

# B

## Laplace Transform

$$F(s) = \mathcal{L} [f(t)] = \int_0^{\infty} f(t)e^{-st} dt$$

**TABLE B.2 LAPLACE TRANSFORM THEOREMS**

Name	Theorem
Derivative	$\mathcal{L} \left[ \frac{df}{dt} \right] = sF(s) - f(0^+)$
$n$ th-Order derivative	$\mathcal{L} \left[ \frac{d^n f}{dt^n} \right] = s^n F(s) - s^{n-1} f(0^+) - \dots - f^{n-1}(0^+)$
Integral	$\mathcal{L} \left[ \int_0^t f(\tau) d\tau \right] = \frac{F(s)}{s}$
Shifting	$\mathcal{L} [f(t-t_0)u(t-t_0)] = e^{-ts} F(s)$
Initial value	$\lim_{t \rightarrow 0^+} f(t) = \lim_{s \rightarrow \infty} sF(s)$
Final value	$\lim_{t \rightarrow \infty} f(t) = \lim_{s \rightarrow 0} sF(s)$
Frequency shift	$\mathcal{L} [e^{-at} f(t)] = F(s+a)$
Convolution integral	$\mathcal{L}^{-1} [F_1(s)F_2(s)] = \int_0^t f_1(t-\tau)f_2(\tau) d\tau$ $= \int_0^t f_1(\tau)f_2(t-\tau) d\tau$

Time function $e(t)$	Laplace transform $E(s)$	z-Transform $E(z)$
$u(t)$	$\frac{1}{s}$	$\frac{z}{z-1}$
$t$	$\frac{1}{s^2}$	$\frac{Tz}{(z-1)^2}$
$\frac{t^2}{2}$	$\frac{1}{s^3}$	$\frac{T^2z(z+1)}{2(z-1)^3}$
$t^{k-1}$	$\frac{(k-1)!}{s^k}$	$\lim_{a \rightarrow 0} (-1)^{k-1} \frac{\partial^{k-1}}{\partial a^{k-1}} \left[ \frac{z}{z-e^{-aT}} \right]$
$e^{-at}$	$\frac{1}{s+a}$	$\frac{z}{z-e^{-aT}}$
$te^{-at}$	$\frac{1}{(s+a)^2}$	$\frac{Tze^{-aT}}{(z-e^{-aT})^2}$
$t^{k-1}e^{-at}$	$\frac{(k-1)!}{(s+a)^k}$	$(-1)^k \frac{\partial^k}{\partial a^k} \left[ \frac{z}{z-e^{-aT}} \right]$
$1 - e^{-at}$	$\frac{a}{s(s+a)}$	$\frac{z(1-e^{-aT})}{(z-1)(z-e^{-aT})}$
$t - \frac{1-e^{-at}}{a}$	$\frac{a}{s^2(s+a)}$	$\frac{z[(aT-1+e^{-aT})z + (1-e^{-aT}-aTe^{-aT})]}{a(z-1)^2(z-e^{-aT})}$
$1 - (1+at)e^{-at}$	$\frac{a^2}{s(s+a)^2}$	$\frac{z\{[1-e^{-aT}-aTe^{-aT}]z + [e^{-2aT} + (aT-1)e^{-aT}]\}}{(z-1)(z-e^{-aT})^2}$
$e^{-at} - e^{-bt}$	$\frac{b-a}{(s+a)(s+b)}$	$\frac{(e^{-aT}-e^{-bT})z}{(z-e^{-aT})(z-e^{-bT})^2}$
$\sin bt$	$\frac{b}{s^2+b^2}$	$\frac{z \sin bT}{z^2 - 2z \cos bT + 1}$
$\cos bt$	$\frac{s}{s^2+b^2}$	$\frac{z(z - \cos bT)}{z^2 - 2z \cos bT + 1}$
$t \sin bt$	$\frac{2bs}{(s^2+b^2)^2}$	
$t \cos bt$	$\frac{s^2-b^2}{(s^2+b^2)^2}$	
$e^{-at} \sin bt$	$\frac{b}{(s+a)^2+b^2}$	$\frac{ze^{-aT} \sin bT}{z^2 - 2ze^{-aT} \cos bT + e^{-2aT}}$
$e^{-at} \cos bt$	$\frac{s+a}{(s+a)^2+b^2}$	$\frac{z^2 - ze^{-aT} \cos bT}{z^2 - 2ze^{-aT} \cos bT + e^{-2aT}}$
$1 - e^{-at} \left( \cos bt + \frac{a}{b} \sin bt \right)$	$\frac{a^2+b^2}{s[(s+a)^2+b^2]}$	$\frac{z(Az+B)}{(z-1)(z^2 - 2ze^{-aT} \cos bT + e^{-2aT})}$
$A = 1 - e^{-aT} \left[ \cos bT + \left( \frac{a}{b} \right) \sin bT \right]$		
$B = e^{-2aT} + e^{-aT} \left[ \left( \frac{a}{b} \right) \sin bT - \cos bT \right]$		

### Definition

The hyperbolic sine function, denoted by  $\sinh$ , and the hyperbolic cosine function, denoted by  $\cosh$ , are given by

$$\sinh x = \frac{e^x - e^{-x}}{2} \quad \text{and} \quad \cosh x = \frac{e^x + e^{-x}}{2}$$

where  $x$  is any real number.

>> help residue

RESIDUE Partial-fraction expansion (residues).

$[R,P,K] = \text{RESIDUE}(B,A)$  finds the residues, poles and direct term of a partial fraction expansion of the ratio of two polynomials  $B(s)/A(s)$ . If there are no multiple roots,

$$\frac{B(s)}{A(s)} = \frac{R(1)}{s - P(1)} + \frac{R(2)}{s - P(2)} + \dots + \frac{R(n)}{s - P(n)} + K(s)$$

Vectors  $B$  and  $A$  specify the coefficients of the numerator and denominator polynomials in descending powers of  $s$ . The residues are returned in the column vector  $R$ , the pole locations in column vector  $P$ , and the direct terms in row vector  $K$ . The number of poles is  $n = \text{length}(A) - 1 = \text{length}(R) = \text{length}(P)$ . The direct term coefficient vector is empty if  $\text{length}(B) < \text{length}(A)$ , otherwise  $\text{length}(K) = \text{length}(B) - \text{length}(A) + 1$ .

If  $P(j) = \dots = P(j+m-1)$  is a pole of multiplicity  $m$ , then the expansion includes terms of the form

$$\frac{R(j)}{s - P(j)} + \frac{R(j+1)}{(s - P(j))^2} + \dots + \frac{R(j+m-1)}{(s - P(j))^m}$$

$[B,A] = \text{RESIDUE}(R,P,K)$ , with 3 input arguments and 2 output arguments, converts the partial fraction expansion back to the polynomials with coefficients in  $B$  and  $A$ .

Based on the preceding definitions, we may now state Mason's gain formula. The formula gives the transfer function from a source (input) node to a sink (output) node *only* and may be stated as

$$T = \frac{1}{\Delta} \sum_{k=1}^p M_k \Delta_k = \frac{1}{\Delta} (M_1 \Delta_1 + M_2 \Delta_2 + \dots + M_p \Delta_p) \quad (2-19)$$

where  $T$  is the gain (transfer function) from the input node to the output node,  $p$  is the number of forward paths, and

- $\Delta = 1 -$  (sum of all *individual* loop gains)  
 $+$  (sum of the products of the loop gains of all possible combinations of nontouching loops taken two at a time)  
 $-$  (sum of the products of the loop gains of all possible combinations of nontouching loops taken three at a time)  
 $+$  (sum of the products of the loop gains of all possible combinations of nontouching loops taken four at a time)  
 $-$  (...)

$M_k =$  path gain of the  $k$ th forward path

$\Delta_k =$  value of  $\Delta$  for that part of the flow graph not touching the  $k$ th forward path

#### 4.1 TIME RESPONSE OF FIRST-ORDER SYSTEMS

In this section the time response of first-order systems is investigated. The transfer function of a general first-order system can be written as

$$G(s) = \frac{C(s)}{R(s)} = \frac{b_0}{s + a_0} \quad (4-1)$$

where  $R(s)$  is the input function and  $C(s)$  is the output function; this notation is common.

A more common notation for the first-order transfer function is

$$G(s) = \frac{C(s)}{R(s)} = \frac{K}{\tau s + 1} \quad (4-2)$$

since physical meaning can be given to both  $K$  and  $\tau$ . We call (4-2) the standard form of the first-order system. Of course, in (4-1) and (4-2),

$$a_0 = \frac{1}{\tau} \quad b_0 = \frac{K}{\tau} \quad (4-3)$$

#### 4.2 TIME RESPONSE OF SECOND-ORDER SYSTEMS

In this section we investigate the response of second-order systems to certain inputs. We assume that the system transfer function is of the form

$$G(s) = \frac{C(s)}{R(s)} = \frac{b_0}{s^2 + a_1 s + a_0} \quad (4-17)$$

However, as in the first-order case, the coefficients are generally written in a manner such that they have physical meaning. The *standard form* of the second-order transfer function is given by

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad (4-18)$$

## 6.1 ROUTH-HURWITZ STABILITY CRITERION

The Routh-Hurwitz criterion is an analytical procedure for determining if all roots of a polynomial have negative real parts and is used in the stability analysis of linear time-invariant systems. The criterion gives the number of roots with positive real parts, and applies to all LTI systems for which the characteristic equation is a polynomial set to zero. This requirement excludes a system that contains an ideal time delay (transport lag). For this special case, which is covered later, the Routh-Hurwitz criterion cannot be employed.

The Routh-Hurwitz criterion applies to a polynomial of the form

$$Q(s) = a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0 \quad (6-4)$$

where we can assume with no loss of generality that  $a_0 \neq 0$ . Otherwise, the polynomial can be expressed as a power of  $s$  multiplied by a polynomial in which  $a_0 \neq 0$ . The power of  $s$  indicates roots at the origin, the number of which is evident; hence, only the latter polynomial need be investigated using the Routh-Hurwitz criterion. We assume in the following developments that  $a_0$  is not zero.

The first step in the application of the Routh-Hurwitz criterion is to form the array below, called the Routh array, where the first two rows are the coefficients of the polynomial in (6-4).

$$\begin{array}{c|cccc} s^n & a_n & a_{n-2} & a_{n-4} & a_{n-6} & \dots \\ s^{n-1} & a_{n-1} & a_{n-3} & a_{n-5} & a_{n-7} & \dots \\ s^{n-2} & b_1 & b_2 & b_3 & b_4 & \dots \\ s^{n-3} & c_1 & c_2 & c_3 & c_4 & \dots \\ \vdots & \vdots & \vdots & & & \\ s^2 & k_1 & k_2 & & & \\ s^1 & l_1 & & & & \\ s^0 & m_1 & & & & \end{array}$$

The column with the powers of  $s$  is included as a convenient accounting method. The  $b$  row is calculated from the two rows directly above it, the  $c$  row, from the two rows directly above it, and so on. The equations for the coefficients of the array are as follows:

$$\begin{aligned} b_1 &= -\frac{1}{a_{n-1}} \begin{vmatrix} a_n & a_{n-2} \\ a_{n-1} & a_{n-3} \end{vmatrix} & b_2 &= -\frac{1}{a_{n-1}} \begin{vmatrix} a_n & a_{n-4} \\ a_{n-1} & a_{n-5} \end{vmatrix}, \dots \\ c_1 &= -\frac{1}{b_1} \begin{vmatrix} a_{n-1} & a_{n-3} \\ b_1 & b_2 \end{vmatrix} & c_2 &= -\frac{1}{b_1} \begin{vmatrix} a_{n-1} & a_{n-5} \\ b_1 & b_3 \end{vmatrix}, \dots \end{aligned} \quad (6-5)$$

and so on. Note that the determinant in the expression for the  $i$ th coefficient in a row is formed from the first column and the  $(i + 1)$  column of the two preceding rows.