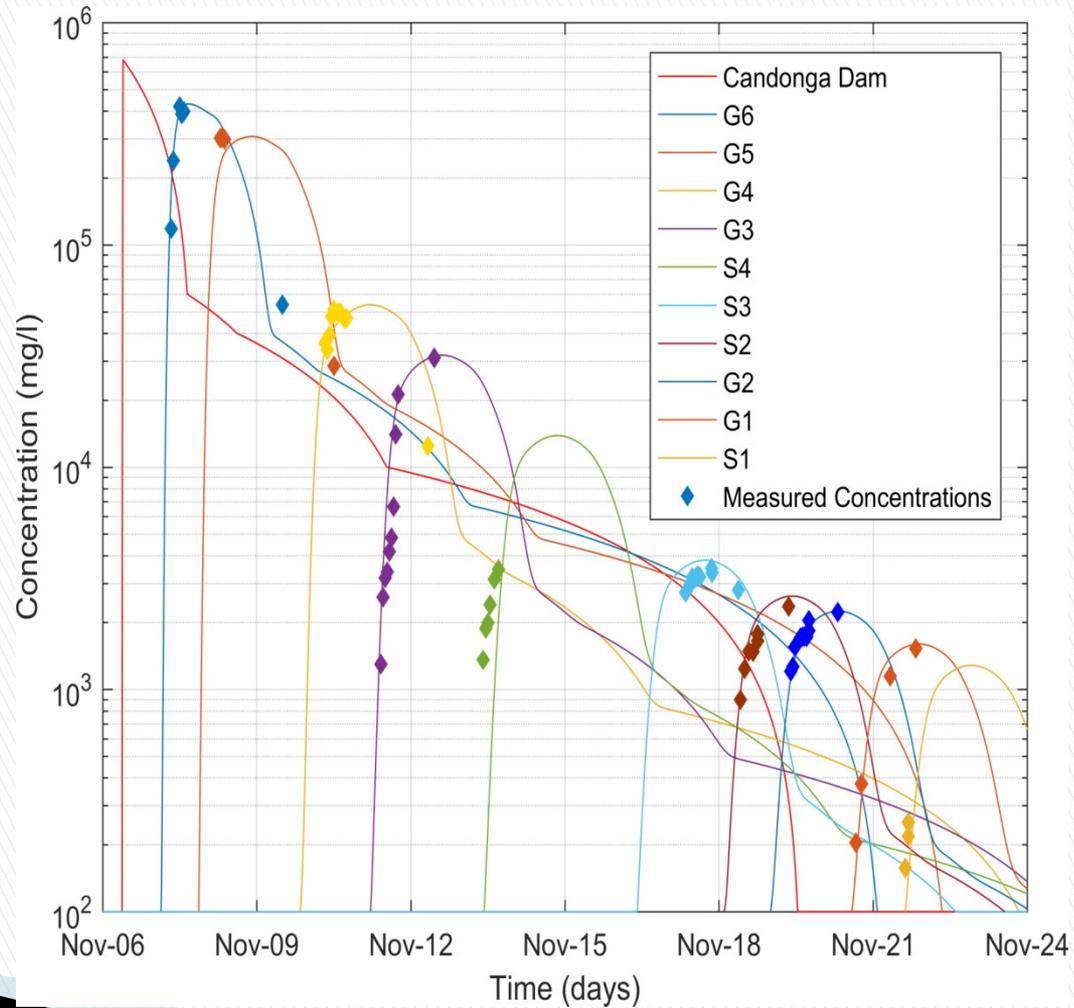
The complementary error function erfc is equal to:

$$\operatorname{erfc}(b) = 1 - \operatorname{erf}(b) = 1 - \frac{2}{\sqrt{\pi}} \int_0^b e^{-\beta^2} d\beta$$

erfc .precise in Xcel



Sediment Concentration Modeling



Summary and Conclusions

1. River Equilibrium

Rivers can reach equilibrium after several years.

2. Aggradation

Aggradation forces out-of-banks rivers and braiding.

3. Degradation below Dams

Degradation causes incision and narrowing with possible impact on structures.

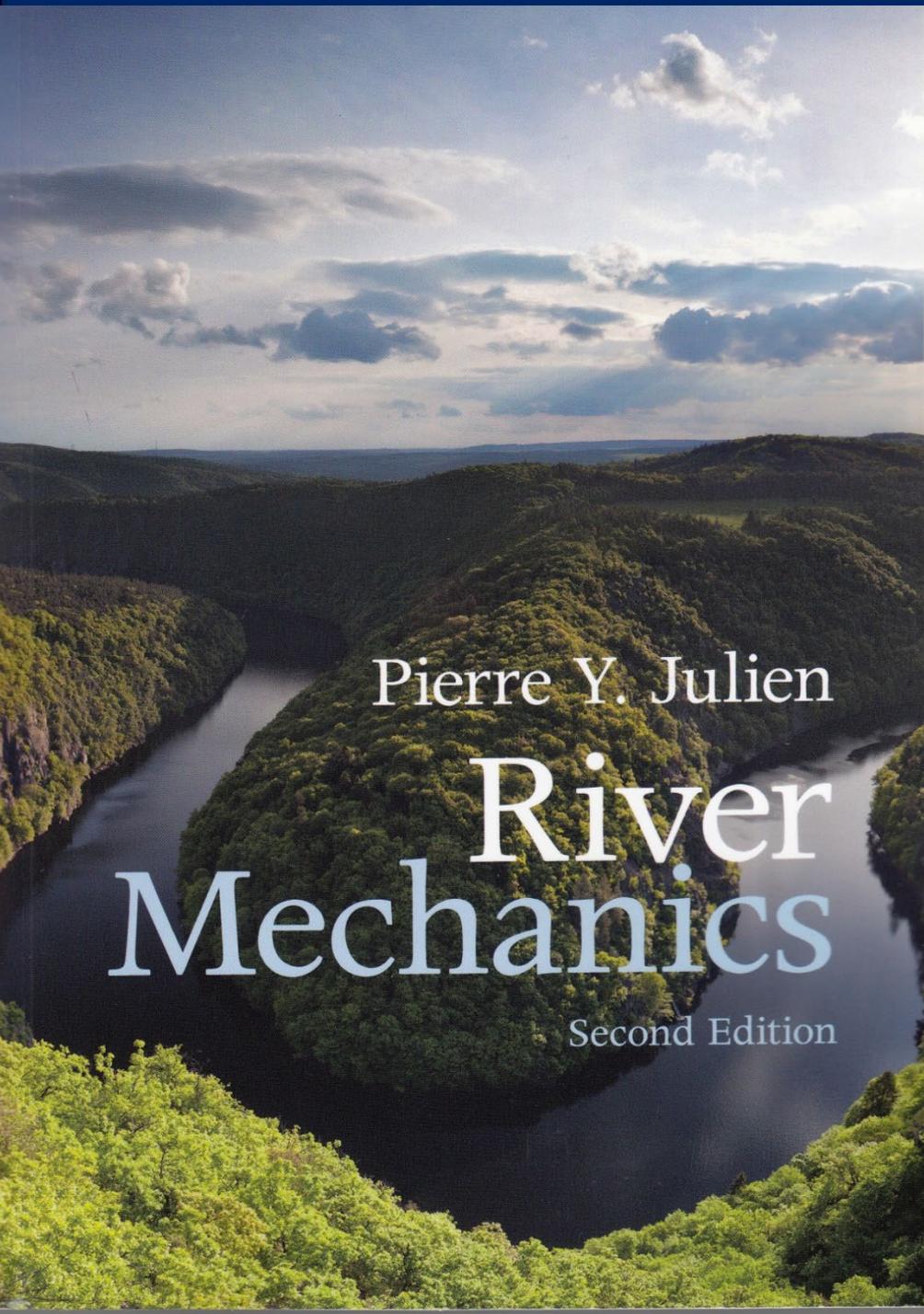
4. Case-study Gupo Bridge

Retrofitting based on stability, not equilibrium.

5. Case-study Dam Break

Numerical modeling of flood and sediment waves.





Thank You!

ACKNOWLEDGMENTS

Dr. Bounthanh Bounvilay, Laos
Dr. Claudio Meier, Chile
Dr. Junke Guo, UNO, USA
Dr. Seema Shah-Fairbank, CalPoly
Dr. Chunyao Yang, HydroTech, USA
Dr. Jimmy O'Brien, FLO, USA
Anna Paris, Maccaferri, USA
Dr. Jaihong Kim, SCSU, USA
Dr. Jose B. Anderson, Brasil
Dr. Jaehoon Kim, KFRI, S. Korea

Pierre Y. Julien

River Mechanics

Second Edition