#### TRANSIENT BEHAVIOUR OF DENSE GAS PLUMES

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#### I INTRODUCTION

The ultimate purpose of this study is to provide basic information on the structure of vapour plumes resulting from LNG spills on land for a realistic range of meteorological variables, source Small scale models of LNG tank-like variables and site features. complexes have been placed in a meteorological wind tunnel capable of simulating the appropriate meteorological conditions. concentrations of dense vapour were determined by sampling concentrations of tracer gas  $(CO_2$ , cooled He-N<sub>2</sub> mixtures, or Freon 12-air Initial measurements utilised mixtures) to simulate the LNG vapour. a series of continuous release rates to interpret the effect of a variable boiloff rate field condition (Meroney et al (1976, 1977) and Neff et al (1976)).

The current program includes measurements of transient boiloff release rates with fast response anemometers and the validation of the modelling criteria.

# II LABORATORY SIMULATION OF CRYOGENIC SPILLS

The reliability of the use of wind tunnel shear layers for modelling atmospheric flows has been demonstrated by several invest-Specific problems associated with the igators (Cermak, 1975). dispersion of cold natural gas plumes have been previously discussed The Froude number is the primary parameter by Meroney et al (1976). which governs plume spread rate, trajectory, plume size and entrainment when gases remain negatively buoyant during their entire traject-Earlier measurements (Neff et al (1976) and Meroney et al (1977)) suggest that heat transfer effects may be small over the significant time scales; hence gas density should be adequately simulated by Visualization of isothermal high molecular weight gas mixtures. similar tests for the range of model scales used (1:130 to 1:666) Concentration results of the indicate a similar plume geometry. different model scales agreed to within the experimental accuracy of Similarly, identical tests also show good approximately ±20%. agreement; hence the Reynolds number must play a minor part in the dense gas dispersion situations considered.

## WIND TUNNEL EXPERIMENT

Scale models (1:200 and 1:400) of two typical LNG storage tanks have been studied in the meteorological wind tunnel for a neutral and stable atmosphere.

Tank facilities considered include a low dike configuration (39  $\mathrm{m}$ diameter tank, 36 m high surrounded by a 6.6 m high dike 93 m by 100 m  $\,$ in area) and high dike configuration (73 m diameter, 39 m high tank surrounded by a concentric 81 m diameter dike 24 m high). examined was a 1:106 scale model of Test 044 from the Capistrano Series supported by the American Gas Association (1974) which involved a spill into a 25 meter diameter by 0.5 meter high dike.

All results presented herein are modelled with pure Carbon dioxide or pre-cooled Helium-Nitrogen mixtures adjusted to simulate boiloff Turbulent diffusion of simulated LNG plumes densities of methane. for the three different LNG tank and dike complexes, two model gas mixtures, two atmospheric stratifications, three scale ratios, and a number of wind speed and boiloff rate combinations were studied. Mean concentration measurements were obtained for as many as 23 different sample points distributed over a ground level zone up to 250 m wide, 50 to 2000 meters long, and in the vertical over a A schematic of the model configuration height of 0 to 100 meters. and the associated concentration measuring equipment is shown in Figure 1.

To obtain an accurate prediction of the extent of hazard associated with the vapourization of LNG, the model should simulate the variable boiloff rate of the gaseous methane characteristic to Typical boiloff curves for the that of the spill configuration. prototype situation along with the actual model gas release for the Capistrano Test 044 are presented in Figure 2. These gas flow rate curves were obtained by use of a programmed cam to close a micrometer needle valve controlling the flow of simulation gas at a predetermined rate.

The transient nature of the boiloff rates simulated necessitated the use of a fast response, temperature compensated concentrat-An aspirated dual film probe was designed for this ion transducer. As noted in Figure 3, dual films operated at different project. current levels permitted compensation for temperature drift, while a flared inlet reduced the noise of pressure fluctuations. Calibration suggests a noise level of 0.1% by volume CO2 and an upper frequency response of 1000 Hz.

#### TEST PROGRAM RESULTS IV

Test results consisted of (1) a qualitative study of the flow field arou. The different tank and dike localities by visual observation of the plume released from the model area; and (2) a quantitative study of gas concentrations produced by the release of a tracer from the model area.

# Continuous Boiloff Release Results

Continuous releases of CO2 made from the high and low tankdike configurations agree well with the earlier Freon-12-N $_2$ simulations performed by Neff et al (1976). The dimensionless concentration coefficient  $XUH_T^2/Q$  scales with non-dimensional down-The dimensionless concentration wind distance  $x/H_T$  (Figure 4). coefficient curves asymptotically approach the slope of those given by the appropriate Pasquill diffusion category for both neutral and No significant differentiation appeared between  ${\rm CO}_{2}$ stable flow. and pre-cooled HeN, simulation gases.

### Variable Boiloff Release Results

Figure 5 displays the dilution time history of the Capistrano Model Test and the field situation superimposed for the typical The time and magnitude of highest test position (320', 0', 0'). concentrations observed at most of the test locations is in good The arrival time of the transient plume at the measurement location is reasonably close. The model does not, however, predict the large and intermittent concentration peaks at late times as observed in the field. Such variations are likely due to gustiness and changes of wind direction recorded for the field case but not present in the wind tunnel.

Transient measurements made downwind of the typical high and low dike configurations reveal that mean concentration measurements made at constant boiloff rates appear to upper bound conditions to the maximum concentrations detected during a transient boiloff situation.

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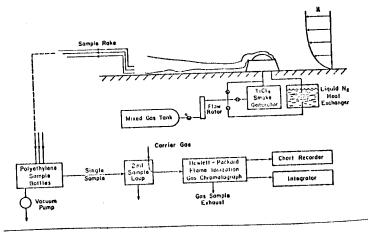


Figure 1: Block Diagram of Gas-Mixture Release System and Mean Concentration Sampling System.

