

# Lecture 6

- fixed-pt implementation
- zero-placing FIR filter design
- Linear phase filters
- FIR implementation on the DSK

## Fixed-point

ex Assume  $0 \leq |h[k]| \leq 1$   $k=0,1,\dots,N$   
4 bits of resolution

If  $h[k] = .703125$   $h[k]$  (one filter coeff)

(decimal)  $0.703125$   $\longleftrightarrow$  (binary)  $0.101101$   
 $(= \frac{1}{2} + \frac{1}{8} + \frac{1}{16} + \frac{1}{32})$

multiply by  $2^3 (=8)$   $\longleftrightarrow$  bit shift 3 bits left

$5.625$   
 $(= 4 + 1 + \frac{1}{2} + \frac{1}{8})$

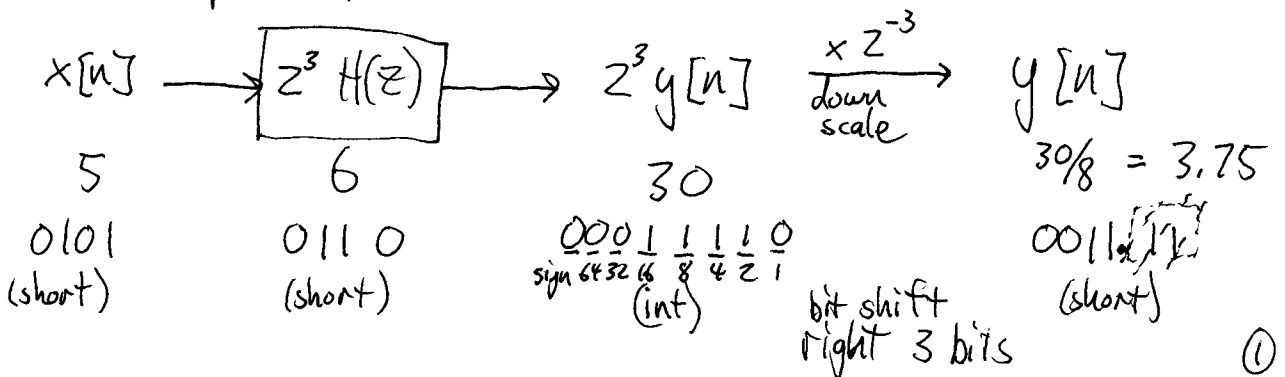
$0101.101$   
 sign bit  $\uparrow$

round to nearest integer  
 $\downarrow$   
 $6$

round to nearest integer  
 $\downarrow$   
 $0110$

NB:  $\text{round}(5.625) = \text{floor}(5.625 + 0.5) = \text{floor}(6.125) = 6$   
 $\text{round}(0101.101) = \text{floor}(5 + 0.1) = \text{floor}(5.1) = 5$   
 $= \text{floor}(0110.000) = 0110$

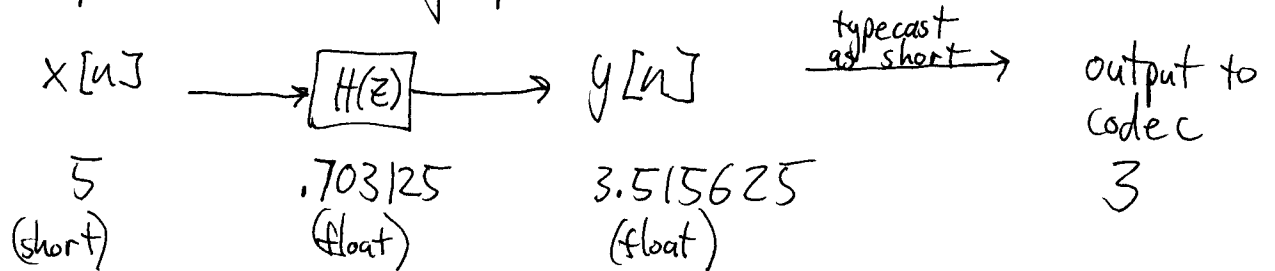
## fixed-pt. implementation



At the output,  $y[n]$  is cast as a short, so the output to the fixed-pt codec is

$$y[n] = 3$$

Compared to floating-point



On the DSK

(fixed)

- 16-bits of resolution (one sign bit) (short)
- scale filter coeff.  $h[k]$  by  $2^{15}$  → fixed-pt arithmetic
- ~~filtered~~ output stored in 32-bit int.
- output sent to codec scaled by  $2^{-15}$  (bit shift 15 places to the right or  $(output \gg 15)$  in C) and typecasted as a 16-bit short

(floating-pt)

- 32-bit IEEE floating-pt (~6 decimal places)
- floating-pt arithmetic
- filter output store in 32 bit float
- output sent to codec typecasted as a 16-bit short

## Zero-placing FIR design

$$h[k] \text{ real} \longleftrightarrow H(e^{j\omega t_0}) = \overline{H(e^{-j\omega t_0})}$$

$$H(z) \stackrel{\text{or}}{=} \overline{H(z^{-1})}$$

Implies that the poles and zeros of  $H(z)$  must appear in complex conjugate pairs, or they must be real (i.e.  $\omega = 0, \pm \frac{\pi}{2}$ ).

To place a zero at  $\omega = \omega_1$ ,

$$\begin{aligned} H_1(z) &= (1 - e^{j\omega_1 t_0} z^{-1})(1 - e^{-j\omega_1 t_0} z^{-1}) \\ &= 1 - e^{j\omega_1 t_0} z^{-1} - e^{-j\omega_1 t_0} z^{-1} + z^{-2} \\ &= 1 - z \left( \frac{e^{j\omega_1 t_0} + e^{-j\omega_1 t_0}}{z} \right) z^{-1} + z^{-2} \end{aligned}$$

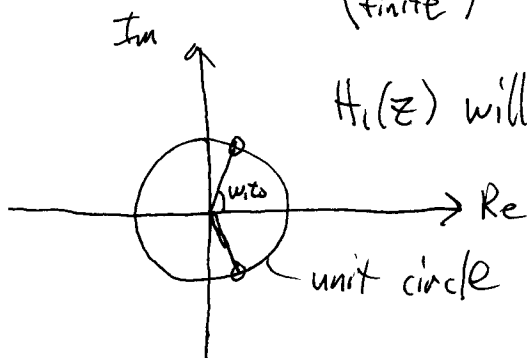
$$= 1 - 2 \cos(\omega_1 t_0) z^{-1} + z^{-2}$$

$$= h_1[0] + h_1[1] z^{-1} + h_1[2] z^{-2}$$

$$\text{(Recall } H(z) = \sum_{k=0}^N h[k] z^{-k} = h[0] + h[1] z^{-1} + \dots + h[N] z^{-N} \text{)}$$

(assuming  
causality  
and  
finite)

(Notch Filter)



$H_1(z)$  will zero out inputs of the form  $A \cos(\omega_1 t + \phi)$

Transfer Function zeros.

$$\begin{aligned} \text{Let } H_i(z) &= (1 - r_i e^{j\omega_i t_0} z^{-1}) (1 - r_i e^{-j\omega_i t_0} z^{-1}) \\ &= 1 - 2r_i \cos(\omega_i t_0) z^{-1} + r_i^2 z^{-2} \end{aligned}$$

$r_i < 1$       minimum-phase zero

$r_i = 1$       true zero (notch)

$r_i > 1$       non-minimum phase zero

To place more than one zero in a transfer function create

$$H(z) = \underbrace{H_1(z) H_2(z) H_3(z) \dots}_{\text{multiply out polynomials}}$$

Design

Coded in MATLAB

$$H_1(z) = 1 - 2r_1 \cos(\omega_1 t_0) z^{-1} + r_1^2 z^{-2} \iff h1 = [1 - 2r_1 \cos(\omega_1 t_0) \quad r_1^2]$$

$$H_2(z) = 1 - 2r_2 \cos(\omega_2 t_0) z^{-1} + r_2^2 z^{-2} \iff h2 = [1 - 2r_2 \cos(\omega_2 t_0) \quad r_2^2]$$

$$\text{Then, } H(z) = H_1(z) H_2(z) \iff h = \text{conv}(h1, h2);$$

↑  
filter coefficients stored  
in the row vector h

(show design example)

$$\text{NB: In } \cos(\omega_i t_0) \quad \omega_i t_0 = 2\pi f_i t_0 = 2\pi \frac{f_i}{f_0}$$

```
% Zero-placing example coded in MATLAB
r1 = 1.1; % non-minimum phase
r2 = .8; % minimum phase
r3 = 1; % notch

f1 = 1000;
f2 = 2000;
f3 = 3000;

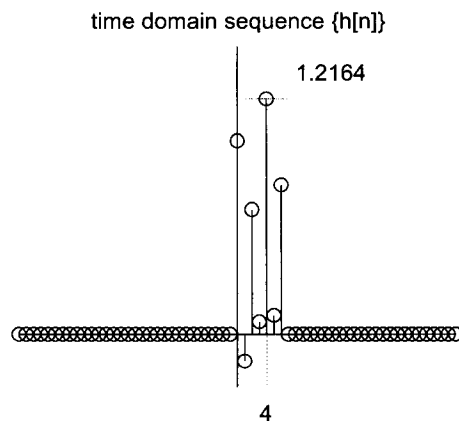
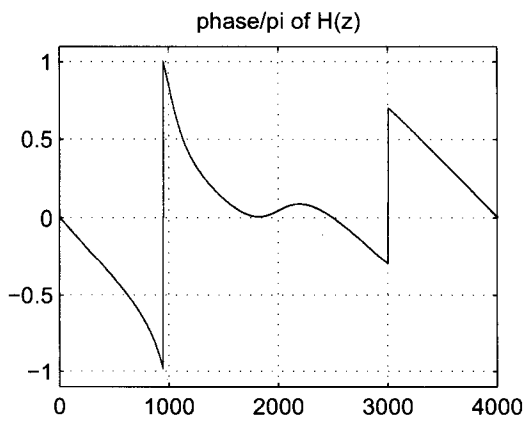
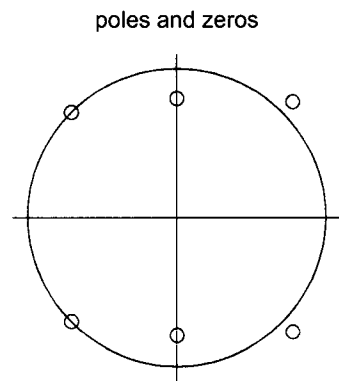
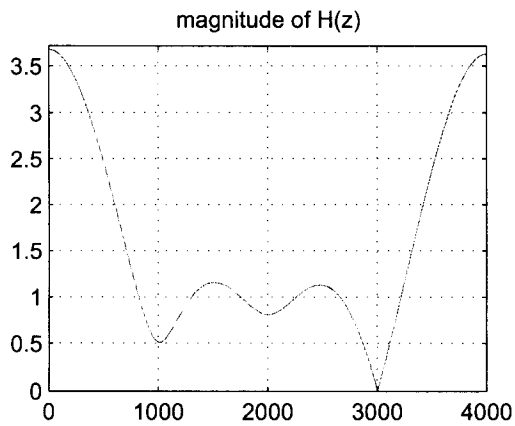
f0=8000;

h1=[1 -2*r1*cos(2*pi*f1/f0) r1^2];
h2=[1 -2*r2*cos(2*pi*f2/f0) r2^2];
h3=[1 -2*r3*cos(2*pi*f3/f0) r3^2];

h = conv(h1,h2);
h = conv(h,h3);

plotZTP_FIR(h,8000)
```

- non-minimum phase zero at 1000Hz
- minimum phase zero at 2000Hz
- zero at 3000Hz
- $H(z) = (1 - 1.1e^{j\omega_1 t_0} z^{-1})(1 - 1.1e^{-j\omega_1 t_0} z^{-1})(1 - .8e^{j\omega_2 t_0} z^{-1})(1 - .8e^{-j\omega_2 t_0} z^{-1})(1 - e^{j\omega_3 t_0} z^{-1})(1 - e^{-j\omega_3 t_0} z^{-1})$
- $\omega_1 = 2\pi * 1000\text{rad/sec}$ ,  $\omega_2 = 2\pi * 2000\text{rad/sec}$ ,  $\omega_3 = 2\pi * 3000\text{rad/sec}$ ,  $t_0 = 1/f_0$
- Sample Rate of Filter:  $f_0 = 8\text{kHz}$



## Linear Phase FIR Filters

$$\cos[\omega n t_0] \longrightarrow \boxed{H(e^{j\omega t_0})} \longrightarrow |H(e^{j\omega t_0})| \cos[\omega n t_0 + \arg\{H(e^{j\omega t_0})\}]$$

time delay of  $\tau$  seconds

$$\cos[\omega(n t_0 - \tau)] = \cos[\omega n t_0 + \theta]$$

$$\Rightarrow \theta = -\omega \tau$$

(The phasing of a cosine by  $\theta$  will delay the signal  $\tau = \frac{-\theta}{\omega}$  seconds in time)

$$\therefore \arg\{H(e^{j\omega t_0})\} = -\omega \tau$$

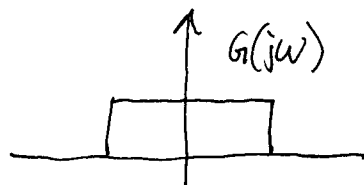
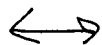
in order to ensure that all of the frequency content in the input, is shifted by the same amount in time (i.e. there is no phase distortion in the filter)

How can we guarantee a linear phase?

Recall from last time

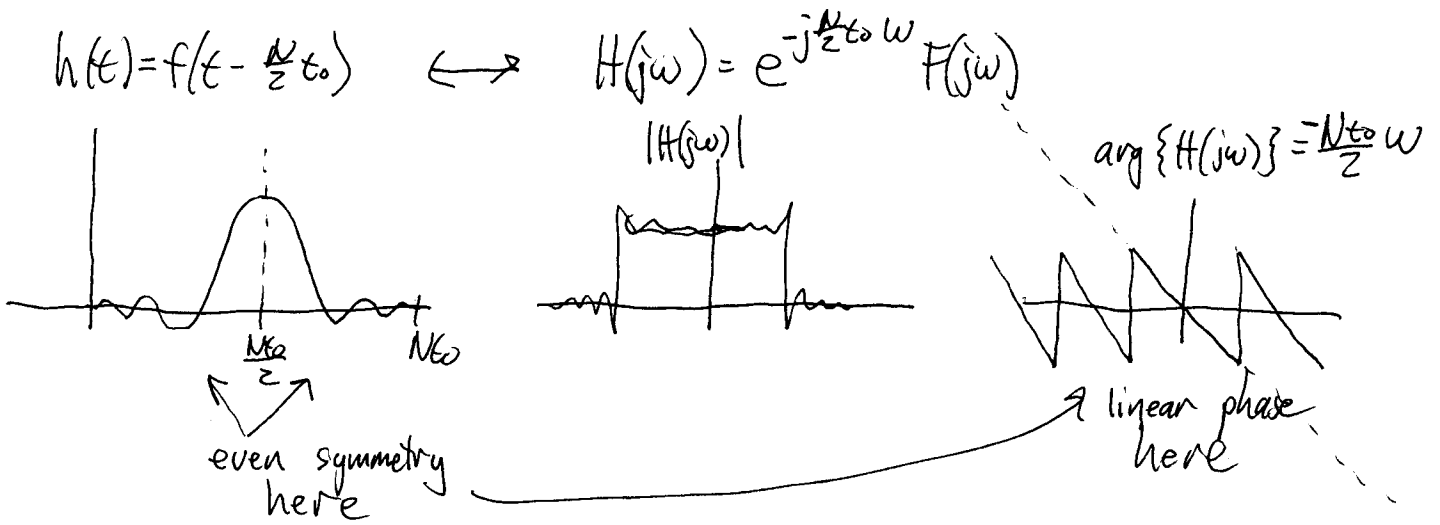
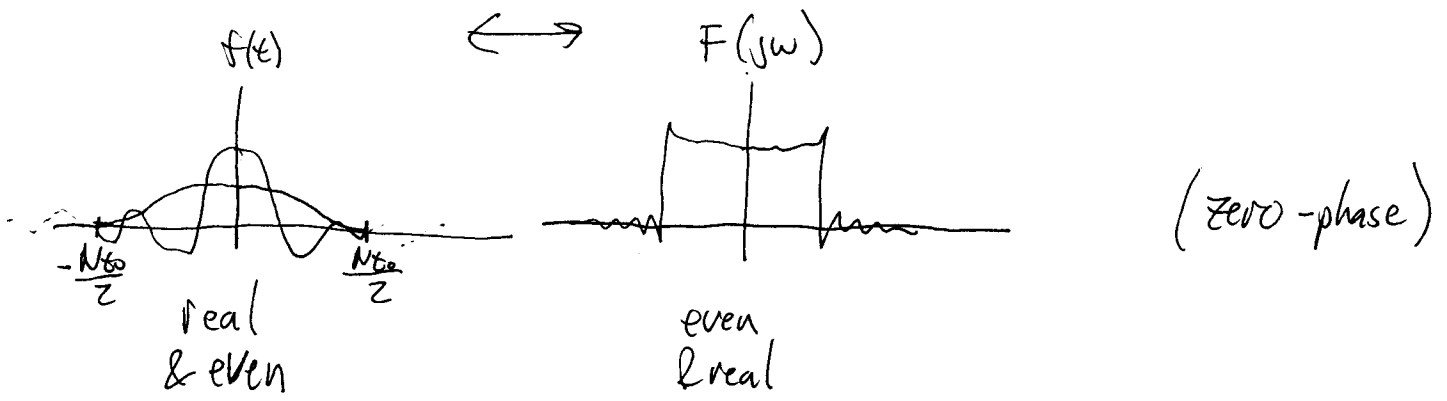


real  
& even



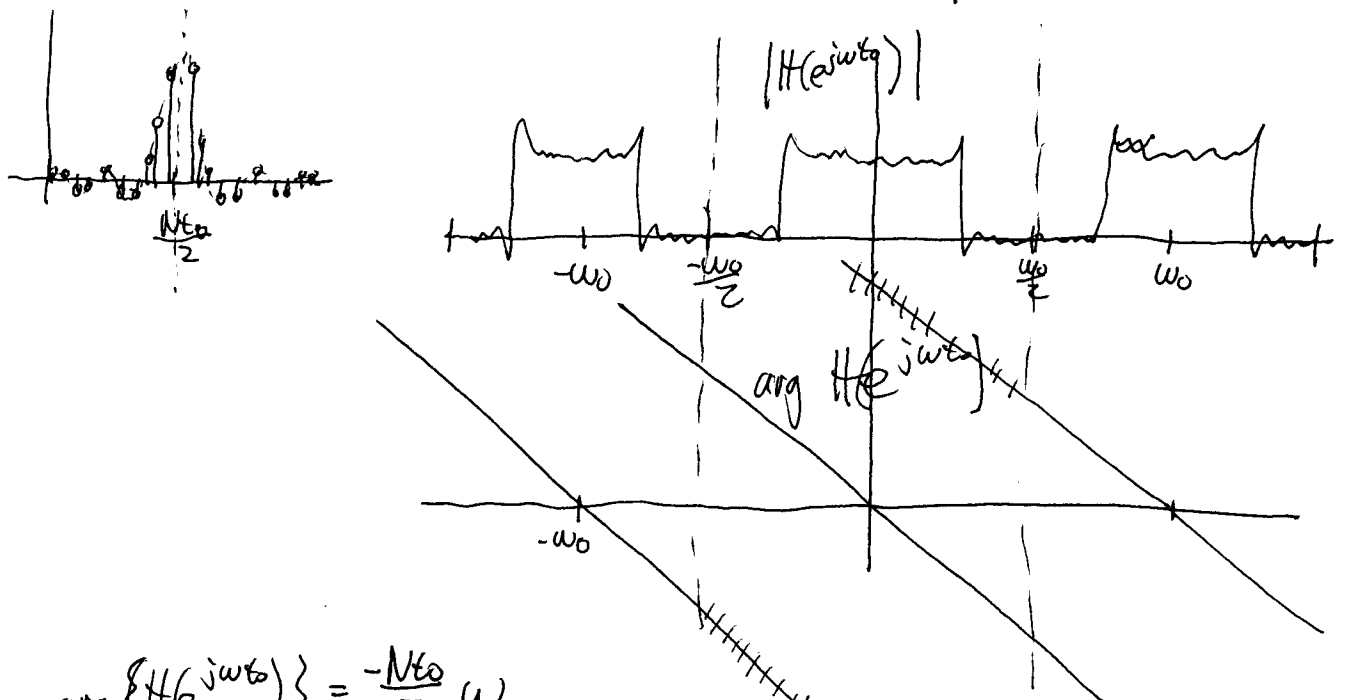
Hermitian Symmetric  
& real

$$\text{phase} = 0$$



$h[n] = t_0 h(nt_0)$

$H(e^{j\omega t_0}) = \sum_{k=-\infty}^{\infty} H(j(\omega - k\omega_0))$



$\therefore \arg\{H(e^{j\omega t_0})\} = -\frac{Nt_0}{2}\omega$   
 or delay  $\tau = \frac{Nt_0}{2}$  seconds



- linear phase results from initial zero-phase constraint and time invariance
- All causal N-order FIR filters that have even symmetry about the sample point  $N/2$  will have a (strict) linear phase.

← Differentiators and Hilbert Transformers have the phase constraint  $\arg\{G(j\omega)\} = \pm \pi/2$

$$\begin{array}{ccc}
 G(j\omega) & \longleftrightarrow & g(t) \\
 \text{(purely imaginary)} & & \text{(odd symmetry)} \\
 e^{j\omega t} = \pm j & & 
 \end{array}$$

• Same design process (with even windows) will preserve the phase constraint.

$$\text{(i.e. } \arg\{H(e^{j\omega t_0})\} = \underbrace{\pm \frac{\pi}{2}}_{\text{phase constraint}} - \underbrace{\frac{N}{2} t_0 \omega}_{\text{linear phase (required for causal implementation)}}$$

Remark: When  $\arg\{H(e^{j\omega t_0})\} = -\alpha\omega + \beta$ , the filter  $H(e^{j\omega t_0})$  is said to have a generalized linear phase where

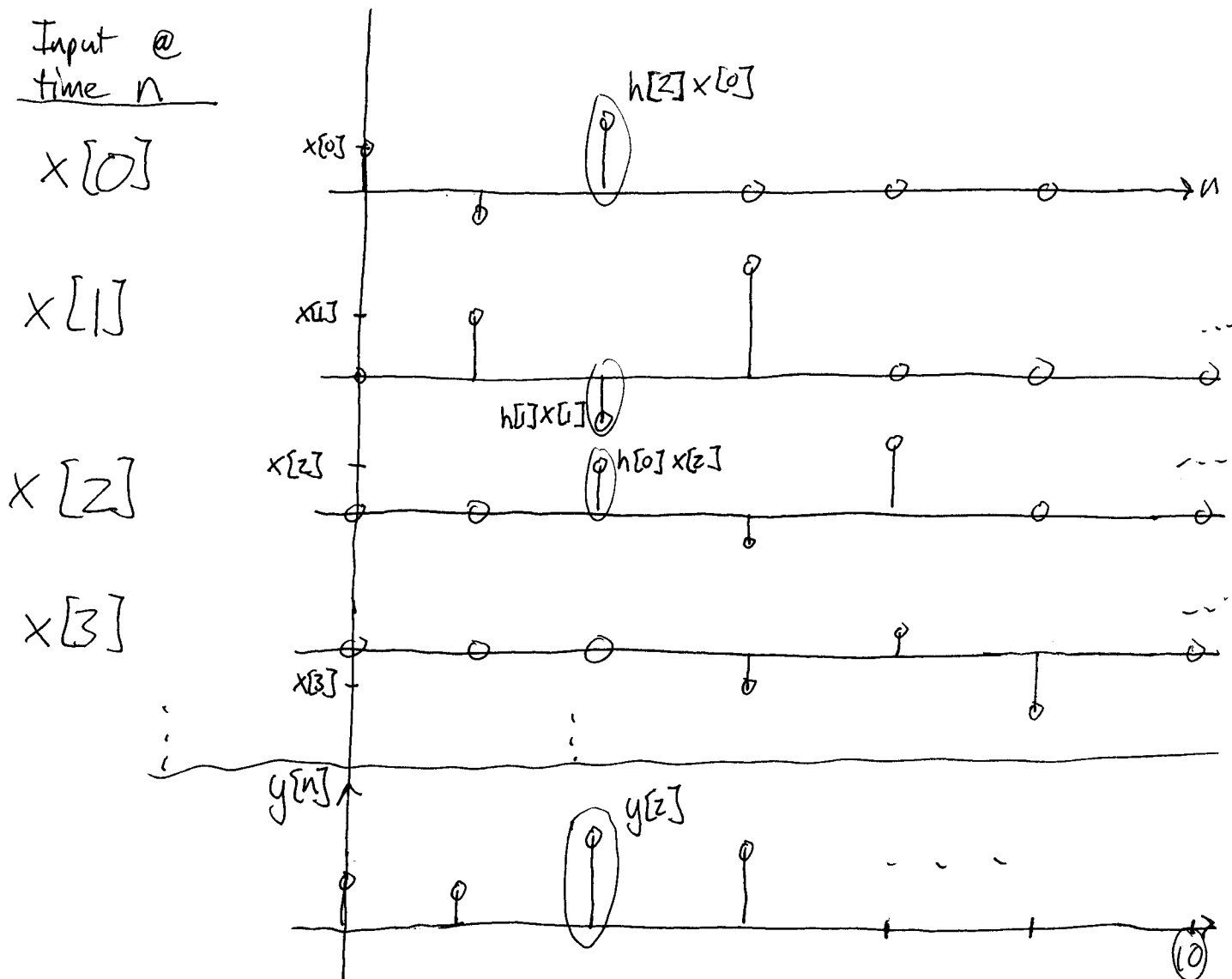
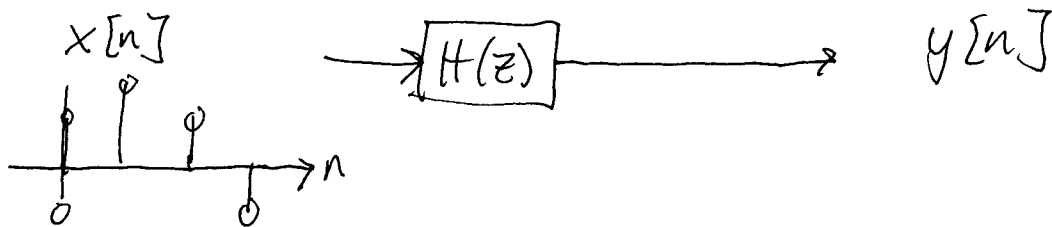
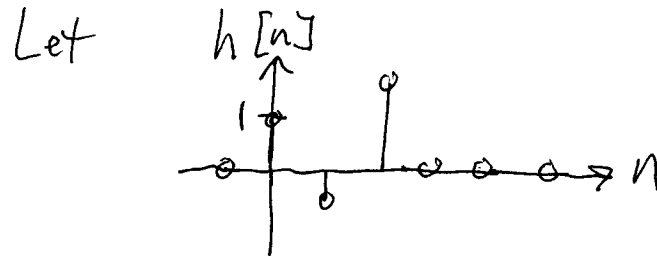
$$\begin{array}{l}
 \beta: \text{ phase constraint} \\
 \alpha: \text{ time delay associated with making it causal}
 \end{array}
 \quad
 \left( \begin{array}{l}
 \text{not a function of } \omega \\
 \beta = \beta \quad \omega > 0 \\
 \beta = -\beta \quad \omega < 0
 \end{array} \right)$$

conjugate symmetry required in  $H(e^{j\omega t_0})$

NB: When  $\beta = 0$ ,  $H(e^{j\omega t_0})$  is said to have a strict linear phase.

# FIR Filter Implementation on the DSK

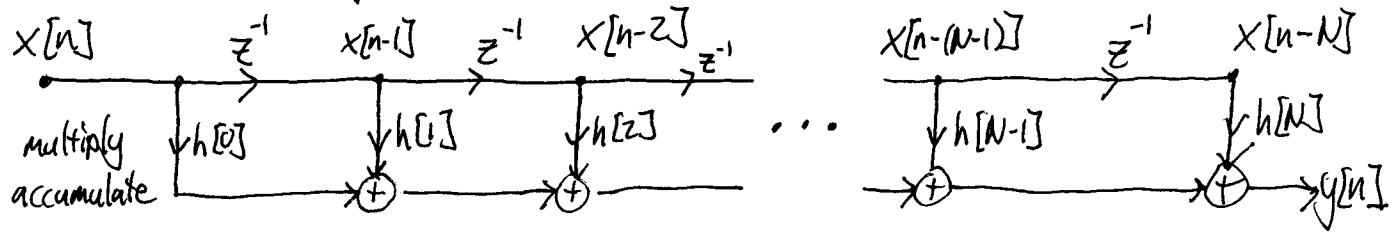
Action of a filter :



$$\therefore y[z] = h[0]x[z] + h[1]x[1] + h[2]x[0]$$
 In general, 
$$y[n] = \sum_{k=0}^N h[k]x[n-k]$$
 (convolution sum)

↑  
 Here  $N=2$

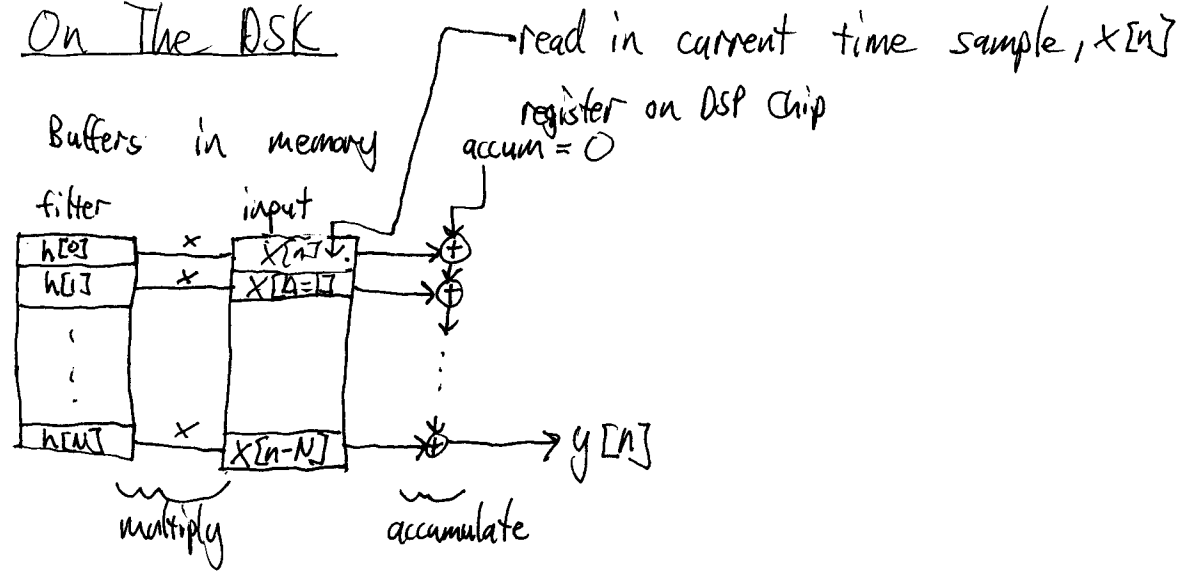
Hardware Diagram



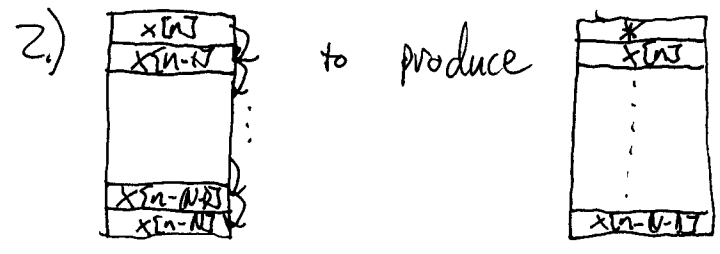
On The DSP

1.) Buffers in memory

Process



Update input buffer



At next time step (next interrupt), go to step 1, read in current time sample and repeat process