Interferometric lithography with an amplitude division interferometer and a desktop extreme ultraviolet laser

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We demonstrate a compact interferometric lithography nanopatterning tool based on an amplitude division interferometer (ADI) and a 46.9 nm wavelength desktop size capillary discharge laser. The system is designed to print arrays of lines, holes, and dots with sizes below 100 nm on high resolution photoresists for the fabrication of arrays of nanostructures with physical and biological applications. The future combination of this ADI with high repetition rate tabletop lasers operating at shorter wavelengths should allow the printing of arrays of sub-10 nm size features with a tabletop setup. © 2008 Optical Society of America

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1. INTRODUCTION

The fabrication of large arrays of metallic or semiconduc-
tor pillars and holes with sizes below 100 nm has at-
tracted attention due to their potential applications in
several fields. These include, for example, the manufac-
turing of nanoscale rf oscillator arrays [1,2], patterned
magnetic storage devices [3], and convenient devices for
DNA sequencing [4]. Different approaches have been ap-
plied to the fabrication of arrays of nanoscale pillars and
holes including electron beam lithography, self-assembly
of nanospheres, or replication by embossing, molding, or
printing with master stamps [5,6]. Electron beam lithog-
raphy provides an outstanding spatial resolution capabil-
ity but is a time consuming approach due to the intrinsic
serial characteristic of the writing process [7]. The self-
assembly approach permits the fabrication of large area
periodic structures with nanometer size features; how-
ever special effort should be made in order to avoid dislo-
cations, discontinuities, or the spontaneous generation of
reduced size domains [8]. A very interesting alternative is
replication with master stamps, a technique that has
demonstrated feature sizes below 100 nm but requires a
different master for each motif [9,10].

Interferometric lithography (IL) has emerged as an at-
ttractive maskless alternative to print in a relatively
simple way arrays of nanoscale periodic features. This
 technique, which requires the use of a coherent light
source, relies on the activation of a photoresist by the in-
terference pattern generated by two or more mutually co-
herent light beams [11–17]. When two mutually coherent
beams are combined in the surface of a photoresist, the
generated interference pattern can activate the photon-
sist and print periodic lines with a period given by
p = \lambda / (2 \sin \theta), where \lambda is the wavelength of the illumina-
tion and \theta is the incidence angle. Several schemes can be
implemented based on the same idea, but in all cases the
ultimate resolution, \lambda/2, is limited by the wavelength of
the illumination. Thus, reducing the wavelength is a di-
rect path toward realizing interference patterns with di-
mensions of tens of nanometers and below. This charac-
teristic has been the motivation for using extreme
ultraviolet (EUV) and soft x-rays (SXR) synchrotron light
for this application [15,18]. Feature sizes as small as
19 nm have been printed using a Lloyd’s mirror interfer-
ometer with synchrotron illumination [17,18]. However,
the widespread use of IL in nanotechnology applications
would benefit from the implementation of more compact
and easily accessible setups. The increased average power
of compact plasma-based EUV lasers offers the possibility
of implementing EUV IL on a tabletop. In recent work we
demonstrated a compact nanopatterning system based on
a Lloyd’s mirror interferometer configuration illuminated
with a 46.9 nm wavelength tabletop capillary discharge
laser that allowed the printing of gratings and arrays of
nanodots [19,20].

In this paper we describe a compact interferometric
nanopatterning tool based on the combination of an am-
plitude division interferometer (ADI) and a desktop \lambda
= 46.9 nm capillary discharge laser. With interfering
beams of equal path length and originating from the same
part of the wavefront, the ADI has significant advantages as compared with the wavefront division Lloyd’s mirror configuration. First, with the ADI it is possible to print larger areas due to its relaxed spatial coherence requirements. This represents an important advantage, in particular when the interferometer is used in combination with laser-pumped tabletop EUV lasers that are not fully spatially coherent. In the ADI the interference in the sample plane is obtained by the superposition of two beams corresponding to the two branches that are replicas of the original wavefront impinging the beam splitter diffraction grating. Second, both beams have practically the same intensity and thus produce a higher and more uniform contrast in the interference pattern over the whole printed area.

2. EXPERIMENTAL DETAILS

For this initial demonstration of the ADI lithography tool we used an extremely compact, “desktop” $\lambda = 46.9$ nm Ne-like Ar capillary discharge laser configured to emit pulses with energy of $\sim 10 \mu J$ and $\sim 1$ ns FWHM duration. The EUV laser can operate at repetition rates up to 12 Hz producing pulses corresponding to average powers up to 0.12 mW. Due to its short capillary plasma column length (21 cm) its spatial coherence length is only a fraction of a millimeter at the sample location, a value that is significantly smaller than that corresponding to the tabletop capillary discharge laser used in previous Lloyd’s mirror IL experiments [21,22]. The laser temporal coherence length is approximately $470 \mu m$ determined by its line width $\Delta \lambda / \lambda < 1 \times 10^{-4}$. The laser unit is extremely compact; it occupies a footprint of $0.8 \times 0.4 \ m$ including its turbomolecular pump and has a small power supply that can fit under the optical table [23]. The ADI follows a Mach–Zehnder configuration, where the beam splitter is a transmission diffraction grating. Figure 1 shows a diagram of the interferometer and a photograph of the experimental setup with the paths of the two beams indicated by dashed curves. The 1 and −1 orders of the grating, that for the 46.9 nm illumination are separated by 2.68°, are used to form the two arms of the interferometer. The zero order is blocked from reaching the sample plane. The folding mirrors were implemented using two Si wafers placed at an incidence angle between 5° and 8° depending on the patterned period. The footprint of the interferometer is small, $\sim 0.2 \ m \times 0.4 \ m$. Its overall light throughput is at a maximum 6%, considering that the grating diffraction efficiency in the first order is 40.5%, the reflectivity of the Si mirrors is 94%, and the transparency of the Si membrane is 15%. The interference gives rise to a sinusoidal pattern of period $p$ that is recorded on a hydrogen silsesquioxane (HSQ) photoresist deposited on a Si wafer.

The transmission grating used to split the beam has a $2 \mu m$ period with 50% duty cycle lines. It was fabricated in a $2 mm \times 0.6 \ mm$ Si membrane $\sim 100$ nm thick. Figure 2(a) schematically shows the sequence of steps in the grating fabrication process. A thin layer of Si was sputtered on top of a Si$_3$N$_4$ membrane fabricated in a 550 $\mu m$ thick Si wafer. Subsequently, a 350 nm thick photoresist layer was deposited by spin coating on top of the sputtered Si. The grating was patterned in the photoresist by electron beam lithography. Finally, the Si$_3$N$_4$ layer was removed by chemically assisted ion beam etching through the substrate opening leaving a self-standing 100 nm thick Si membrane with the grating defined in the photoresist. The thin Si membrane provides 15%–20% transparency to the $\lambda = 46.9$ nm photons, while the photoresist that remains in the membrane acts as perfectly absorbent regions, constituting an amplitude transmission diffra-
tion grating. Figure 2(b) shows an atomic force microscope (AFM) scan of the completed grating, revealing a highly regular profile. The resulting open areas were measured to be 980 nm wide and to have a period of 2.02 μm. The interferometer was positioned at 1.4 m from the exit of the capillary discharge plasma, where the laser beam uniformly illuminates the whole grating.

The optical path difference between the two branches of the interferometer can easily be adjusted within a distance smaller than 470 μm, the longitudinal coherence of the laser source. The required accuracy in the overlapping of the two beams at the sample’s surface is defined by the spatial coherence of the beams, which for the λ=46.9 nm laser used in this experiment is a fraction of a millimeter at the location of the sample. The system is very robust, requiring only minor adjustments after its initial alignment.

3. RESULTS

Figure 3(a) shows a dense line grating pattern with a period of 145 nm (72.5 nm thick lines) printed on the HSQ with the ADI setup. The printed area corresponds to the size of the grating beam splitter (in this experiment 2 mm × 0.6 mm). The penetration depth of the 46.9 nm light in the photoresist is ~120 nm. The images shown in Fig. 3 are AFM scans of the sample obtained with the AFM working in the tapping mode. To print gratings of a smaller period we increased the angle between the two beams impinging at the sample by changing the angle of incidence at the two Si mirrors and by correcting the position of the sample. A dense line pattern with a ~95 nm period (47.5 nm wide lines) printed on the HSQ over an area of 2 mm × 0.6 mm was obtained in this case. An AFM scan of this dense line pattern is shown in Fig. 3(b). Since the laser was operated at a repetition rate of only 3 Hz, exposures of more than 10 min were required. The exposures can be reduced by more than 1 order of magnitude by combining this ADI with the tabletop version of the capillary discharge laser (footprint 1 m × 0.5 m), which is capable of producing milliwatt average powers [21,22].

The 95 nm period lines show an increased noise as compared with the larger pitch sample. One possible explanation for this lower quality printing is the influence of vibrations during the exposure. In addition the print quality may possibly be affected by photoresist scumming, which is particularly severe in 50% duty cycle lines with line widths approaching 50 nm [24] or by the presence of scattering centers in the grating and mirrors that introduce a random noise background reducing the fringe visibility.

The HSQ thickness in these experiments was 80 nm, which was set in order to match the measured penetration depth of the laser radiation in the photoresist and facilitate the subsequent processing of the substrate. The influence of the resist thickness in the spatial resolution was not evaluated at this time and will be the object of further investigation.

This proof-of-principle experiment can also be extended to demonstrate the printing of more complex two dimensional motifs, such as arrays of dots or holes. This can be realized by performing a second exposure after rotating the sample. The shape of the printed features can be altered by selecting the rotation angle and the exposure. This requires the incorporation of suitable rotation mechanisms for the sample similar to the experiment de-
scribed in [20]. Larger areas are also possible by either utilizing a transmission grating beam splitter of larger dimensions or by precisely translating the sample and realizing multiple exposures. Efforts are currently in progress in order to further develop this technique to print smaller and more complex features over larger areas using shorter wavelength lasers.

4. SUMMARY

In summary, we have demonstrated a compact EUV IL tool that combines an ADI with a desktop size EUV laser. In this proof-of-principle experiment we demonstrated the printing of gratings over areas of 2 mm × 0.6 mm with periods down to 95 nm. As the average power of the shorter wavelength (e.g., 13.9 nm) high repetition rate tabletop EUV lasers increases, their combination with this interferometer will allow the printing of arrays with a sub-10 nm feature size on a tabletop [25]. These capabilities would enable the demonstration of a practical EUV IL tool for the fabrication of large arrays of periodic features that so far were restricted to the use of large synchrotron facilities.

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