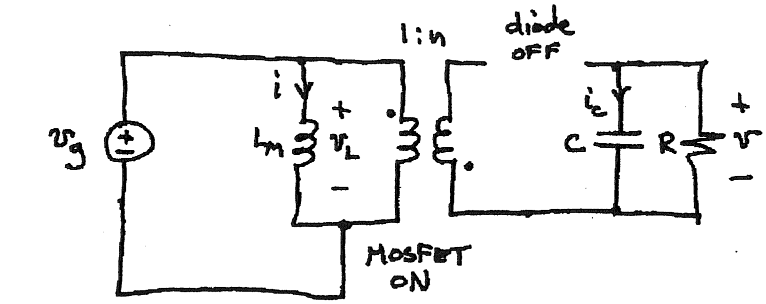
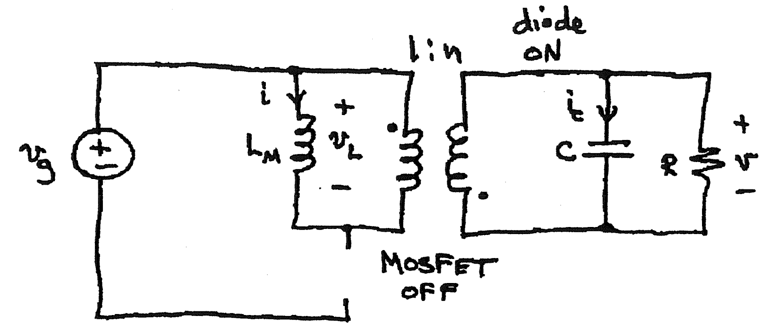
CL3 L12
UL14

Problem 6.2

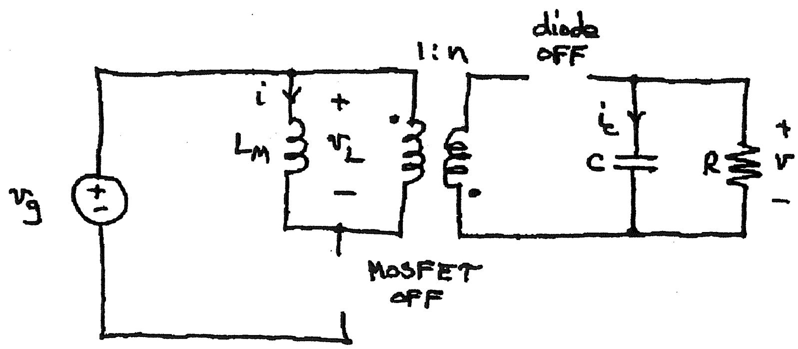
a)



interval
1



interval
2



interval
3
$i = 0$

b) From the text, the steady-state solution of this converter in CCM is

$$V = n \frac{D}{1-D} V_g \qquad I = \frac{nV}{(1-D)R}$$

The inductor current ripple (in the magnetizing current, referred to primary side) is

$$\Delta i = \frac{V_g D T_s}{2 L_M}$$

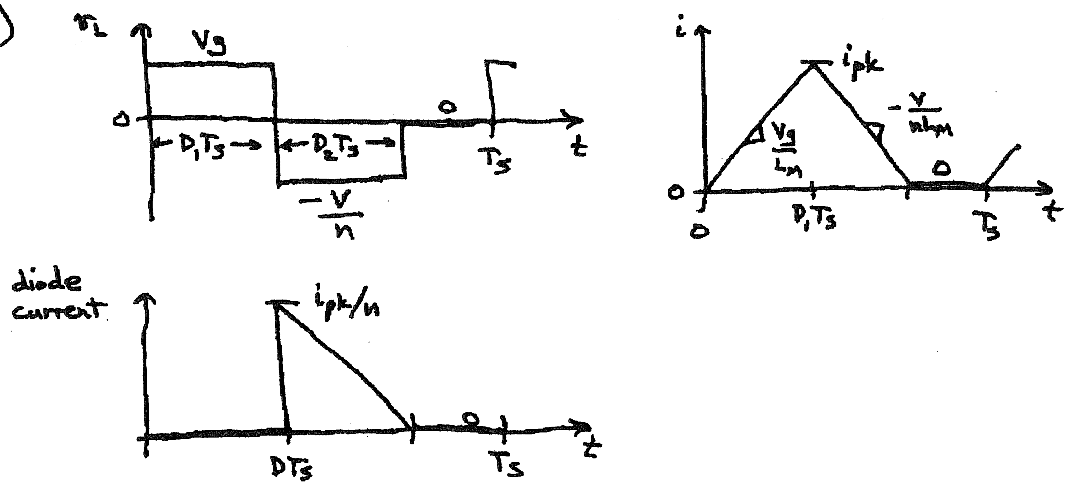
The converter operates in DCM when $\Delta i > I$, or

$$\frac{V_g D T_s}{2 L_M} > \frac{nV}{(1-D)R} \qquad \text{with } V = V_g\, n \frac{D}{(1-D)}$$

$$\Rightarrow \qquad (1-D)^2 > \frac{2 L_M n^2}{R T_s}$$

which resembles the result for the buck-boost listed in Chapter 5. The factor of n^2 occurs because L_M is referred to the primary, but R is connected to the secondary side.

c)



Inductor volt-second balance: $D_1 V_g - D_2 \frac{V}{n} = 0$

Capacitor charge balance: $\frac{1}{2} D_2 \frac{i_{pk}}{n} = \frac{V}{R}$

with $i_{pk} = \frac{V_g D_1 T_s}{L_M}$

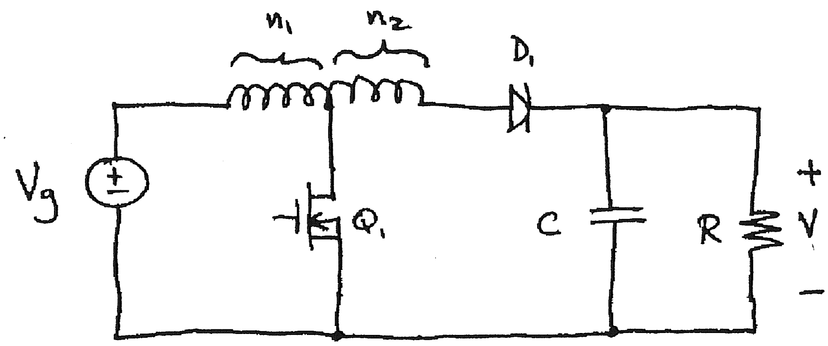
<u>Solve:</u> $V = V_g \, n \frac{D_1}{\sqrt{K}}$ where $K = \frac{2 n^2 L_M}{R T_s}$

and $D_2 = \sqrt{K}$

Tutorial

Solution to Problem 6.1

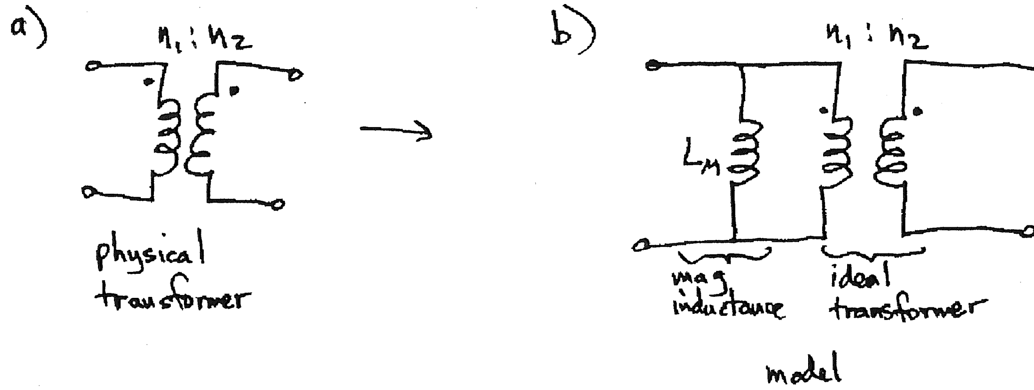
Analysis of tapped-inductor boost converter



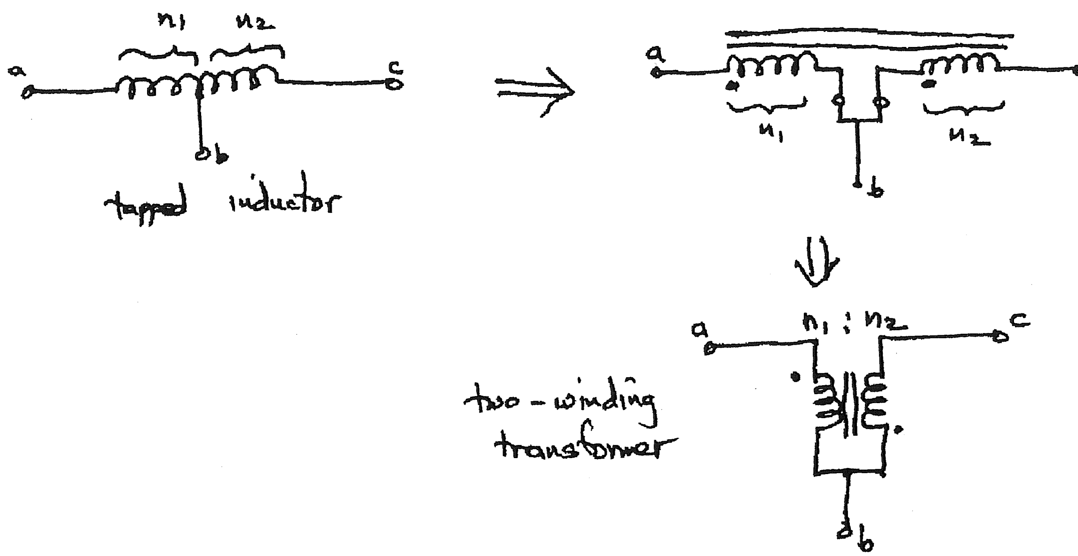
Inductance of entire (n_1+n_2) turn inductor is L

a) Sketch an equivalent circuit model for the tapped inductor, which includes an ideal transformer and a magnetizing inductance.

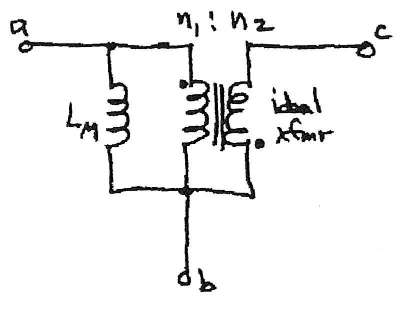
The equivalent circuit model of Fig. 6.17:



The tapped inductor can be viewed as a two-winding transformer:



Use two-winding transformer model:

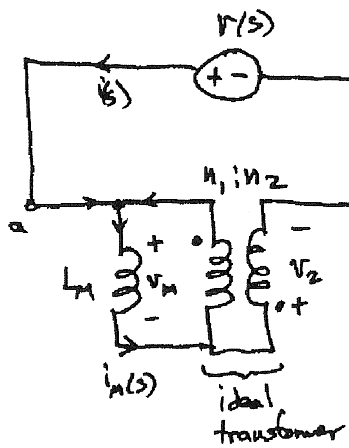


What is the value of L_M?

We are given that the inductance of the entire (n_1+n_2) turn winding is L. So we should choose the value of L_M such that the inductance between terminals a and c, with terminal b open, is L.

Measurement of inductance between terminals a and c:

inject ac voltage v, measure current i, Impedance is $Z(s) = sL = \frac{v(s)}{i(s)}$



- current in n_2 winding is $i(s)$, going into dot

⇒ current in n_1 winding is $\frac{n_2}{n_1} i(s)$, coming out of dot

⇒ node equation for magnetizing current $i_M(s)$:

$$i_M(s) = i(s) + \frac{n_2}{n_1} i(s) = \frac{n_1+n_2}{n_1} i(s)$$

⇒ voltage across inductor is

$$v_M(s) = sL_M i_M(s) = sL_M \frac{n_1+n_2}{n_1} i(s)$$

⇒ voltage across n_2 winding (positive at dot) is $v_2 = \frac{n_2}{n_1} v_M(s) = \frac{n_2(n_1+n_2)}{n_1^2} sL_M i(s)$

⇒ voltage $v(s)$ is

$$v(s) = v_M(s) + v_2(s) = sL_M i(s) \left(\frac{n_1+n_2}{n_1} + \frac{n_2(n_1+n_2)}{n_1^2} \right)$$

$$= s\left(\frac{n_1+n_2}{n_1}\right)^2 L_M \, i(s)$$

So the inductance between terminals a and c is

$$L = \left(\frac{n_1+n_2}{n_1}\right)^2 L_M$$

$$\Rightarrow \quad L_M = \left(\frac{n_1}{n_1+n_2}\right)^2 L$$

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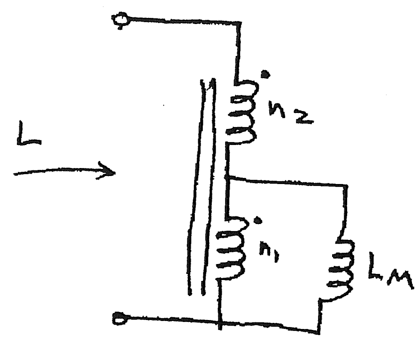
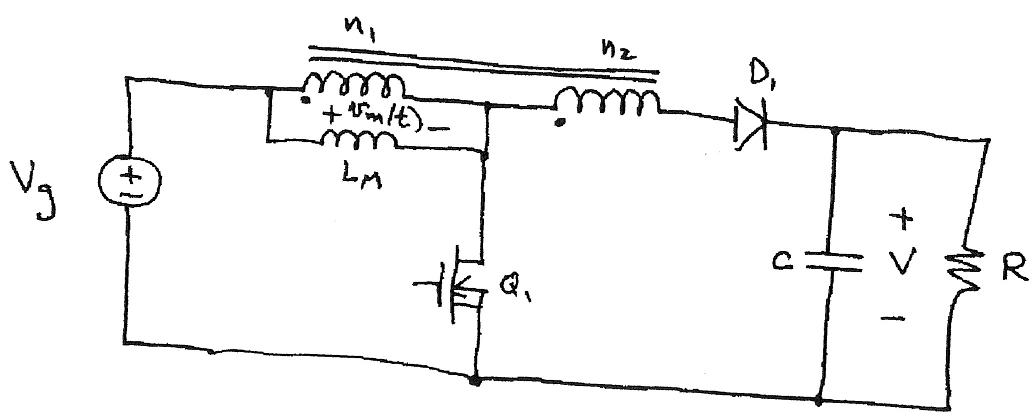
an easier way: reflect L_M through auto transformer



$$L = \left(\frac{n_1+n_2}{n_1}\right)^2 L_M$$

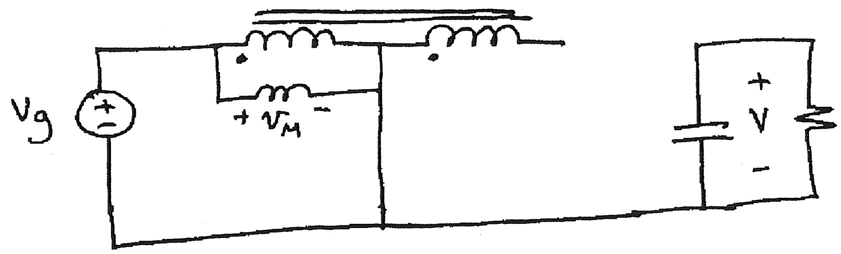
So the converter circuit becomes



b) Determine an analytical expression for $M(D) = \frac{V}{V_g}$ in CCM, no losses.

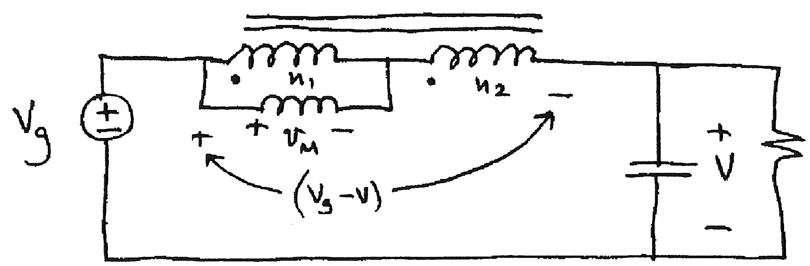
Apply volt-second balance to L_M

$0 < t < DT_s$ Q_1 on, D_1 off

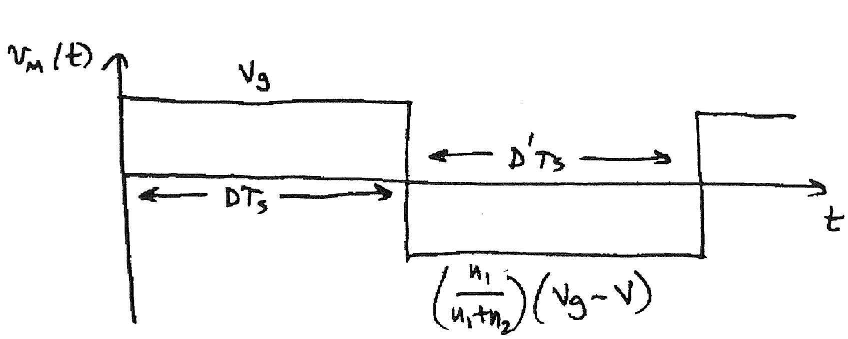


$$v_M = V_g$$

$DT_s < t < T_s$ Q_1 off, D_1 on



$$v_M = \frac{n_1}{n_1 + n_2}(V_g - V)$$



$$\langle v_M \rangle = 0 = D V_g + D'\left(\frac{n_1}{n_1 + n_2}\right)(V_g - V)$$

Solve for V:

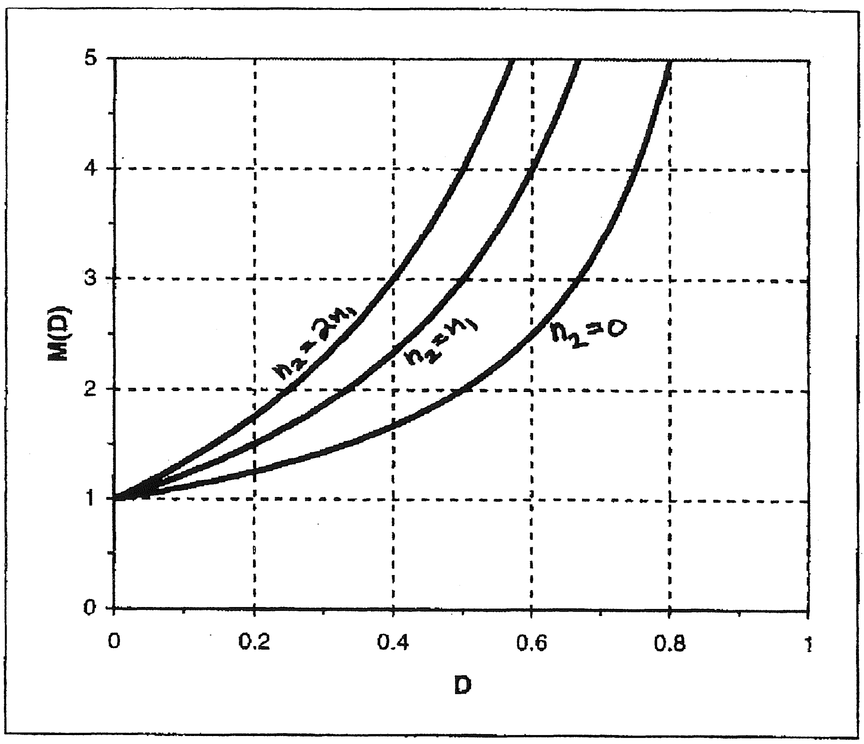
$$V D'\left(\frac{n_1}{n_1+n_2}\right) = D V_g + D' V_g \frac{n_1}{n_1+n_2}$$

$$\Rightarrow \frac{V}{V_g} = \frac{D + D'\left(\frac{n_1}{n_1+n_2}\right)}{D'\left(\frac{n_1}{n_1+n_2}\right)} = \frac{1}{D'} \cdot \left[D \frac{n_1+n_2}{n_1} + D' \right]$$

$$M(D) = \left(\frac{1}{D'}\right)\left(1 + \frac{n_2}{n_1} D\right)$$

which differs from the conventional untapped ($n_2 = 0$) boost $M(D)$ by a factor of $\left(1 + \frac{n_2}{n_1} D\right)$.

c)



Tapped case yields increased output voltage