

Experiments on stratification of heterogeneous sand mixtures

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Key words. – Stratification, Sediment mixtures, Lamination.

Abstract. – Superposed strata in sedimentary rocks are believed to have been formed by successive layers of sediments deposited periodically with interruptions of sedimentation. This experimental study examines possible stratification of heterogeneous sand mixtures under continuous (non-periodic and non-interrupted) sedimentation. The three primary aspects of stratification are considered: lamination, graded-beds, and joints. (1) Experiments on segregation of eleven heterogeneous mixtures of sand size quartz, limestone and coal demonstrate that through lateral motion of a sand mixture, the fine particles fall between the interstices of the rolling coarse particles. Coarse particles gradually roll on top of fines and microscale sorting is obtained. Microscale segregation similar to lamination is observed on plane surfaces, as well as under continuous settling in columns filled with either air or water. (2) The formation of graded-beds is examined in a laboratory flume under steady flow and a continuous supply of heterogeneous sand particles. Under steady uniform flow and plane bed with sediment motion, the coarse particles of the mixture roll on a laminated bed of mostly fine sand particles. In non-uniform flow, the velocity decrease caused by a tailgate induces the formation of a stratum of coarse particles propagating in the downstream direction. On top of this cross-stratified bed, fine particles settle through the moving bed layer of rolling coarse sand particles and form a near horizontally laminated topset stratum of finer particles. Over time, a thick stratum of coarse particles thus progresses downstream between two strata of laminated fine particles, continuously prograding upward and downstream. (3) Laboratory experiments on the desiccation of natural sands also show preferential fracturing, or joints, of crusty deposits at the interface between strata of coarse and fine particles.

Rather than successive sedimentary layers, these experiments demonstrate that stratification under a continuous supply of heterogeneous sand particles results from: segregation for lamination, non-uniform flow for graded-beds, and desiccation for joints. Superposed strata are not necessarily identical to successive layers.

Expériences sur la stratification de mélanges sableux hétérogranulaires

Mots-clés. – Stratification, Mélanges hétérogranulaires, Lamination.

Résumé. – Les strates dans les roches sédimentaires sont généralement assimilées à des couches sédimentaires successives déposées avec arrêt périodique de la sédimentation. Cette étude expérimentale examine la possibilité de stratification de mélanges de sables hétérogranulaires en sédimentation continue (sans interruption et périodicité de la sédimentation). Les trois aspects principaux de la stratification sont considérés : lamination, lits stratifiés, et joints. (1) Les expériences sur la ségrégation de onze mélanges hétérogranulaires de quartz, calcaires et charbons démontrent que lors du mouvement latéral de sables hétérogènes, les particules fines tombent dans les interstices entre particules grossières en mouvement. Les particules grossières roulent sur les fines et la ségrégation est obtenue à l'échelle microscopique. Cette ségrégation microscopique similaire à la lamination est observée sur des surfaces planes, tout comme en sédimentation continue en colonnes d'air ou d'eau. (2) La formation de lits stratifiés est examinée au laboratoire dans un canal avec écoulement permanent et alimentation continue de particules hétérogranulaires. A partir d'un écoulement permanent et uniforme sur un lit hétérogranulaire plan, les grosses particules du mélange roulent sur la surface d'un dépôt laminé de particules fines. En écoulement permanent non-uniforme, la diminution de vitesse d'écoulement provoquée par l'insertion d'un seuil à l'aval du canal induit la formation d'une strate deltaïque de particules grossières en progression vers l'aval. Une strate laminée de particules fines se forme simultanément au dessus du lit stratifié obliquement. Une strate de particules grossières en progression vers l'aval se forme donc continuellement entre deux strates laminées de particules fines en progradation verticale et vers l'aval. (3) Les expériences en laboratoire sur la dessiccation de sables naturels montre des fractures préférentielles, ou joints, à l'interface des strates de grosses et de fines particules dans les dépôts séchés à l'air.

Ces expériences démontrent que la stratification de mélanges sableux sous alimentation continue en sédiments hétérogranulaires résulte de : la ségrégation produisant la lamination, l'écoulement non-uniforme produisant les lits stratifiés, et la dessiccation produisant les joints. Les strates superposées ne sont donc pas nécessairement le résultat de couches sédimentaires successives.

I. – INTRODUCTION

As stratification usually describes layering in rocks, a single layer of homogeneous lithology is referred to as a stratum. Stratification has often been associated with intermittent sedimentary layers. Superposed strata in sedimentary rocks are believed to have been formed by successive layers of sediment deposited periodically with interruptions of sedimentation.

McKee *et al.* [1967] reported on the sedimentary structure, texture and shape of the massive sand deposits developed during the Bijou Creek flood in July 1965. Stratified sand deposits up to 12 feet (3.8 m) in thickness

formed within a few hours. The violent flood deposited superposed thick horizontal strata of fine and coarse sands, characteristic of the upper flow regime with internal layering in the form of microscale lamination. Is stratification resulting from successive intermittent layers in such rapid and quite continuous sedimentary flow? The primary features of interest in the Bijou Creek sand deposits are : (1) lamination seen as a microscale sorting of coarse and fine particles at a vertical scale not exceeding 10 mm; (2) graded-beds or strata of coarse and fine particles of thickness exceeding 10 mm; and (3) horizontal joints between sediment deposits.

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TABL. I. – Summary of hypotheses explaining the origin of horizontal lamination.

TABL. I. – *Synthèse des hypothèses expliquant l'origine des laminae horizontales.*

Reference	Summary of Hypothesis
1. Kuenen & Menard (1952) Kuenen (1953, 1957)	Velocity pulsations in turbidity current.
2. Ksiazkiewicz (1952)	Diluted secondary turbidity currents suspended above bed.
3. Ten Haaf (1956)	Sorting action of vortices by turbulence in turbidity currents.
4. Hsü (1959)	Settling and laminar flow of fluidized sediment along bed.
5. Unrug (1959) Wood & Smith (1959)	Settling from tail of turbidity current with a non-uniform concentration.
6. Bouma (1962) & Lombard (1963)	Small turbulent eddies. Current velocity pulses with settling or traction.
7. Moss (1963) Kuenen (1966)	Grains of similar susceptibility to transport tend to deposit together, i.e. spatial & temporal selection of similar grains due to grain interaction under quasi-steady flow condition - the "like-seek-like" principle.
8. Allen (1964)	Pulsating sediment supply due to separate large scale eddies. Upper regime plane bed.
9. Walker (1965)	Intermittent supply of mixed sediment to top of viscous sublayer followed by differential settling through; for finer grained laminae. Coarser grained laminae under upper regime plane bed.
10. Sanders (1965)	Settling and traction during current velocity fluctuation. Not upper regime plane bed.
11. Jopling (1967)	Attributed laminae to the superposition of longitudinal segregations of bedload grains under aggradation of a upper regime plane bed.
12. Pettijohn (1957,1975)	Transitory phases or minor chance fluctuations in velocity of depositing current.
13. Middleton (1970)	Smaller grains filter down between larger ones during flow, thus displacing the larger ones towards the free surface.
14. Smith (1971) McBride et al. (1975)	Migration of very low relief bedforms (diminished ripples and dunes).
15. Frostick & Reid (1977)	Combine the ideas of Pettijohn, Moss and Kuenen.
16. Bridge (1978)	Described possible lamination formation due to the effect of single burst-sweep cycle on a plane bed.
17. Hesse & Chough (1980)	Suggested that a horizontal lamination formed with multiple burst and sweep events on plane bed.
18. Allen (1984)	Laminae form due to the shifting distribution of boundary shear stress as large eddies move downstream over a plane bed.
19. Bridge & Best (1988)	Laminae form by both migration of low-relief bedwaves and the turbulent bursting process.
20. Paola, Wiele & Reinhart (1989)	Extremely low amplitude bedforms. Initial deposition from small scale turbulent fluctuations in shear stress followed by sieving out mechanism resulting in a smooth surface process termed glazing.

Hjulstrom [1935] defined a relationship between velocity and motion of particles of different sizes. Various hypotheses formulated to explain the origin of near-horizontal lamination in unidirectional flow were compiled by Bridge [1978], and Cheel and Middleton [1986], and are summarized in table I. Allen [1984] stated that many authors have qualitatively recognized the importance of some periodic or quasi-periodic phenomenon, either located in the flow or in the uppermost levels of the bed. Velocity pulses, large eddies and turbulent fluctuations have had a wide appeal [Kuenen and Menard, 1952; Kuenen, 1953, 1957; Ten Haaf, 1956; Pettijohn, 1957, 1975; Bouma, 1962; Lombard, 1963; Allen, 1964].

Bridge [1978] proposed the "burst-sweep cycle" in the turbulent boundary layers to explain the vertical sorting that defines laminae. Accordingly, bursts would cause upward dispersion of the suspended load throughout the flow, also some of the saltating load would carry coarser grains due to higher shear stress. As bed shear stress decreases, the dispersed particles settle down to form a laminated layer. Allen [1984] suggested a model based on the larger coherent structures of the turbulent boundary layers to explain the formation of horizontal laminae under plane bed in the upper flow regime. Cheel and Middleton [1986] suggested that the probable mechanism for the formation of FU (fining-upward) and CU (coarsening-upward) laminae was the burst-sweep process. Unrug [1959], and Wood and Smith [1959] saw parallel lamination as caused by the segregation of the coarser grains into distinct clouds within the flow. Hsü [1959] attributed lamination to laminar flow at the bed.

On the basis of field observations or laboratory experiments, other investigators have explained parallel laminations by the travel of extremely flat symmetrical to strongly asymmetrical bed waves [Jopling, 1965, 1967; Jopling and Walker, 1968; Smith, 1971; McBride *et al.*, 1975; Allen, 1982], although not always in the context of an upper-stage plane bed. Paola *et al.* [1989], along with Bridge and Best [1988], explained that lamination results from the superposition of two processes: (1) high-frequency erosion and deposition due to turbulence; and (2) migration of low-amplitude bed forms that is neither upper- nor lower flow-regime.

A "like-seeks-like" mechanism of grain sorting in the bedload layer was advocated by Moss [1962, 1963] and Kuenen [1966]. Interestingly, Kuenen [1966] reported that: "current pulsations are so numerous that they should produce ten to a hundred times more laminae than are present." He also stated in his abstract: "the selective concentration is due to the tendency of particles moving along the bottom to join stationary ones of equal weight, density and shape..." He added that "in spite of extremely uniform discharge without pulsation, lamination developed in nearly all experiments." Guy *et al.* [1966] noted the sorting of coarse and fine sand particles in laboratory flumes. Middleton [1970] proposed that grading arose because smaller grains tended to filter down between the larger ones during flow, thus displacing the larger grains toward the free surface. This segregation mechanism is also referred to as "kinematic sieving" in Allen [1982]. A sorting process was also advocated by Frostick and Reid [1977]. Berthault [1986, 1988] found that the thickness of laminae in still

water increased as the difference between the size of particles became greater, and the laminae thickness also increased with flow velocity of running water.

The fundamental study reported herein focuses on laboratory experiments addressing three key issues in sediment stratification: (1) lamination (thinner than 10 mm) resulting from segregation of heterogeneous sand mixtures; (2) graded-beds (thicker than 10 mm) of heterogeneous sand mixtures that may result from steady non-uniform flow and continuous settling; and (3) horizontal joints at the interface between strata. The use of sand mixtures with coarse and fine particles of different colors ensures a better visualization of the sediment sorting besides providing an assessment of the distribution of different particle sizes. This article summarizes several laboratory reports by Julien and Chen [1989a,b] and Julien and Lan [1989, 1990a, 1990b] on recent laboratory experiments carried out in the Hydraulic Laboratory of the Engineering Research Center at Colorado State University.

II. - EXPERIMENTS ON SEGREGATION AND LAMINATION

Laboratory experiments on segregation of sand size mixtures of quartz, limestone and coal were carried out to examine how clearly various mixtures of particles of different sizes, density and shape can separate into thin layers of coarse and fine particles not exceeding a few millimeters in thickness: (1) under horizontal motion; and (2) through settling in air and water.

A) Sediment mixtures

Thirteen different sand size materials, have been used in the experiments. For each material, the particle size distribution, mass density, angle of repose, angularity and color are summarized in table II. Note that D_{10} , D_{25} , D_{50} ,

TABL. II. - Characteristics of sands tested.

TABL. II. - Caractéristique des sables utilisés.

Sand	Color	Mass density g/cm ³	Angle of repose in air (degree)	Angle of repose in water (degree)	Angularity	Particle diameter				
						D_{10} (mm)	D_{25} (mm)	D_{50} (mm)	D_{75} (mm)	D_{90} (mm)
B2040	black	2.70	39.5	38	angular	.38	.48	.57	.67	.76
B3060	black	2.70	37	36	angular	.14	.20	.33	.55	.62
ERC #1	white	2.45	35	32	rounded	.08	.11	.13	.15	.18
ERC #2	white	2.65	37	34	rounded	.72	.90	1.20	1.50	1.90
ERC #3	white	2.65	37.5	35	rounded	.48	.55	.63	.73	.82
ERC #4	white	2.65	--	--	--	.09	.13	.16	.19	.29
ERC #5	beige	2.65	42.5	35	rounded	.15	.29	.55	.97	--
limestone #1	white	2.65	--	--	rounded	--	.31	.39	.47	--
limestone #2	white	2.65	37	34	rounded	--	.76	.91	1.00	--
coal #1	black	1.30	--	--	angular	--	.26	.41	.57	--
coal #2	black	1.30	40	40	very angular	--	--	.25	--	--
coal #3	black	1.30	--	--	angular	--	--	.66	--	--
coal #4	black	1.30	--	--	angular	--	--	1.24	--	--

D_{75} and D_{90} represent the particle size for which 10%, 25%, 50%, 75% and 90%, respectively, of the particles are finer. The measured angle of repose increases as the subjective (angular vs. rounded) microscopic observation of angularity increases. Both parameters indicate that ERC #1, ERC #2, ERC #3, ERC #5, limestone #1, and limestone #2 are rounded, while coal #1, coal #3, coal #4, B2040 and B3060 are angular. Equal weights of materials of different sizes and colors were mixed to form a total of eleven mixtures listed in table III.

B) Experiments on segregation

Simple experiments were conducted to investigate possible segregation of sediment particles on a transparent horizontal plexiglas plate $30 \times 40 \text{ cm}^2$. A small volume (not exceeding 10 cm^3) of a given homogeneous sand mixture was poured onto the plate which was then gently agitated manually for a few minutes in the horizontal direction of the plexiglas plate. Pictures were then taken above and below the plate to examine whether segregation occurs. The same procedure was repeated for each sand mixture. Typical experimental results, shown on figure 1, demonstrate how easy it is to segregate these two types of particles with the finer white particles (ERC #1) underneath (see fig. 1a), and the coarser black particles (B2040) on top (see fig. 1b).

The experimental results for the segregation of 12 different mixtures scrutinized by Julien and Lan [1990b] are summarized in table III. The pattern of particle segregation generally includes three types: (1) no segregation; (2) fine particles on top of coarse particles; and (3) coarse particles on top of fine particles (fig. 1). Segregation of particles always takes place if the two types of particles in the mixture have different sizes or densities. The particle segregation diagram on figure 2 illustrates the three types of particle segregation according to particle diameter D_{50} and mass density ρ of the data from table III.

The most fundamental mechanism explaining the segregation of heterogeneous sand mixtures of constant mass

density starts from a uniform mixture of coarse and fine particles as sketched in figure 3. Only the lateral motion of the mixture in any direction is necessary to induce segregation. During lateral motion of the sand mixture in figure 3a, the fine particles fall through the interstices between coarse particles and reach the bottom of the moving

TABLE III. – Horizontal segregation of sand mixtures.

TABLE III. – *Ségrégation horizontale des mélanges sableux.*

#	Mixture†	Content‡	Observation
A	ERC #1 & B2040	$\rho_2 \cong \rho_1, D_2 \neq D_1$	Clear segregation. Coarse black particles on top of fine white particles (see Fig. 1).
B	ERC #3 & B2040	$\rho_2 \cong \rho_1, D_2 \cong D_1$	No apparent segregation.
C	ERC #1 & B3060	$\rho_2 \neq \rho_1, D_2 \neq D_1$	Clear segregation. Coarse black particles on top of fine white particles.
D	ERC #1 & coal #1	$\rho_2 \neq \rho_1, D_2 \neq D_1$	Clear segregation. Coarse black particles on top of fine and white particles.
E	ERC #3 & coal #3	$\rho_2 \neq \rho_1, D_2 = D_1$	Clear segregation. Coarse coal particles on top of fine white particles.
F	limestone #1 & B3060	$\rho_2 \cong \rho_1, D_2 \cong D_1$	No clear segregation of particles.
G	limestone #2 & coal #1	$\rho_2 \neq \rho_1, D_2 \neq D_1$	Clear segregation. Fine black particles on top of coarse white particles.
H	ERC#2 & coal #1	$\rho_2 \neq \rho_1, D_2 \neq D_1$	No clear segregation is observed.
I	limestone #1 & coal #2	$\rho_2 \neq \rho_1, D_2 \neq D_1$	Clear segregation. Fine black particles on top of coarse limestone particles.
J	limestone #1 & B2040	$\rho_2 \cong \rho_1, D_2 \neq D_1$	Clear segregation. Coarse black particles on top of limestone particles.
K	B3060 & ERC #3	$\rho_2 \neq \rho_1, D_2 \neq D_1$	Clear segregation. Coarse white particles on top of fine black particles.

† Mixtures are comprised of equal weight of each material.

‡ Mass density ρ , particle diameter D , different \neq , same $=$, comparable \cong , (e.g. $D_2 = D$, same particle diameter $\rho_2 \neq \rho$, different mass density)

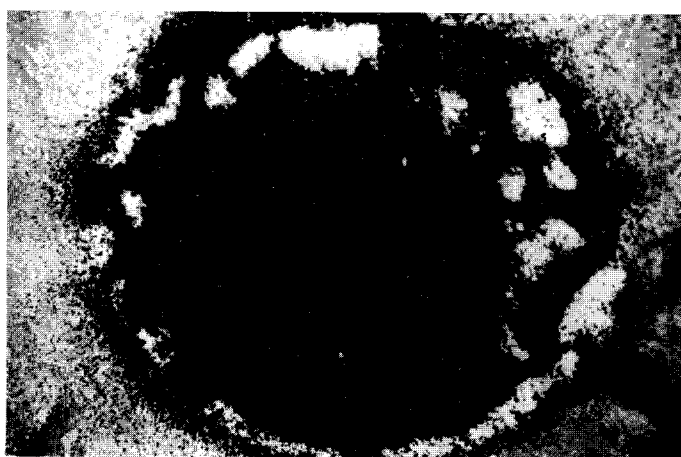


FIG. 1a. – Clear segregation of mixture ERC#1 & B2040, from above.

FIG. 1a. – *Ségrégation nette du mélange ERC#1 & B2040, vue de dessus.*



FIG. 1b. – Clear segregation of mixture ERC#1 & B2040, from underneath.

FIG. 1b. – *Ségrégation nette du mélange ERC#1 & B2040, vue de dessous.*

layer, while the coarse particles start rolling on top of the fine particles (fig. 3b). After a certain time, the fine particles stabilize at the bottom of the moving layer while the coarse particles remain mobile on top (fig. 3c). In order to obtain segregation with particles of the same mass density, it is important that the fines be sufficiently small to fall between the interstices of the coarse particles, and also, the coarse particles must be able to roll on top of the small ones. Particles of equivalent sizes and different densities also segregate with lighter particles on top of heavier particles.

Segregation is possible without bedforms and without turbulence, in that regard the segregation process is very different from the "glazing" process suggested by Paola *et al.* [1989]. Middleton [1970] and Allen [1982] also debated whether the dispersive shear stress arising from inter-particle collisions exerts a significant influence on segregation. Given that the dispersive stress is proportional to the square of the rate of deformation, we repeated our experiments under extremely low rates of deformation without inter-particle impact, thus negligible dispersive stress. The similar patterns that developed demonstrate that the segregation process results from the displacement of smaller grains between the coarser grains rather than from high speed inertial impact between particles.

C) Experiments on lamination

The objective of these experiments in a settling column was to examine possible repetitive segregation, or lamination, of various heterogeneous sand mixtures settling in air and in water. The visualization of the repetitive segregation under continuous settling of these mixtures falling into a column filled with air or water is possible through the plexiglas sidewalls of a square cylindrical settling column 10 cm × 10 cm × 84 cm (shown in fig. 4). A valve was installed at both ends of the cylinder to supply or drain water

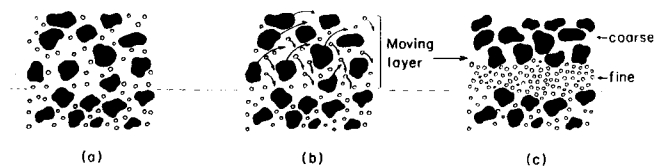


FIG. 3. – Sketch of the segregation process with constant particle mass density, before (a), during (b), and after (c) motion.

FIG. 3. – Schéma du processus de ségrégation des particules de densité constante, avant (a), durant (b), et après (c) mouvement.

during and/or after experiments. Photographs were taken from the sides of the column and the sorting characteristics of various mixtures with different densities, sizes and shapes were documented. A homogeneous mixture was poured at a constant rate (given in table IV) into the cone at the top of the cylinder. The valve controlling the settling rate was then opened to let the mixture settle directly near the center of the stationary cylinder.

During most experiments in air, the splashing of particles after impact was significant, owing to high fall velocities of the particles. The saltating distance of particles reached 5 cm from the point of impact. In many instances, no

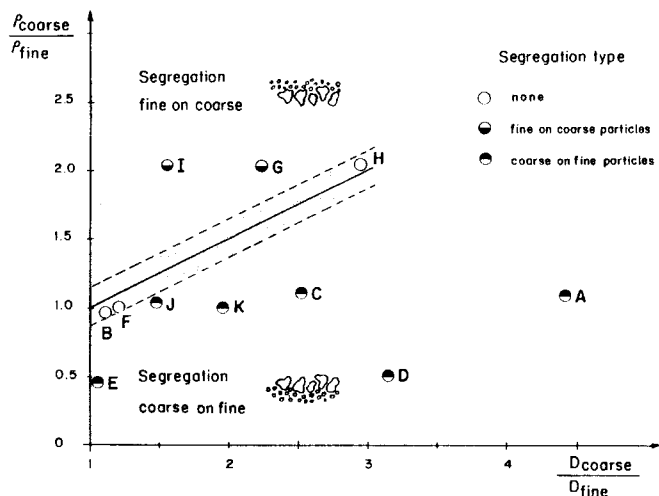


FIG. 2. – Particle segregation diagram.

FIG. 2. – Diagramme de ségrégation des particules.

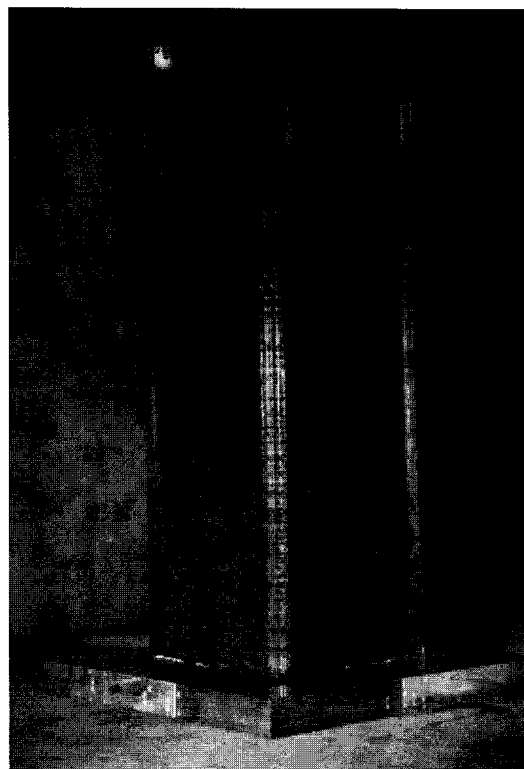


FIG. 4. – Example of clear lamination in air (mixture #C).

FIG. 4. – Exemple de lamination nette à l'air (mélange #C).

laminae formed when rolling of one type of particles on the other was not obvious. Splashing was reduced by raising the base height of the settling column. Clear repetitive segregation, or lamination, was shown in at least two experiments. In such cases as mixture #C, black particles roll on top of white particles before landsliding, resulting in clear lamination with thickness less than 0.5 cm.

The experimental results for each of ten different mixtures of quartz, limestone and coal are summarized in table IV for both runs in air and in water, respectively. Generally speaking, mixtures forming laminae in air often form laminae in water. However, cases such as mixtures #D and #I do not form laminae in water because coal particles settle very slowly in water. When the cylinder was slightly inclined at an angle of approximately 5°, the experiment with mixture #C highlights the importance of the rolling distance of the moving layers. Lamination becomes clearer as the rolling distance increases. The laminae thickness, however, remains unaffected by the inclination angle of the cylinder.

These experiments on lamination, summarized in table IV, support the following conclusions:

1) laminae can develop in either: (a) mixtures of the same density but different particle size – mixture #C; (b) mixtures of the same size but different particle density – mixture #E; or (c) mixtures of different particle density and different particle size – mixture #D;

2) laminae can be produced in both air and water. In air, splashing of the particles becomes predominant as the mixture gets coarser due to higher fall velocity. Splashing is greatly reduced in water, although the turbulence induced by the settling of coarser particles enhances suspension of finer particles. The settling of such mixtures becomes more uniform in that no laminae can be found because the segregation mechanism does not take place;

3) under a continuous supply of sediment, lamination is found to be essentially the result of the mechanical interaction between particles of different size, shape and density. The segregation process of heterogeneous sand mixtures under lateral motion, sketched in figure 3, is the primary

cause of lamination. Segregation results from the rolling of one particle over the other, and lamination is possible without fluid turbulence and without the migration of low amplitude bedforms. Superposed laminae cannot be identified to discontinuous sedimentation into successive layers.

III. – EXPERIMENTS ON GRADED-BEDS

Laboratory experiments on graded-beds were conducted to determine whether stratification of heterogeneous sand mixtures is possible under steady flow and a continuous supply of sand particles. As opposed to segregation and lamination where sorting of particles occurs at a scale not exceeding a few millimetres, the graded-beds experiments determine whether graded-beds of coarse and fine sands, at a scale exceeding 10mm, are possible. The flow conditions examined in the laboratory flume are: i.e. upper regime plane bed, flow conditions similar to those of Bijou Creek during the 1965 flood.

A) Experimental procedure

Laboratory experiments on graded-beds were carried out in a tilting plexiglas flume (0.15 m wide, 0.15 m deep, and 2.40 m long) shown on figure 5. The flume recirculates both water and sediment in order to provide a continuous supply of heterogeneous sand particles under steady flow conditions during the course of each experiment. Particular design consideration of the headbox and the entrance profile of the flume ensured complete sediment mixing and steady inflow of sediment.

Four types of sands identified in table I as ERC #2, ERC #4, B2040 and B3060 were selected to prepare two sand mixtures identified as SM2 (equal weights of B2040 and ERC #4), and SM3 (equal weights of B3060 and ERC #2). These mixtures have been used by Julien and Chen [1989a], and by Julien and Lan [1990b].

TABL. IV. – Settling lamination in air and water.

TABL. IV. – *Lamination des dépôts à l'air et submergés.*

Mixture	Characteristic	In Air		In Water	
		Settling Rate (cm ³ /s)	Lamination	Settling Rate (cm ³ /s)	Lamination
B B2040 & ERC #3	$\rho_2 \approx \rho_1$ $D_2 \approx D_1$	2.05	not clear	1.02	none
C ERC #1 & B3060	$\rho_2 \neq \rho_1$ $D_2 \neq D_1$	9.14	clear	9.11	not clear
D ERC #1 & coal #1	$\rho_2 \neq \rho_1$ $D_2 \neq D_1$	7.00	clear	9.0	none
E ERC #3 & coal #3	$\rho_2 \neq \rho_1$ $D_2 = D_1$	4.01	not clear	0.80	clear
F limestone #1 & B3060	$\rho_2 \approx \rho_1$ $D_2 \approx D_1$	9.00	none	0.84	not clear
G limestone #2 & coal #1	$\rho_2 \neq \rho_1$ $D_2 \neq D_1$	5.20	none	1.05	none
H ERC #2 & coal #1	$\rho_2 \neq \rho_1$ $D_2 \neq D_1$	9.00	none	0.75	none
I limestone #1 & coal #2	$\rho_2 \neq \rho_1$ $D_2 \neq D_1$	3.44	not clear	1.30	none
J limestone #1 & B2040	$\rho_2 \approx \rho_1$ $D_2 \neq D_1$	1.62	not clear	0.76	clear
L limestone #2 & B3060	$\rho_2 \approx \rho_1$ $D_2 \neq D_1$	9.00	none	0.90	none



FIG. 5. – Small recirculating flume.

FIG. 5. – *Petit canal de recirculation.*

TABL. V. – Summary of graded-bed measurements.

TABL. V. – *Compilation des mesures sur lits stratifiés.*

Step	Discharge Q (cm ³ /s)	Flow Depth h (cm)	Average Velocity V _m (cm/s)	Upstream Velocity V _u (cm/s)	Downstream Velocity V _d (cm/s)	H-Lam † (cm)	Froude Number Fr	Delta Thickness (cm)
Run: SM2A (Horizontal) D₅₀ = 0.28 mm								
SM2A-1	2650	2.9	57.5	53.2	33.2	0.27	.99	1.9
SM2A-2	3470	3.9	57.4	47.6	40.0	0.8	.59	0.8
SM2A-3	3949	4.0	63.6	50.0	46.3	1.1	.64	0.4
SM2A-4	4480	4.1	70.4	54.5	52.5	1.2	.74	0.2
Run: SM2D (Horizontal) D₅₀ = 0.28 mm								
SM2D-1	2750	3.4	52.1	46.7	26.2	0.4	.81	2.9
SM2D-2	4026	4.0	64.9	57.5	37.6	0.5	1.07	2.3
Run: SM2C (Pos. slope S = +0.005) D₅₀ = 0.28 mm								
SM2C-1	2778	3.7	48.4	42.0	35.5	0.6	.65	0.8
SM2C-2	3470	3.8	58.9	50.0	41.4	0.7	.93	0.9
SM2C-3	4007	4.5	57.4	50.0	45.3	0.7	.75	0.5
SM2C-4	4428	4.4	64.9	53.8	50.0	0.9	.98	0.4
Run: SM2B (Adv. Slope S = -0.005) D₅₀ = 0.28 mm								
SM2B-1	3334	4.0	53.7	45.7	36.4	0.7	.73	1.2
SM2B-2	3601	4.1	56.6	50.0	41.5	0.6	.80	0.9
SM2B-3	3644	4.0	58.7	50.0	42.7	0.7	.88	0.8
SM2B-4	3988	4.1	62.7	52.5	42.1	0.8	.98	1.2
Run: SM3A (Horizontal) D₅₀ = 0.62 mm								
SM3A-1	3558	3.9	58.8	50.0	44.0	0.7	.90	0.8
SM3A-2	3850	3.9	63.6	49.6	45.1	1.1	1.06	0.5
SM3A-3	4304	4.4	63.1	49.6	42.0	1.2	.92	1.0
SM3A-4	4939	4.5	70.8	54.9	51.4	1.3	1.14	0.4

† Horizontally laminated deposit thickness

Prior to each experiment, the flume slope was set (horizontal, positive, or adverse slope). The flow rate was controlled by a gate valve and measured by a Venturi orifice. The flow of water and sediment first ran freely near critical flow conditions without downstream gate control until reaching the equilibrium plane bed with sediment transport. Starting from equilibrium plane conditions, the deposition of sand in the flume in non-uniform flow was induced by inserting a first tailgate, 0.15 m wide and 0.02 m high, at the downstream end of the flume. The water depth and the thickening of sediment deposits were measured through the transparent sidewall of the flume. Local velocity measurements upstream and downstream of the delta were taken using a Ultrasonic Doppler Velocimeter Model UDV-89 with an accuracy of + 0.003 m/sec or 2 % of reading, whichever was greater. Measurements of discharge, surface

velocity and depth were taken and compiled in table V, and the progression of the deltaic sediment deposits was recorded. The new deposit reached the downstream end of the flume about 20 to 30 minutes after inserting the tailgate and new equilibrium conditions were then obtained. After completing the measurements, the second gate was inserted to form a second deposit and the documentation procedure was repeated.

B) Experimental results

This experimental procedure clearly demonstrated the formation of stratified graded beds. A schematic description of the formation of graded beds is sketched on figure 6. Under initial steady uniform flow conditions and a continu-

ous supply of heterogenous sand size particles, coarse particles roll on a bed of fine sand particles. The plane bed laminated deposit is comprised mostly of fine sand particles. The insertion of a single tailgate induces first the formation of a deltaic stratum of coarse black particles which propagates in the downstream direction. On the delta, fine particles cover the top set slope, while coarse particles roll on a laminated bed of fine particles. Coarse particles settle on the foreset slope of the delta, which progresses in the downstream direction as shown in figure 7. On the top of the delta, the fine white particles in the moving layer of rolling black particles deposit on the topset deposit of fine white particles. The thickness of the laminated topset deposit gradually increases until the delta foreset reaches the downstream end of the flume. Typical cross-sectional and longitudinal views of the deposit after a single tailgate in figures 8a and 8b clearly illustrates the stratified nature of the deposit of coarse black particles between two laminated deposits of finer white particles.

Elaborate descriptions of the deposits for each run (4 sets with mixture SM2 identified as SM2A to SM2D and

one set with mixture SM3 noted SM3A) are found in Julien and Chen [1989a]. Flume bed slopes are given in table V for each set of runs. The horizontally laminated (H-Lam) layer thickness was examined in terms of depth-averaged velocities upstream V_u and downstream V_d at the tip of the delta in table V. It was found that for the runs SM2A, V_u varies slightly, although V_d and H-Lam significantly increase with discharge, while the delta thickness decreases with discharge. At a comparable discharge, the runs SM2D showed an expected increase in delta thickness with gate height. With positive slope, runs SM2C, the results were similar to those with horizontal slope (SM2A) except that the thickness of deposits was less sensitive to changes in discharge. Under adverse slopes, runs SM2B, the thickness variability with discharge was also less significant.

These results primarily show that the delta thickness increases as V_d decreases, while V_u remains fairly constant ($V_u \approx 50$ cm/s). The effect of slope shows that the delta and H-Lam thicknesses vary with discharge for horizontal slope. Results are uncertain for both positive and adverse slopes.

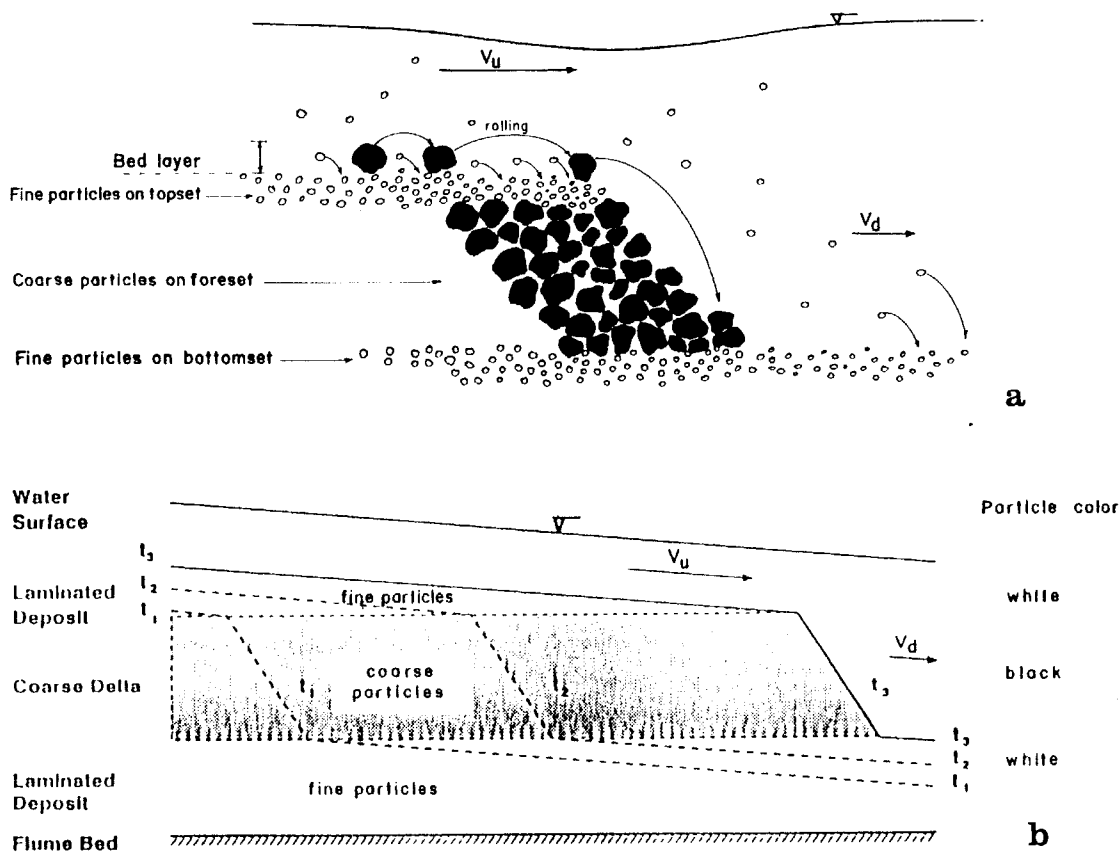


FIG. 6a. – Schematic formation of graded-beds.

FIG. 6a. – Schéma de formation de lits stratifiés.

FIG. 6b. – Time sequence of deposit formation for $t_1 < t_2 < t_3$.

FIG. 6b. – Séquence de formation des dépôts pour $t_1 < t_2 < t_3$.

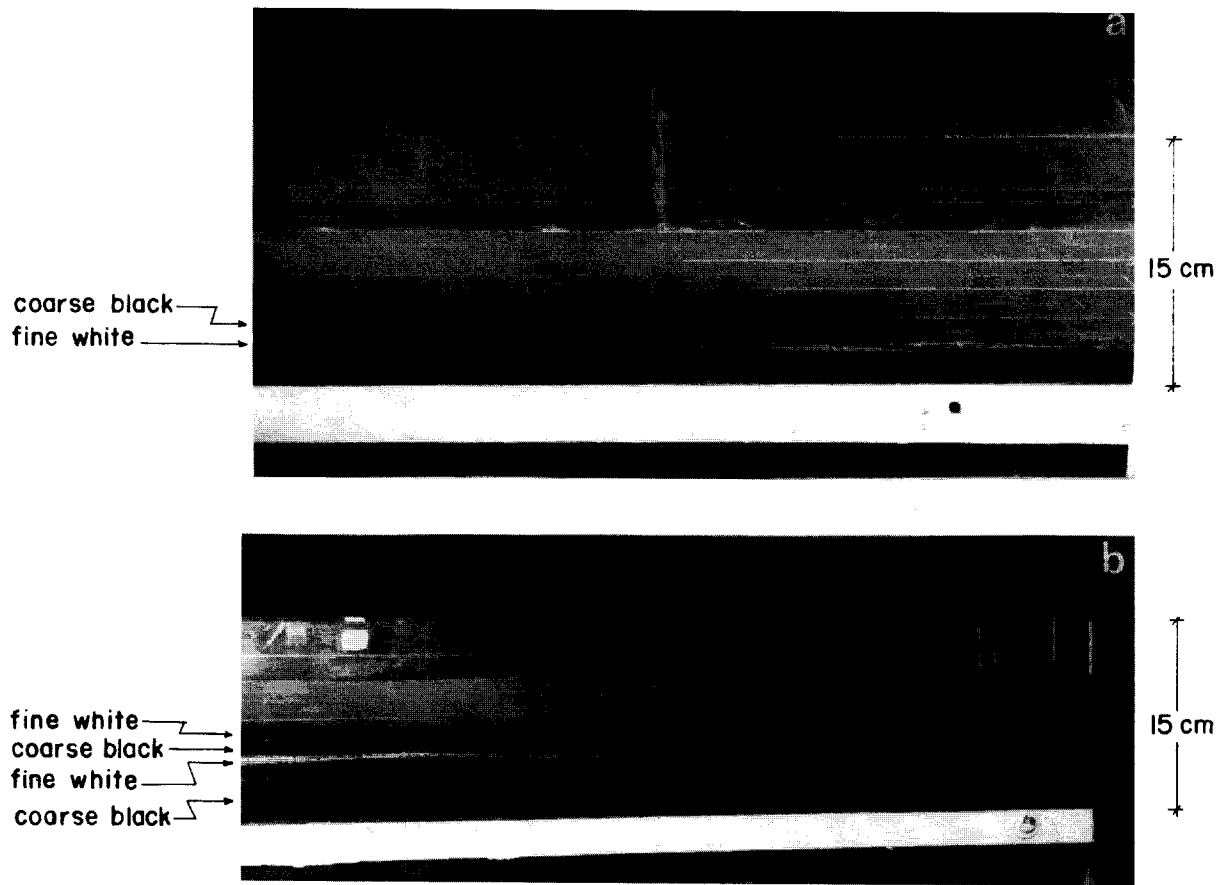


FIG. 7a. – Example of graded-beds with first tailgate.

FIG. 7a. – *Exemple de lits stratifiés avec premier seuil.*

FIG. 7b. – Example of graded-beds with second tailgate.

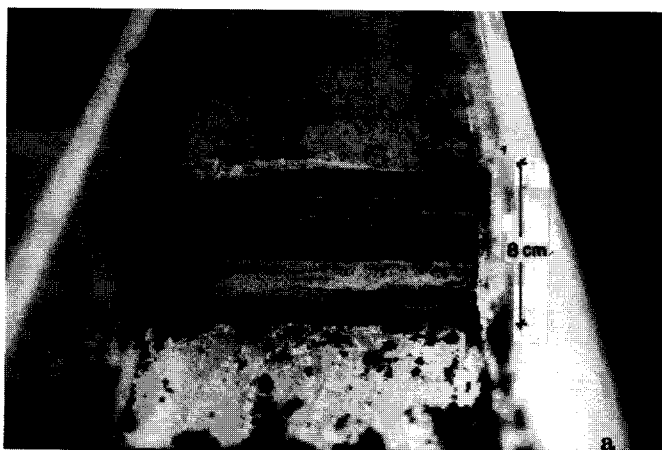
FIG. 7b. – *Exemple de lits stratifiés avec second seuil.*

FIG. 8a. – Typical cross-sectional view of deposit.

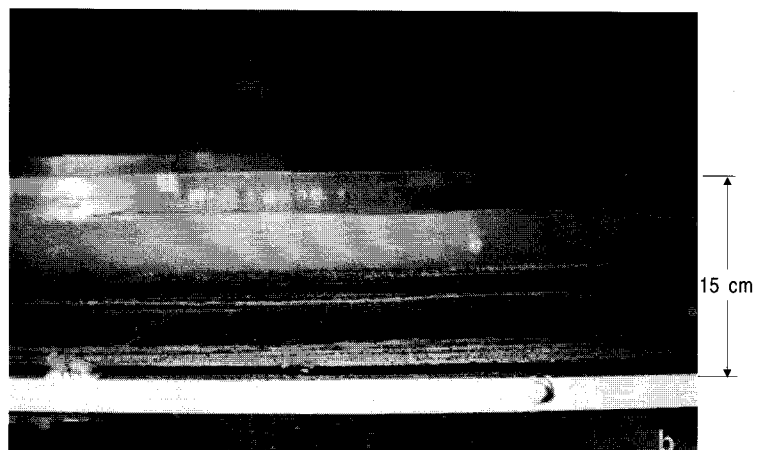
FIG. 8a. – *Coupe transversale typique du dépôt.*

FIG. 8b. – Typical longitudinal view of deposit (flow from right to left).

FIG. 8b. – *Coupe longitudinale typique du dépôt (écoulement vers la gauche).*

In summary, the velocity change in the downstream direction induces selective settling of particles of different sizes, thus forming graded-beds which develop in the downstream direction. These observations of graded-bed formation highlight the simultaneous development of topset and foreset deposits as sketched in figures 6 and 7. A laminated stratum of fine particles forms on top and at the base of a cross-stratified foreset stratum of coarse particles. The time sequence of the formation of this stratified deposit shows that sets of laminae develop vertically upward and propagate downstream as the cross-stratified bed of coarse particles progresses in the downstream direction. At a microscopic scale on the surface of the deposit, the coarse particles roll on a bed of fine particles in a manner very similar to the segregation process sketched in figure 3 and described in the first part of this experimental program. The experiments demonstrate that stratified deposits can form in steady non-uniform flow under a continuous supply of fine and coarse sediment particles.

IV. – EXPERIMENTS ON JOINTS FROM DESICCATION

The purpose of laboratory experiments on horizontal stratification joints was to examine, through desiccation, the possible appearance of vertical cracks and horizontal planes of preferential fracturing. The experiments focused on depositional and drying characteristics of the Bijou Creek natural sand in a small recirculating flume. This study was limited to deposits under steady flow and continuous supply of natural sand over a plane bed without bed forms [Julien and Chen, 1989b].

A) Experimental procedure

The sediment used in this experiment was the natural sand from the surface of the main channel bed of Bijou Creek near Hoyt, Colorado. The sample was taken near the locality III in the investigation of McKee *et al.* [1967]. Prior to the experiments, this natural sand was sieved to remove pebbles and organic material. The particle size ranged from fine to very coarse sand ($D_{10} = 0.34$ mm, $D_{50} = 0.75$ mm, and $D_{90} = 1.65$ mm), and the silt and clay content (passing the sieve #230) is only 0.1 percent of the sediment. The sediment size distribution was similar to that reported by McKee *et al.* [1967].

The procedure used was similar to that of the flume experiments discussed in the previous section. The graded-beds left in the flume after the experiment were exposed to solar lights for seven days until complete desiccation of the deposit.

B) Experimental results

No vertical cracks were found in the stratified deposit after seven days under solar lights, which may be attributed to the low silt and clay content (less than 1 %) of the hard crusted deposit. The horizontal planes, or joints, between the crusted finer sands and the coarser sands separated easily as shown in figure 9. These joints separating particles of different sizes constitute preferential planes for the propagation of fractures in dried sediment deposits. These

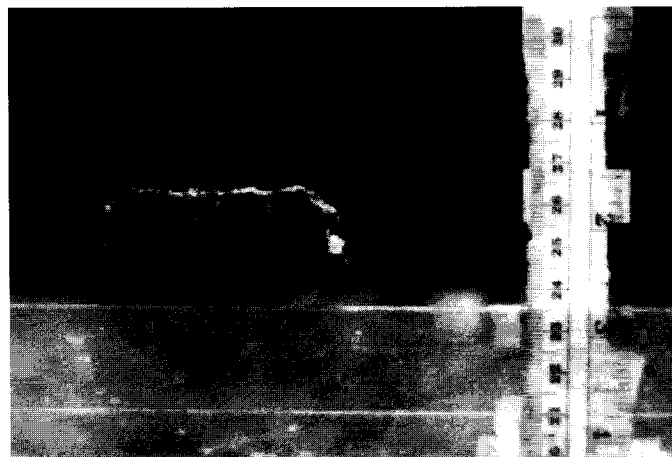


FIG. 9. – Horizontal fracturing of the Bijou Creek sand.

FIG. 9. – *Fractures horizontales du sable de Bijou Creek.*

experiments simply support previous observations that joints can result from desiccation and not necessarily from periods without sediment settling.

V. – CONCLUSIONS

This fundamental study demonstrates the usefulness of laboratory experiments in the analysis of stratification of heterogeneous sand mixtures. Upper flow regime conditions similar to the Bijou Creek flood can be reproduced in the laboratory, and clear stratification of heterogeneous mixtures is evidenced by using coarse and fine sand grains of different colors.

Lamination essentially results from the mechanical segregation of heterogeneous particles in a moving layer. Lamination is possible without turbulence and without the migration of low amplitude bedforms. Through lateral movement of particles of constant mass density, finer particles fall within the interstices of rolling coarser particles. Coarse particles then roll on top of fines and microscale segregation of particles is then obtained. The degree of segregation depends on particle size distribution, density and possibly angularity of heterogeneous sand mixtures (see fig. 2). Repetitive segregation is also possible in settling columns where lamination is clearly observed both in air and water. Sufficient space, or rolling distance, is required for clear lamination to develop in moving layers of heterogeneous particles. Particles of comparable size but different densities segregate similarly with heavier particles falling between lighter particles.

The graded-bed experiments clearly demonstrate the simultaneous formation of stratified deposits under steady flow conditions and a continuous supply of heterogeneous particles. The deposition process involves the formation of a stratum of coarse particles between laminated deposits of fine particles as a result of velocity changes in non-uniform flow. The time sequence of the deposit formation shows

that sets of laminae develop vertically upward and progress in the downstream direction. At a microscopic scale, at the surface of the deposit, coarse particles roll on a deposit of fine particles as a result of particle segregation.

Desiccation experiments on the Bijou Creek sand deposits in laboratory flumes, indicate preferential fracturing of the crusty deposit along horizontal planes, or stratification joints, separating graded-beds of coarse and fine particles. On the other hand, no vertical cracks were observed in the experiments, which may be explained by the low clay content of the Bijou Creek sand.

In summary, these experiments demonstrate that stratification of heterogeneous sand mixtures can result from: segregation for lamination, non-uniform flow for graded-beds, and desiccation for joints. Therefore, superposed strata are not necessarily identified to successive sedimentary layers.

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