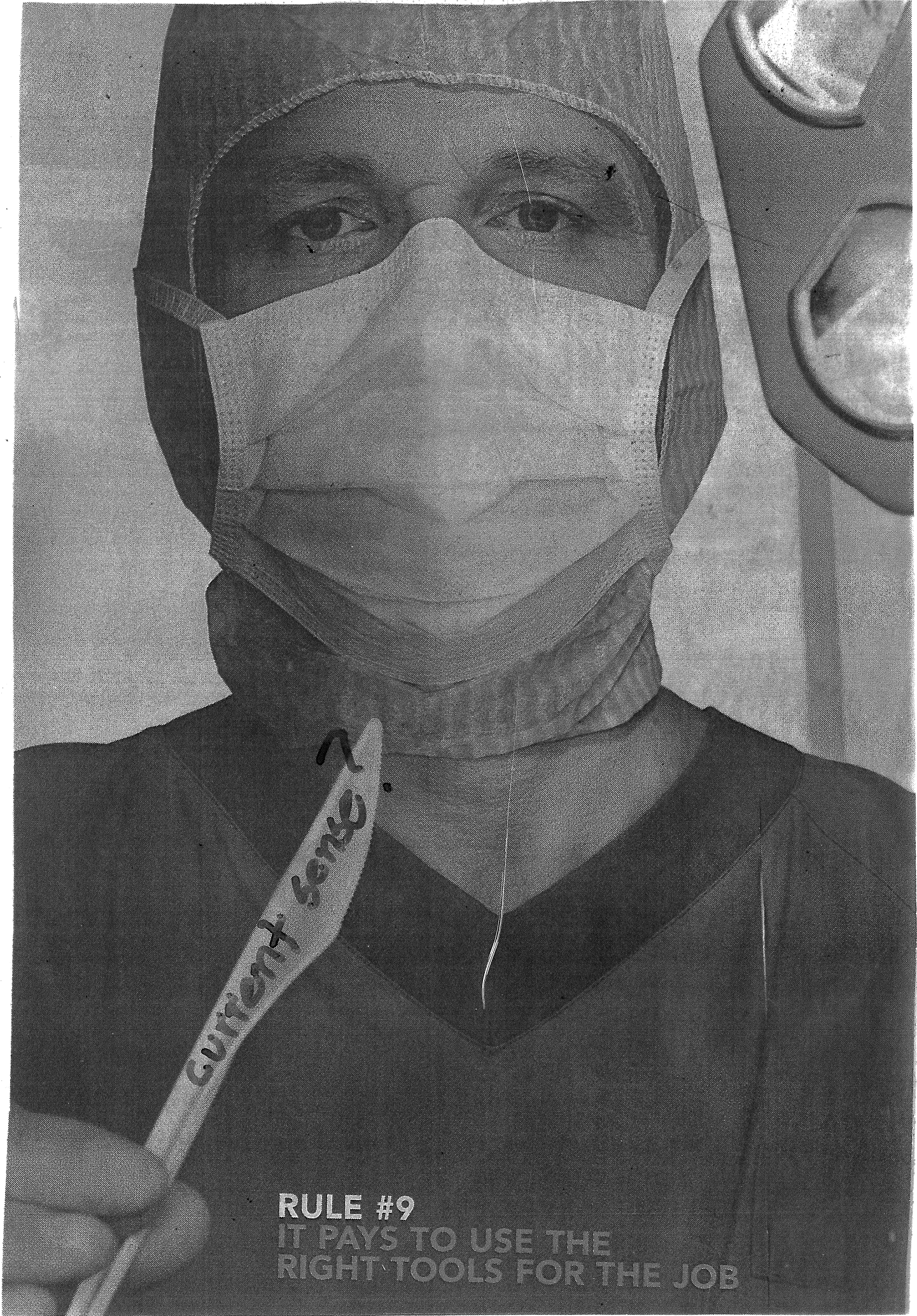


## **Applications:**

- Low-voltage, high-density distributed power systems
- Point-of-load regulation for high-performance DSPs, FPGAs, ASICs and microprocessors
- *Broadband, networking and optical communications infrastructure*
- *Portable computing/notebook PCs*

## **Features:**

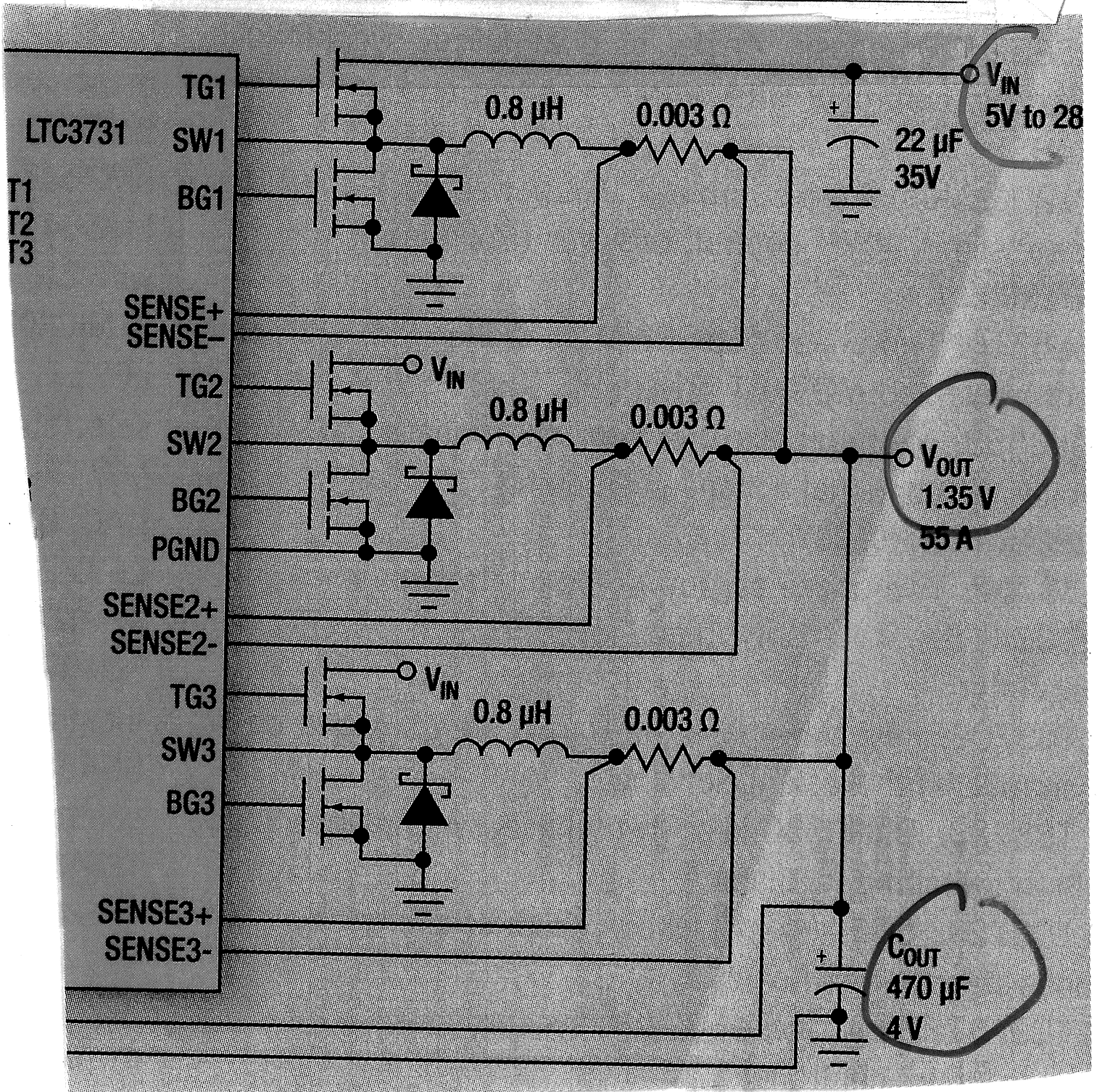
- 3-V to 6-V input
- 30-m $\Omega$ , 12-A peak MOSFET switches for high efficiency at 6-A continuous output
- 0.9-V to 3.3-V adjustable output voltage range with 1.0% initial accuracy; fixed versions available
- *Wide PWM frequency — fixed 350 kHz, 550 kHz or adjustable 280 kHz to 700 kHz*
- *Load protected by peak current limit and thermal shutdown*
- *Complete set of design tools: EVM, software tool and datasheets*
- *TPS5461x starts at \$4.99 per device in quantities of 1,000*



**RULE #9**  
IT PAYS TO USE THE  
RIGHT TOOLS FOR THE JOB



Fig. 1. Linear Technology's LTC3731 is a PolyPhase synchronous step-down switching regulator controller that drives all N-channel external power MOSFET stages in a phase-lockable fixed frequency architecture.



One vendors chip

① Latest  $\uparrow$  \* 5

## The Good Stuff

- ◆ ② Up to 2.5MHz switching frequency
- ◆ >4MHz sync capability
- ◆ Minimum pulse width <25ns
- ◆ Fast current limit: <35ns
- ◆ Built-in 180V start-up circuitry
- ◆ <1mA quiescent current
- ◆ Built-in MOSFET driver: 3 $\Omega$  sink, 7 $\Omega$  source
- ◆ Programmable undervoltage lockout
- ◆ Programmable soft start
- ◆ Resistor programmable current sense threshold
- ◆ Primary power limit for fault conditions
- ◆ Low current <5 $\mu$ A shutdown mode
- ◆ 50% duty cycle limit with MIC9130
- ◆ 75% duty cycle limit with MIC9131
- ◆ 16-pin SOIC and QSOP packages

③ \$5 / chip



$$1 \leq K_{ON} \leq 100 \text{ m}\Omega$$

$V_{FET(ON)} = I R_{ON}$   
if too high use  $V_{CE}$  (bipolar)  
 $\approx 0.1V$

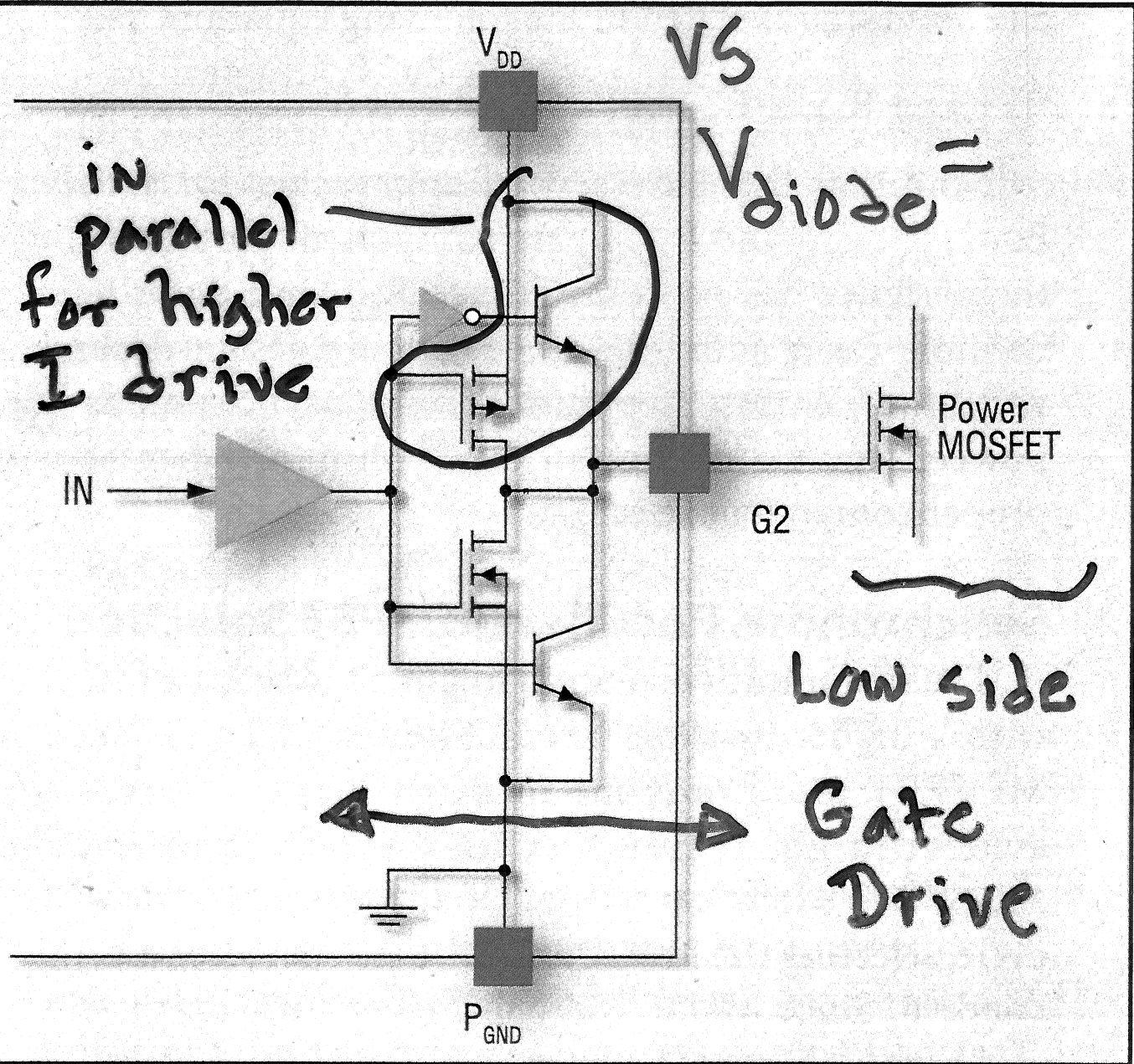
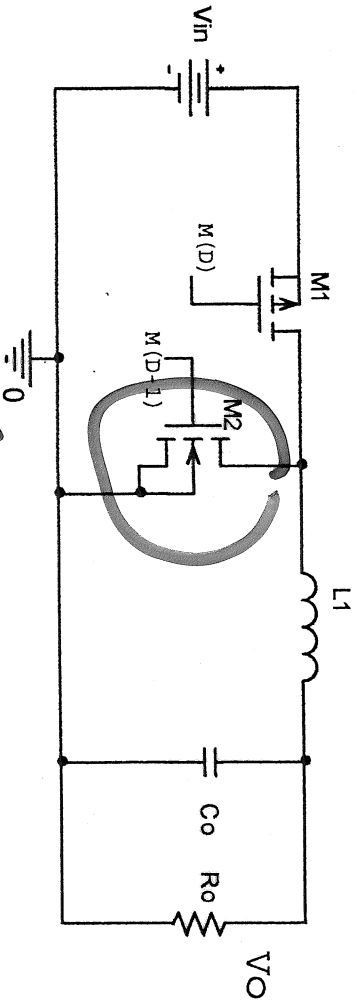


Fig. 3. The TrueDrive gate-drive architecture (low-side only) from Texas Instruments places bipolar and MOS transistors in parallel to deliver the rated drive current while lowering the pull-down impedance for better  $dv/dt$  immunity.

Replace diode with M<sub>2</sub>  
to reduce switch losses

## Synchronous Rectification



Goal:

$$P_{M2\_ON} = R_{M2\_ON} \int_0^2 I_{out}^2 (1-D) dt < P_{diode\_conduction} = V_{diode} * I_{out} * (1-D)$$

-There are other switching losses in M2

-Additional Circuitry Needed in Controller (\$\$)

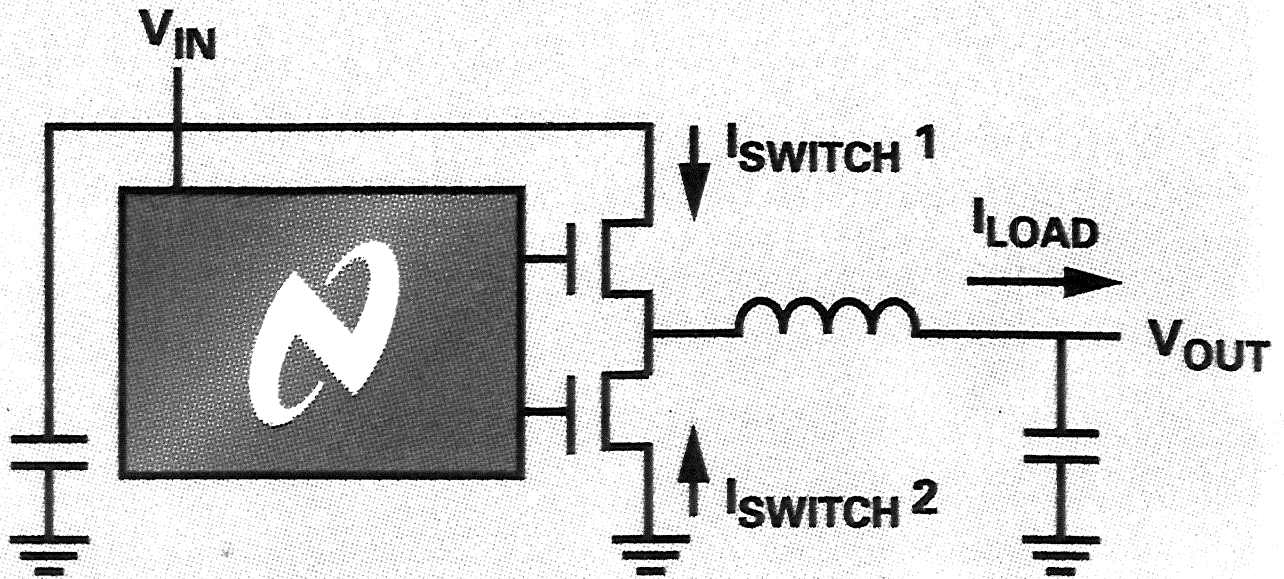
V<sub>on</sub> diode  
say 1/2 V

V<sub>on</sub> FET  
50 mV

⇒ 10 times  
lower



# Synchronous buck



**Function:** Step-down ( $V_{OUT} < V_{IN}$ )

**When to use:** When high efficiency is required with high-output current ( $> 5A$ ) or low duty cycles ( $V_{IN} > 5 \times V_{OUT}$  and/or  $I_{OUT} < 0.5A$ )

**Characteristics:** A second switch replaces the diode in the basic buck topology, reducing losses in the conditions mentioned above

**Devices to use:** Any "synchronous rectification" buck integrated regulator or controller

## Figure 2: Step-down configurations

Cost of FET Drives ?  
vs  
"Smart" diode

# Synchronous Rectification in High-Performance Power Converter Design

— By Robert Selders, Jr., Applications Engineer

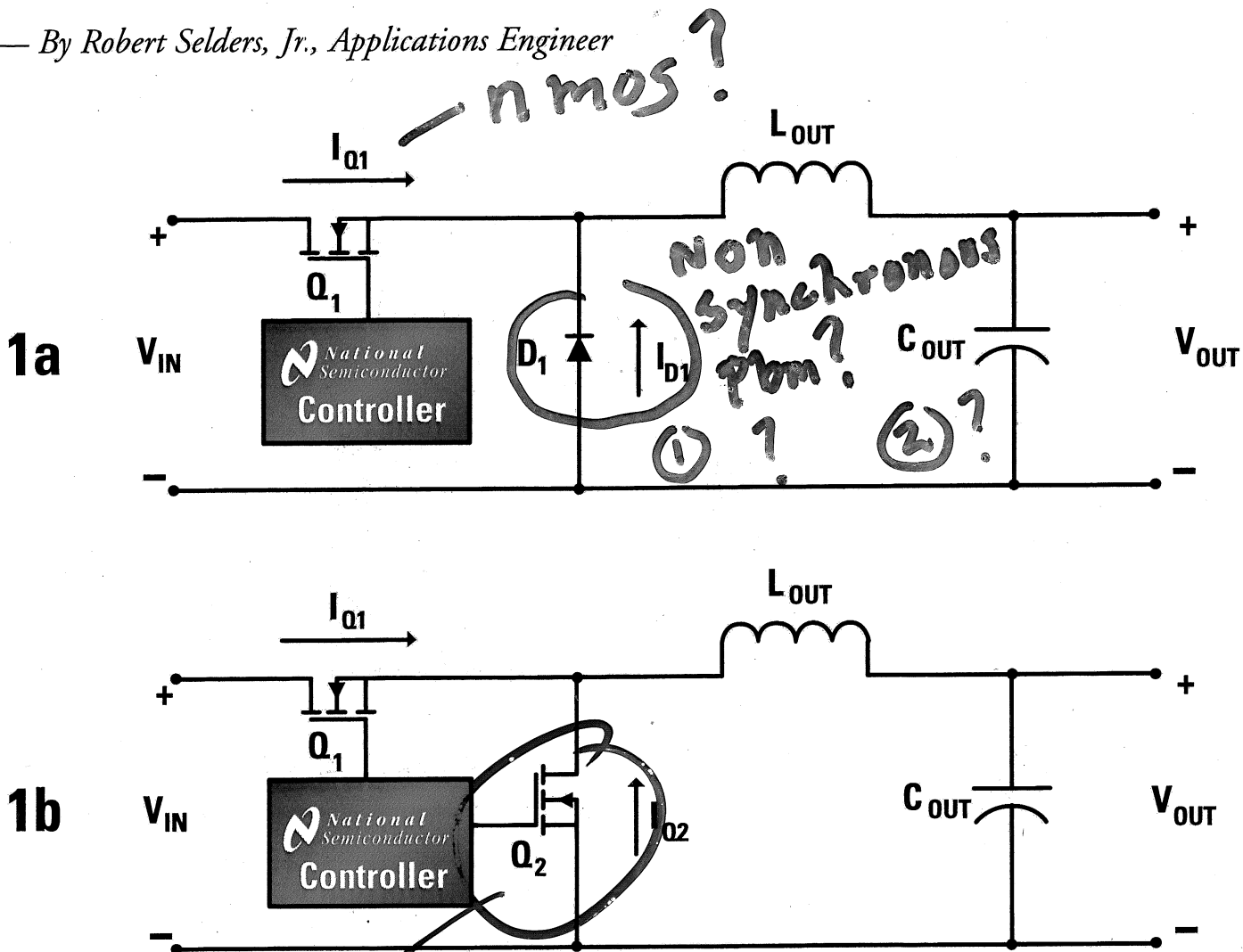


Figure 1. (a) Non-synchronous and (b) Synchronous Buck Converters

replace  $(V_{ON})$  power diode

- ① avoid shoot through from  $Q_{rr}$
- ② Always CCM (no need ch5)
- ③  $V_{ON} = I * R_{DS(on)}$  (parallel FETS)
- ④ Need 100A  $1m\Omega \rightarrow 0.1V$