

Chapter 16 Equations

Circular pitch of the gear (or pinion) in a plane normal to the teeth

$$p_n = p \cos \psi \quad (16.1)$$

Tangent of pressure angle measured in a plane normal to the teeth

$$\tan \phi_n = \tan \phi \cos \psi \quad (16.2)$$

Diametral pitch in normal plane

$$P_n = P / \cos \psi \quad (16.3)$$

Diameter of a helical gear (at pitch circle)

$$d = N/P = N/(P_n \cos \psi) \quad (16.4)$$

Axial pitch

$$p_a = p / \tan \psi \quad (16.5)$$

Equivalent number of teeth (formative or virtual number of teeth)

$$N_e = N / \cos^3 \psi \quad (16.6)$$

Transmitted force (English)

$$F_t = 33,000 \dot{W} / V \quad (16.7)$$

Transmitted force (SI)

$$F_t = \dot{W} / V \quad (16.7a)$$

Radial force component

$$F_r = F_t \tan \phi \quad (16.8)$$

Axial force component

$$F_a = F_t \tan \psi \quad (16.9)$$

Transverse normal force component

$$F_b = F_t / \cos \psi \quad (16.10)$$

Helical-gear tooth force

$$F = F_b / \cos \phi_n = F_t / \cos \psi \cos \phi_n \quad (16.11)$$

Gear-tooth-bending stress (refined Lewis equation)

$$\sigma = \frac{F_t P}{bJ} K_v K_o (0.93 K_m) \quad (16.12)$$

Gear fatigue strength

$$S_n = S'_n C_L C_G C_S k_r k_t k_{ms} \quad (15.18)$$

Surface (Hertz) fatigue stress

$$\sigma_H = C_p \sqrt{\frac{F_t}{bd_p I} \left(\frac{\cos \psi}{0.95 CR} \right) K_v K_o (0.93 K_m)} \quad (16.13)$$

(Chapter 16 Equations Continued)

Gear-tooth surface fatigue strength

$$S_H = S_{fe} C_{Li} C_R \quad (15.25)$$

Shaft angle of crossed helical gears

$$\Sigma = \psi_1 + \psi_2 \quad (16.14)$$

Virtual number of teeth for pinion and gear (bevel gears)

$$N'_p = \frac{2\pi r_{bp}}{p} \quad \text{and} \quad N'_g = \frac{2\pi r_{bg}}{p} \quad (16.15)$$

Virtual number of teeth for pinion and gear (bevel gears)

$$N'_p = 2r_{bp}P \quad \text{and} \quad N'_g = 2r_{bg}P \quad (16.15a)$$

Gear ratio

$$\text{Gear ratio} = \frac{\omega_p}{\omega_g} = \frac{N_g}{N_p} = \frac{d_g}{d_p} = \tan \gamma_g = \cot \gamma_p \quad (16.16)$$

Limit on face width

$$b \leq \frac{10}{P} \quad \text{and} \quad b \leq \frac{L}{3} \quad (L \text{ is defined in Figure 16.9}) \quad (16.17)$$

Average bevel gear diameter (feet)

$$d_{av} = d - b \sin \gamma \quad (16.18)$$

Average velocity (feet per minute)

$$V_{av} = \pi d_{av} n \quad (16.19a)$$

Transmitted force (lb)

$$F_t = 33,000 \dot{W} / V_{av} \quad (16.20a)$$

Average velocity (meters per second)

$$V_{av} = \pi d_{av} n \quad (16.19b)$$

Transmitted force (newtons)

$$F_t = \dot{W} / V_{av} \quad (16.20b)$$

Bevel gear tooth force

$$F = F_t / \cos \phi \quad (16.21)$$

Normal force (to pitch cone) component

$$F_n = F \sin \phi = F_t \tan \phi \quad (f)$$

Axial force component

$$F_a = F_n \sin \gamma = F_t \tan \phi \sin \gamma \quad (16.22)$$

(Chapter 16 Equations Continued)

Radial force component

$$F_r = F_n \cos \gamma = F_t \tan \phi \cos \gamma \quad (16.23)$$

Axial force component (spiral bevel gear)

$$F_a = \frac{F_t}{\cos \psi} (\tan \phi_n \sin \gamma \mp \sin \psi \cos \gamma) \quad (16.24)$$

Radial force component (spiral bevel gear)

$$F_r = \frac{F_t}{\cos \psi} (\tan \phi_n \cos \gamma \pm \sin \psi \sin \gamma) \quad (16.25)$$

Bevel gear-tooth-bending stress

$$\sigma = \frac{F_t P}{bJ} K_v K_o K_m \quad (15.17)$$

Bevel gear-tooth surface fatigue strength

$$\sigma_H = C_p \sqrt{\frac{F_t}{b d_p I} K_v K_o K_m} \quad (15.24)$$

Pitch diameter of worm gear

$$d_g = N_g p / \pi \quad (15.2, \text{modified})$$

Velocity ratio of worm gear set

$$\frac{\omega_w}{\omega_g} = \frac{N_g}{N_w} \quad (16.26)$$

Guideline for worm gear set design

$$N_w + N_g > 40 \quad (16.27)$$

Guideline for maximum power-transmitting capacity of worm gear set

$$\frac{c^{0.875}}{3.0} \leq d_w \leq \frac{c^{0.875}}{1.7} \quad (16.28)$$

Minimum diameter for shell worm

$$d_w = 2.4p + 1.1 \text{ (in.)} \quad (16.29)$$

Guideline for gear face width design

$$b \leq 0.5 d_{w,\text{out}} \quad (16.30)$$

Worm lead angle

$$\tan \lambda = L / \pi d_w \quad (10.1, \text{modified})$$

Tangential force on worm gear

$$F_{gt} = F_{wa} = F_n \cos \phi_n \cos \lambda - f F_n \sin \lambda \quad (\text{g})$$

(Chapter 16 Equations Continued)

Tangential force on worm

$$F_{wt} = F_{ga} = F_n \cos \phi_n \sin \lambda + f F_n \cos \lambda \quad (h)$$

Radial force on gear

$$F_{gr} = F_{wr} = F_n \sin \phi_n \quad (i)$$

Ratio of tangential velocity of gear to tangential velocity of worm

$$V_g/V_w = \tan \lambda \quad (16.33)$$

Efficiency of worm gear set

$$e = \frac{\cos \phi_n - f \tan \lambda}{\cos \phi_n + f \cot \lambda} \quad (16.34)$$

Sliding velocity

$$V_s = V_w/\cos \lambda = V_g/\sin \lambda \quad (16.35)$$

Worm gear set coefficient of friction condition for self-locking

$$f \geq \cos \phi_n \tan \lambda \quad (16.36)$$

Dynamic load

$$F_d = F_{gt} K_v = F_{gt} \frac{1200 + V_g}{1200} \quad (16.39)$$

Maximum allowable value of dynamic load (bending fatigue)

$$F_s = S_n b p y \quad (16.40)$$

Maximum allowable value of dynamic load (surface fatigue)

$$F_w = d_g b K_w \quad (16.41)$$

Rate of heat dissipation

$$H = CA(t_o - t_a) \quad (13.13)$$

External area of conventional worm gear housing

$$A = 0.3c^{1.7} \quad (16.42)$$