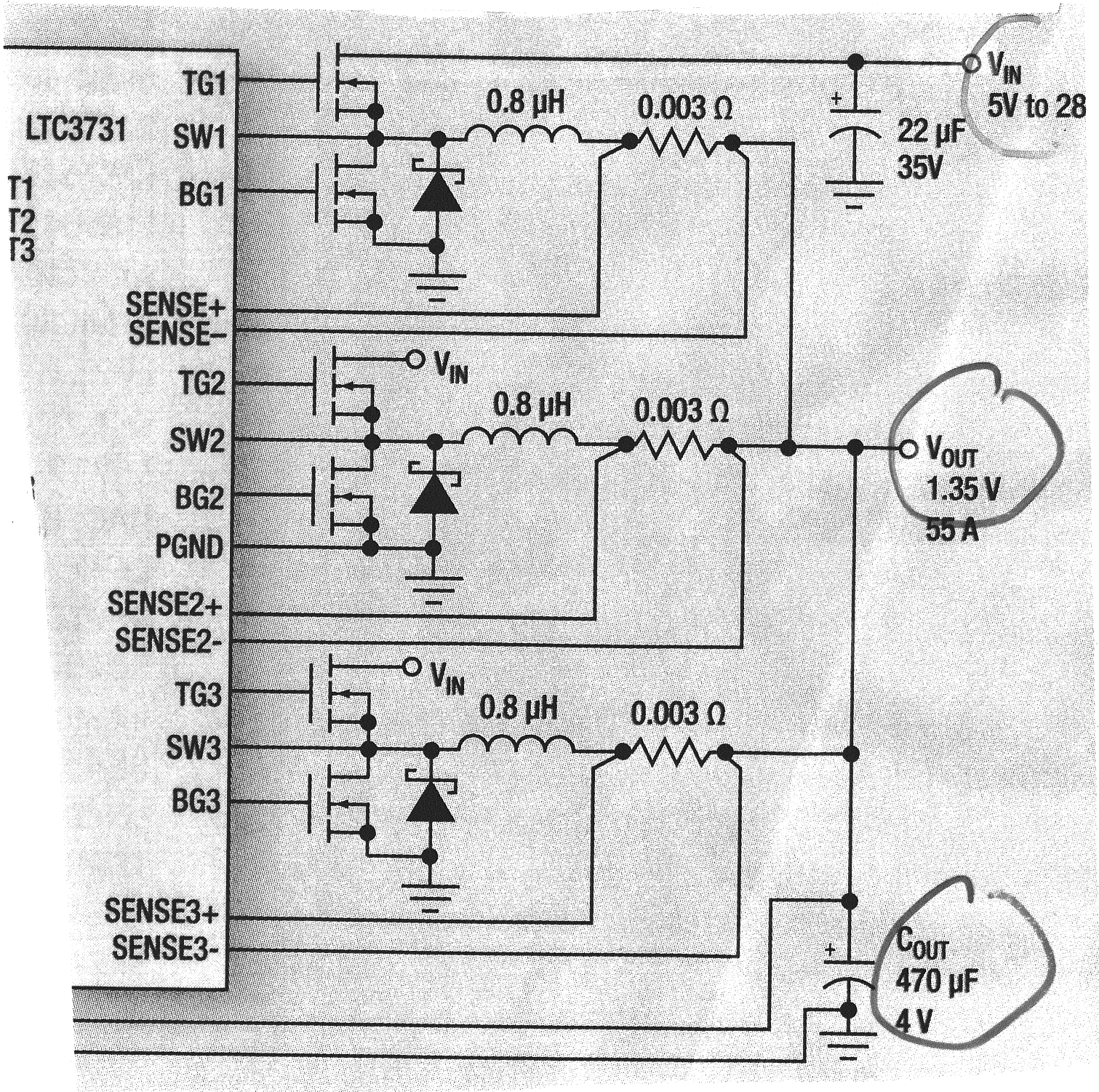
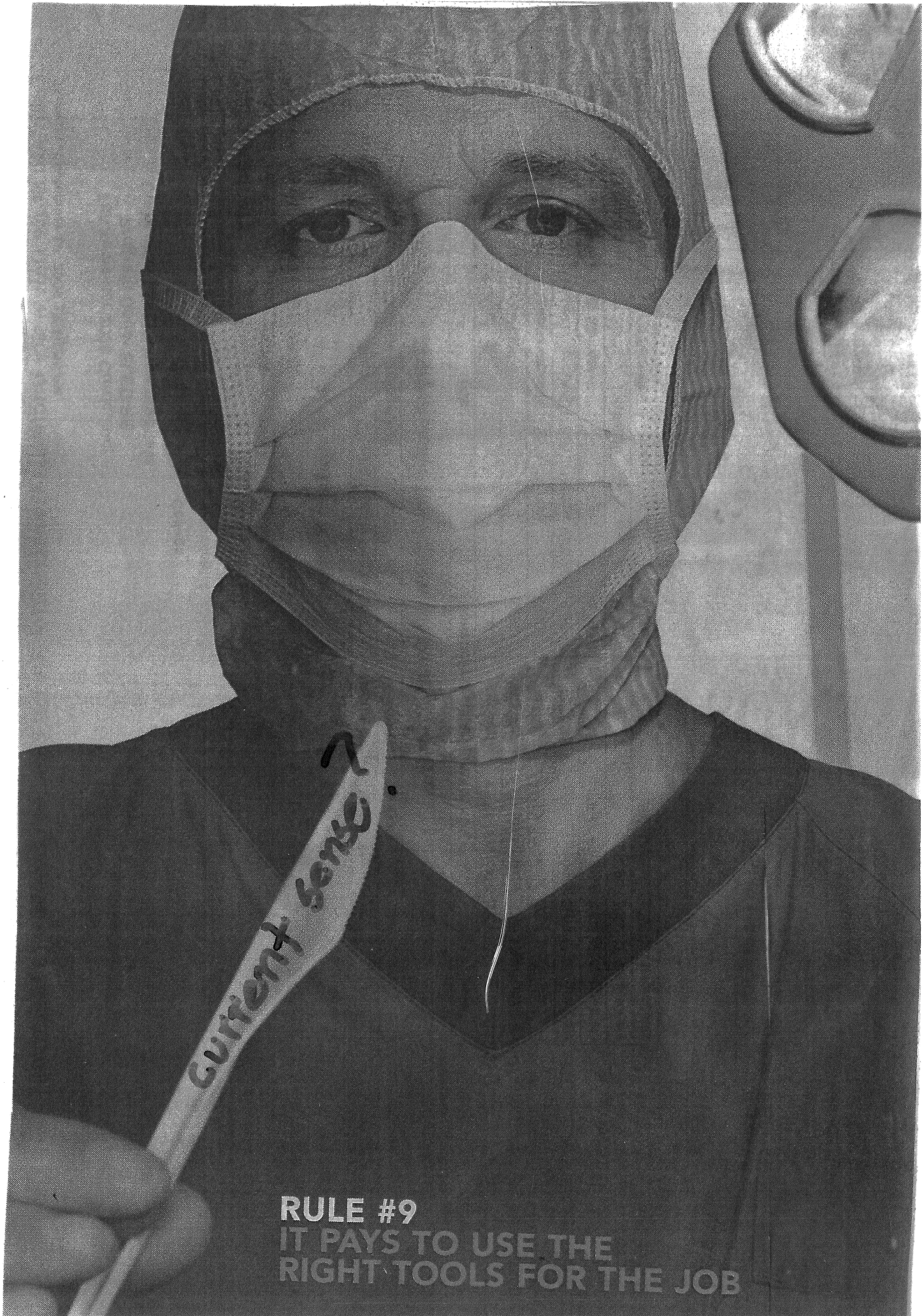


Fig. 1. Linear Technology's LTC3731 is a PolyPhase synchronous step-down

in switching regulator controller that drives all N-channel external power MOSFET s+
in a phase-lockable fixed frequency architecture.



One vendors chip



RULE #9
IT PAYS TO USE THE
RIGHT TOOLS FOR THE JOB

Applications:

- Low-voltage, high-density distributed power systems
- Point-of-load regulation for high-performance DSPs, FPGAs, ASICs and microprocessors
- Broadband, networking and optical communications infrastructure
- Portable computing/notebook PCs

Features:

- 3-V to 6-V input
- 30-m Ω , 12-A peak MOSFET switches for high efficiency at 6-A continuous output
- 0.9-V to 3.3-V adjustable output voltage range with 1.0% initial accuracy, fixed versions available
- Wide PWM frequency — fixed 350 kHz, 550 kHz or adjustable 280 kHz to 700 kHz
- Load protected by peak current limit and thermal shutdown
- Complete set of design tools: EVM, software tool and datasheets
- TPS5461x starts at \$4.99 per device in quantities of 1,000

Synchronous Rectification in High-Performance Power Converter Design

— By Robert Selders, Jr., Applications Engineer

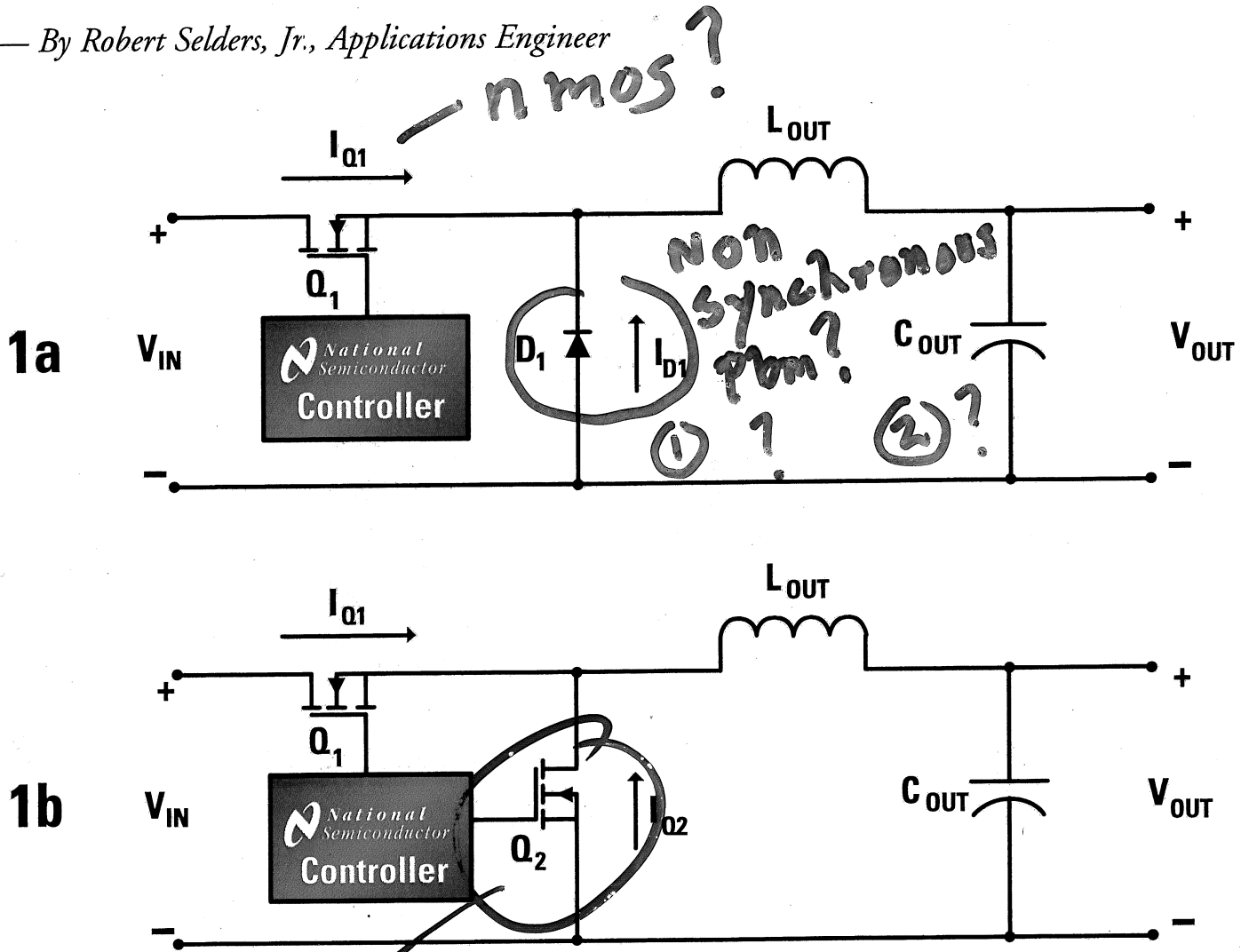
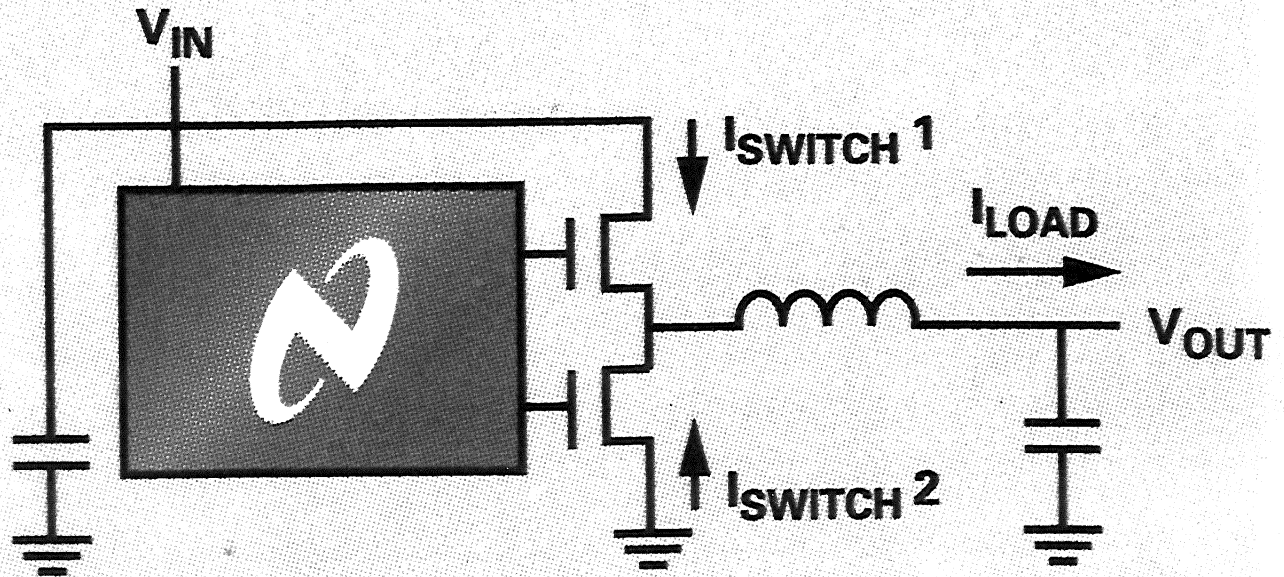


Figure 1. (a) Non-synchronous and (b) Synchronous Buck Converters

replace (V_{ON}) power diode

- ① avoid shoot through from Q_{rr}
- ② Always CCM (no need ch5)
- ③ $V_{ON} = I * R_{ON}$ (parallel FETS)
- ④ Need 100A $1m\Omega \rightarrow 0.1V$

Synchronous buck



Function: Step-down ($V_{OUT} < V_{IN}$)

When to use: When high efficiency is required with high-output current ($> 5A$) or low duty cycles ($V_{IN} > 5 \times V_{OUT}$ and/or $I_{OUT} < 0.5A$)

Characteristics: A second switch replaces the diode in the basic buck topology, reducing losses in the conditions mentioned above

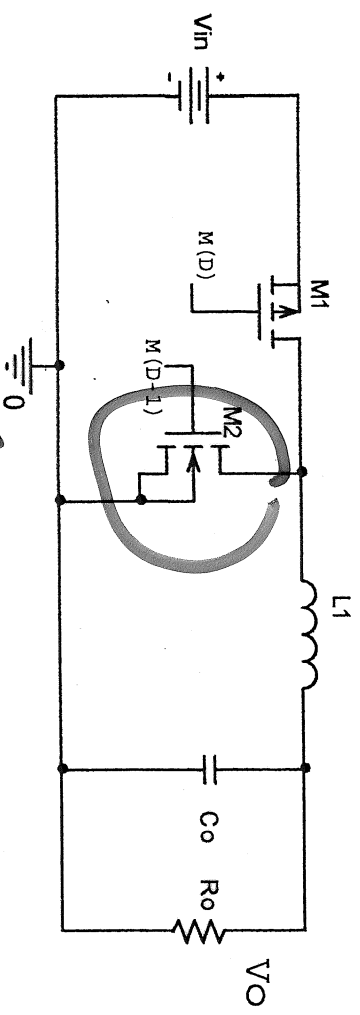
Devices to use: Any "synchronous rectification" buck integrated regulator or controller

Figure 2: Step-down configurations

Cost of FET Drives?
vs
"Smart" diode

Replace diode with M2
to reduce switch losses

Synchronous Rectification



Goal:

$$P_{M2_ON} = R_{M2_ON} \int_0^T I_{out}^2 (1-D)^2 dt < P_{diode_conduction} = V_{diode} * I_{out} (1-D)$$

- There are other switching losses in M2
- Additional Circuitry Needed in Controller (\$\$)

V_{on} diode
say 1/2 V

V_{on} FET
50 mV

⇒ 10 times
lower

$$1 \leq R_{on} \leq 100 \text{ m}\Omega$$

$V_{FET(ON)} = I R_{on}$
if too high use V_{CE} (bipolar)
 $\sim 0.1V$

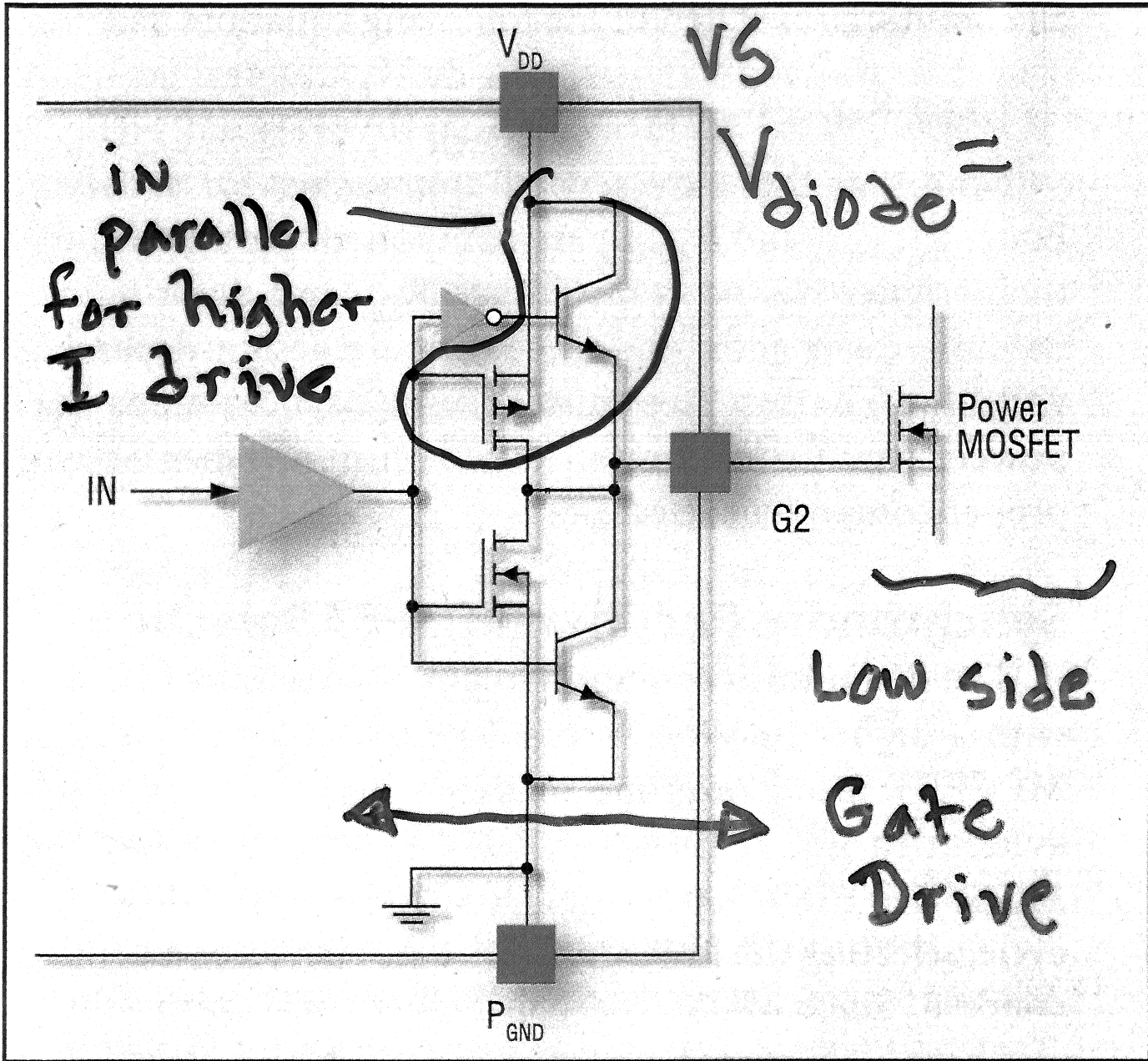


Fig. 3. The TrueDrive gate-drive architecture (low-side only) from Texas Instruments places bipolar and MOS transistors in parallel to deliver the rated drive current while lowering the pull-down impedance for better dv/dt immunity.

① Latest $f \uparrow * 5$

The Good Stuff

- ◆ ② Up to 2.5MHz switching frequency
- ◆ >4MHz sync capability
- ◆ Minimum pulse width <25ns
- ◆ Fast current limit: <35ns
- ◆ Built-in 180V start-up circuitry
- ◆ <1mA quiescent current
- ◆ Built-in MOSFET driver: 3 Ω sink, 7 Ω source
- ◆ Programmable undervoltage lockout
- ◆ Programmable soft start
- ◆ Resistor programmable current sense threshold
- ◆ Primary power limit for fault conditions
- ◆ Low current <5 μ A shutdown mode
- ◆ 50% duty cycle limit with MIC9130
- ◆ 75% duty cycle limit with MIC9131
- ◆ 16-pin SOIC and QSOP packages

③ 45 / chip