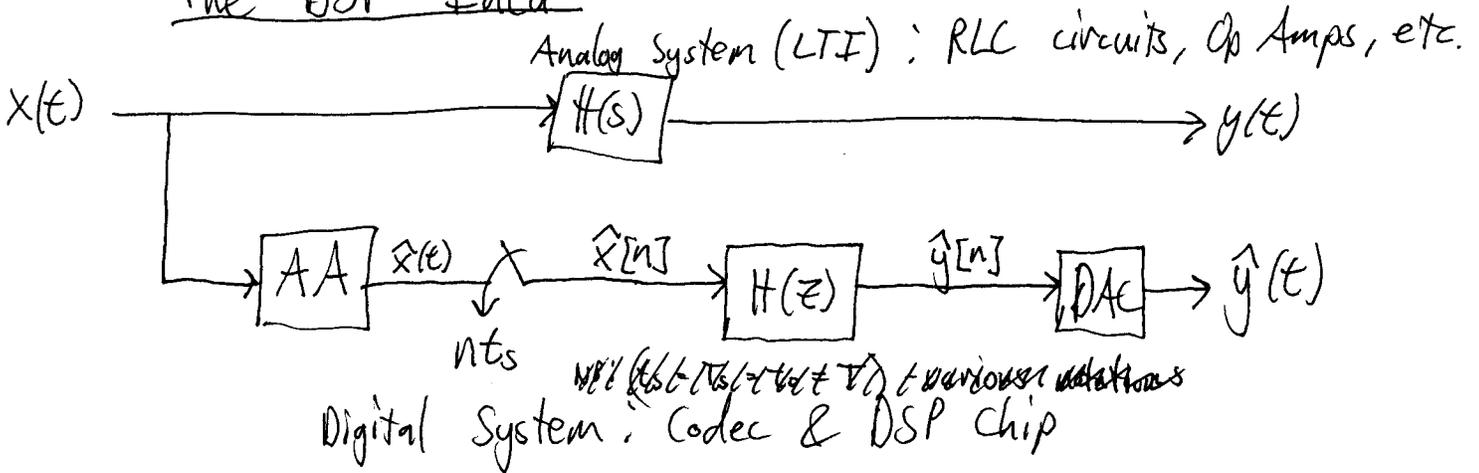


# Lecture 3 : Sampling & Reconstruction

(2 50min lect.)

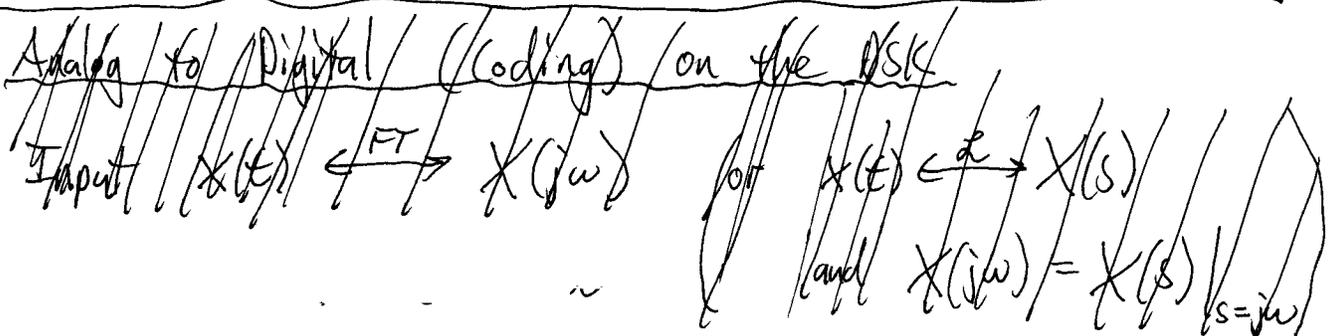
## The DSP Idea



If  $H(z) = 1$  (or  $H(s) = 1$ ) then this system implements a "straight wire". (i.e.  $y(t) = x(t)$ )

Question: Under what conditions does  $\hat{y}(t) \approx y(t)$ ?

To answer this, let's examine the above diagram in more detail.



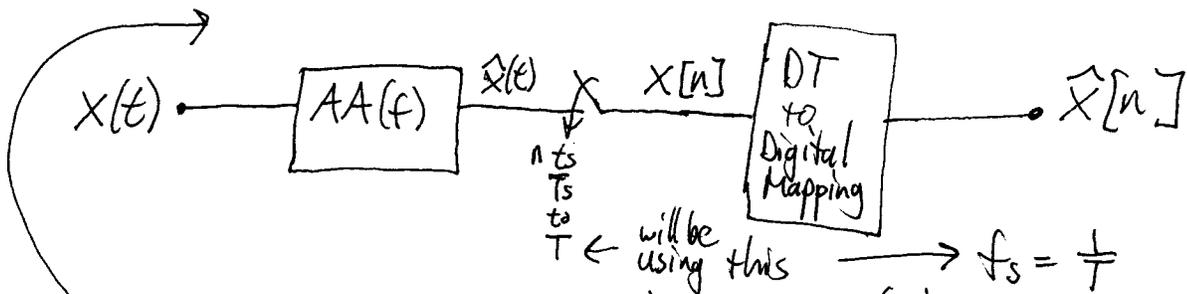
In order to process the signal digitally, the source must be bandlimited in frequency.

# The Modulator: Analog to Digital Conversion (Coding)

Analog Signal:

Discrete-Time Signal:

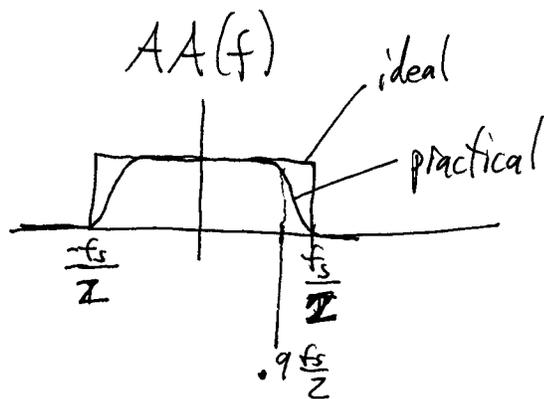
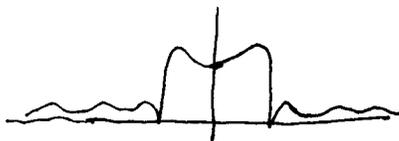
Digital Signal:



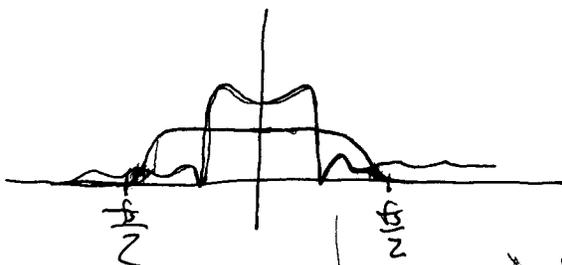
NB:  $AA(j\omega) \equiv AA(j2\pi f) \equiv AA(f)$

$\uparrow$  rad/sec                       $\uparrow$  Hz                       $\uparrow$  Hz

$X(t) \leftrightarrow X(f)$



$\hat{X}(t) \leftrightarrow \hat{X}(f)$



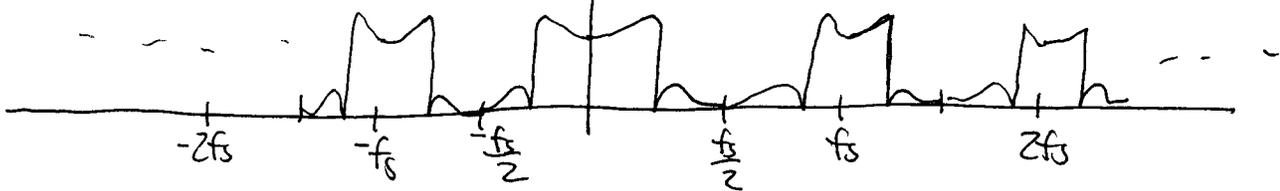
some information is lost

$$x[n] = \hat{x}(nT)$$

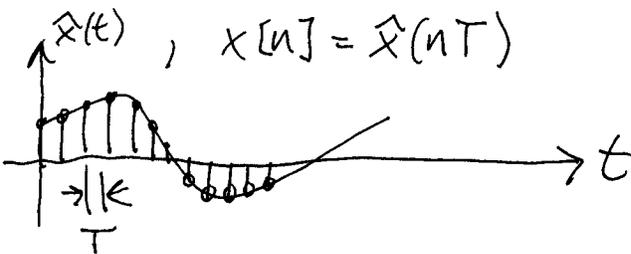
$$X(e^{jz\pi fT}) = \frac{1}{T} \sum_{k=-\infty}^{\infty} \hat{X}(f - kT) \quad \text{(Sampling Theorem)}$$

integers  
 $m \in \mathbb{Z}$

$X(e^{jz\pi fT})$  : periodic  $f = m(\frac{1}{T}) = mT_s$



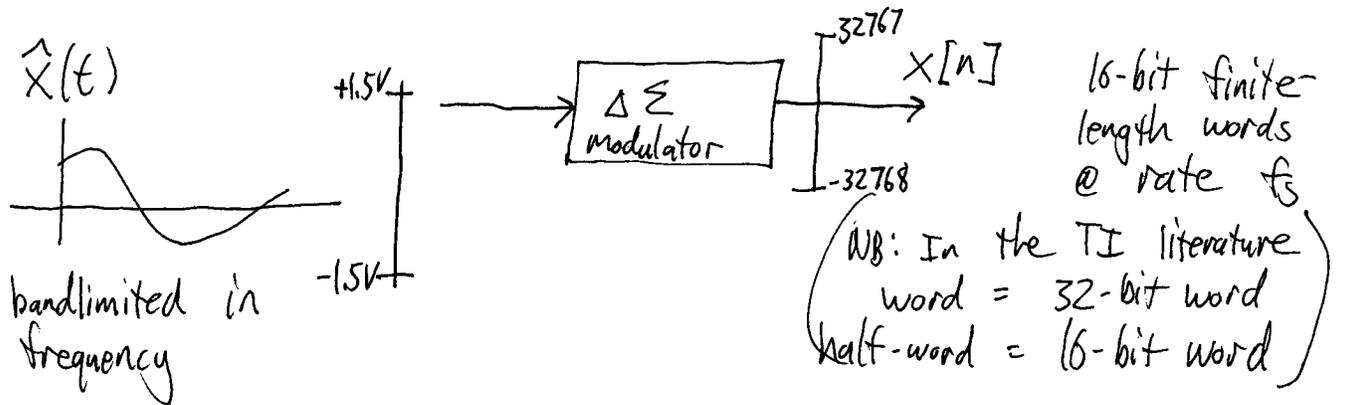
Without the AA filter, these spectra would overlap, which results in aliasing.



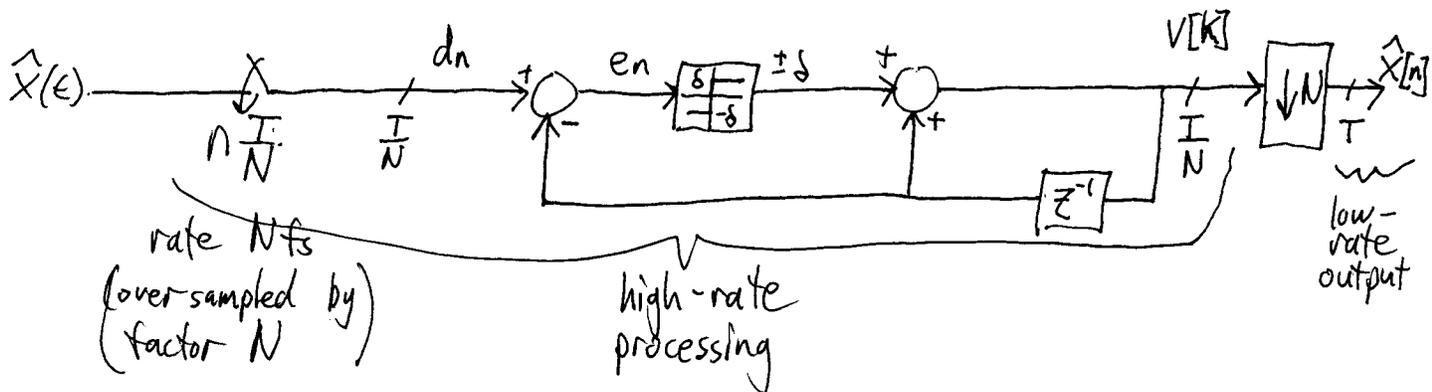
In order to represent these samples as a binary word, the discrete-time samples must be quantized to specific amplitude intervals and assigned a binary value based on quantized amplitude.



On the DSK



The Idea (not a standard model)



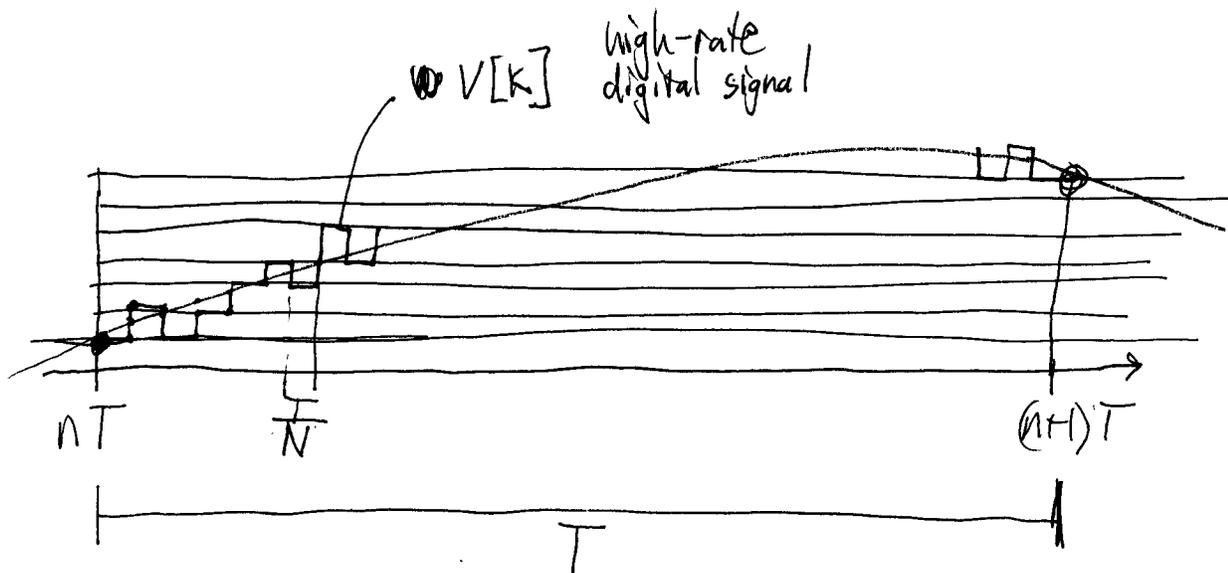
$d_n, e_n$  : DT measurement

$V[k]$  : high-rate digital signal

$\hat{X}[n]$  : low-rate digital signal output

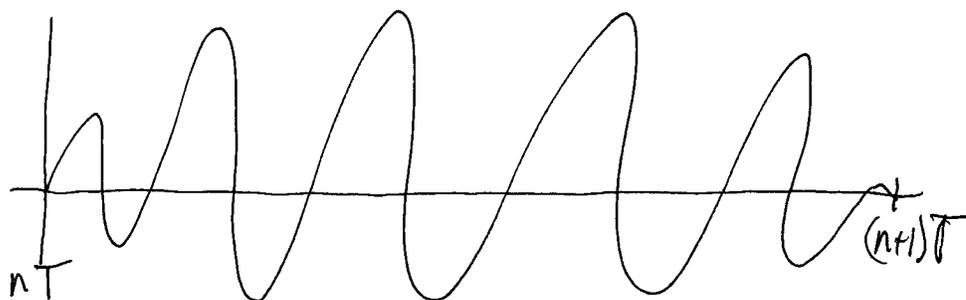
$$\hat{X}[n] = V\left[\frac{K}{N}\right] \quad \text{for } \frac{K}{N} \text{ an integer}$$

↕  
not intuitive - see picture



$$\begin{aligned}
 X[n] &= X[n-1] + \delta_1 + \delta_2 + \dots + \delta_{N-1} \\
 &= X[n-1] + \underbrace{\sum_{e=1}^{N-1} \delta_e}_{\substack{\text{sum of correction} \\ \uparrow \text{sigma} \quad \quad \uparrow \text{delta}}}
 \end{aligned}$$

Can we have?



On the DSK (standard),

$$\begin{aligned}
 \delta &= \text{one bit correction} \\
 N &= 64
 \end{aligned}$$



# Digital to Analog Conversion (Decoding)

Basic idea (theoretical)

Notation  
 $T = t_s =$  sample duration  
 $\frac{1}{T} = f_s =$  sampling frequency

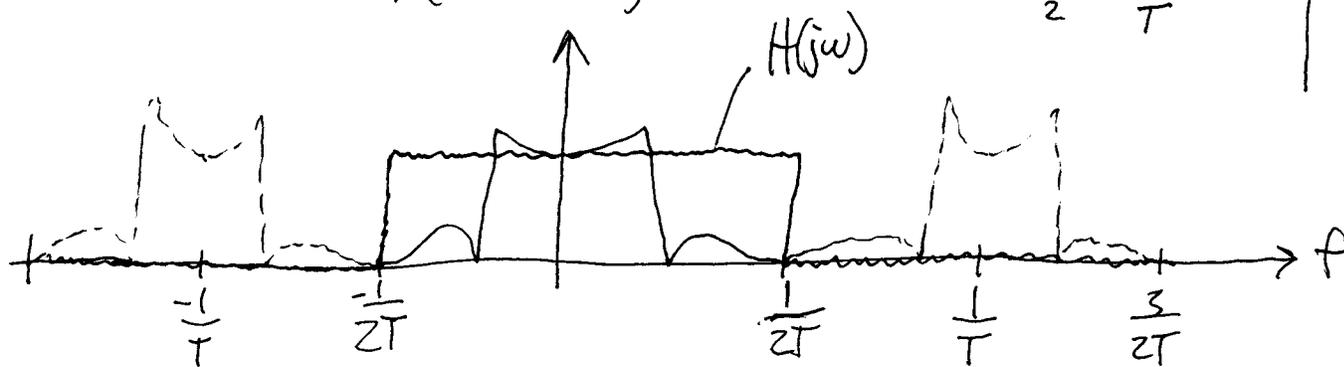


We could do this with a really good analog reconstruction filter

$$y[n] \leftrightarrow Y(e^{jz\pi f T})$$

$$Y(e^{jz\pi f T})$$

Notation	$f_z$
rad/sec	$f$
$\omega$	$\frac{1}{2T} = \frac{f_s}{2}$
$\frac{\omega}{2} = \frac{\pi}{T}$	



$$H(j\omega) = \begin{cases} 1 & |\omega| \leq \frac{1}{2T} \\ 0 & |\omega| > \frac{1}{2T} \end{cases} \longleftrightarrow h(t) = \text{sinc}\left(\frac{\pi t}{T}\right)$$

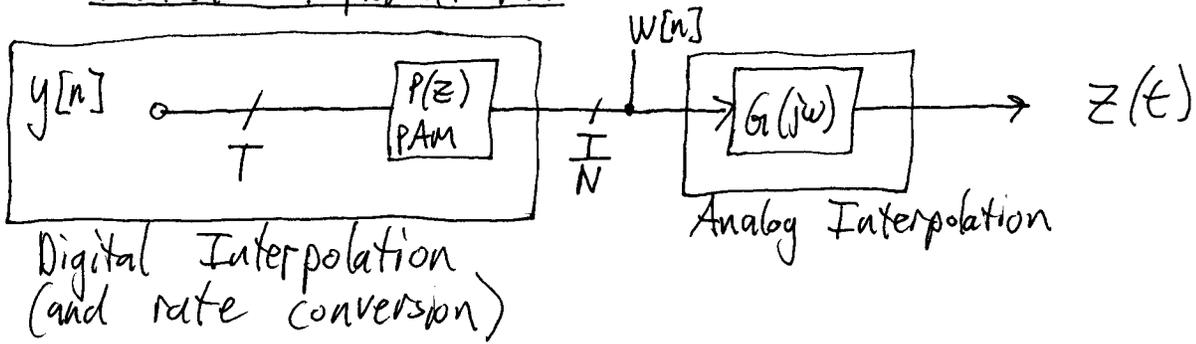
$$z(t) = \sum_{k=-\infty}^{\infty} y[k] h(t - kT) \longleftrightarrow Z(j\omega) = H(j\omega) Y(e^{jz\pi f T})$$

(see sig & sys Lab 10 ~~the~~ Figure 3 for a time domain plot of this)

Problems: Building  $H(j\omega)$  is impossible.

Approximating  $H(j\omega)$  is expensive (no room for roll-off)

practical implementation



Comments:  $y[n]$  : digital signal @ rate  $\frac{1}{T}$  samples/sec

$w[n]$  : digital signal @ rate  $\frac{N}{T}$  samples/sec.

$z(t)$  : reconstructed analog signal that is (approximately) bandlimited to  $\frac{1}{2T}$  Hz.

$y[n] \longleftrightarrow Y(e^{jz\pi fT})$  - periodic in frequency with period  $\frac{1}{T}$  Hz.

$w[n] \longleftrightarrow W(e^{jz\pi f\frac{T}{N}})$  - periodic in frequency with period  $\frac{N}{T}$  Hz.

$z(t) \longleftrightarrow Z(z\pi f)$  (or  $Z(f)$ ) - NOT periodic in frequency  
 $Z(j\omega) \approx 0 \quad |\omega| > \frac{1}{2T}$

NB: remember  $\begin{matrix} \text{time} \\ \text{(frequency)} \end{matrix} \longleftrightarrow \begin{matrix} \text{frequency} \\ \text{(time)} \end{matrix}$

$\begin{matrix} \text{periodic} \\ \text{discrete} \end{matrix} \longleftrightarrow \begin{matrix} \text{discrete} \\ \text{periodic} \end{matrix}$

Working backwards, mathematically

Analogy Interpolation

$$z(t) = \sum_{k=-\infty}^{\infty} w[k] g(t - kT)$$

(assuming causality)  
( $w[k] = 0$  for  $k < 0$ )

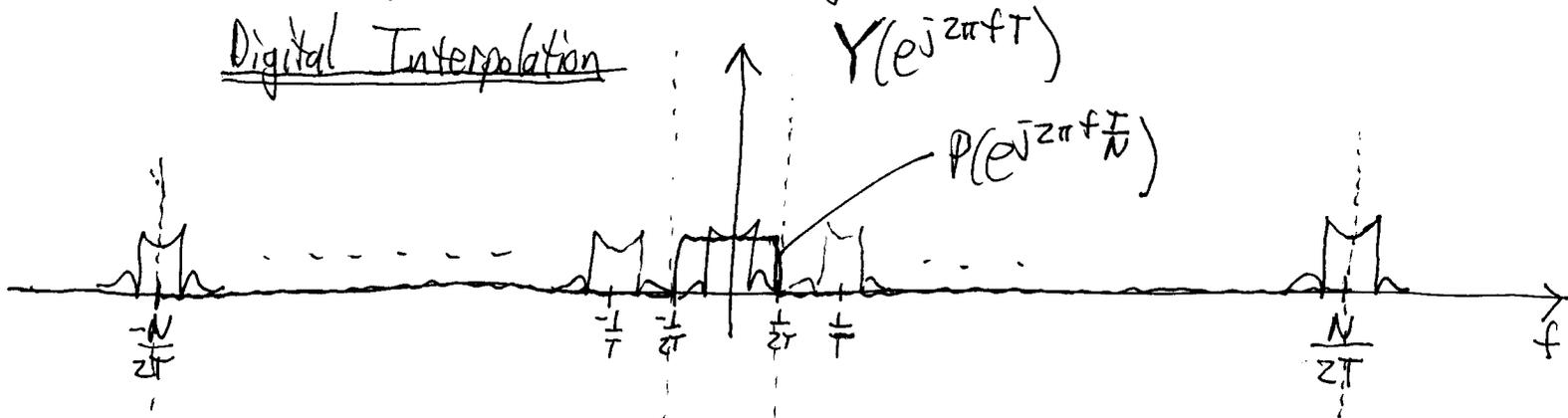
$$= \sum_{k=0}^{\infty} w[k] g(t - kT) = W(e^{j2\pi f T}) G(j2\pi f) = Z(f)$$

Digital Interpolation

$$w[n] = \sum_{k=0}^{\infty} y[k] p[n - kN] \leftrightarrow Y(e^{j2\pi f T}) P(e^{j2\pi f T}) = W(e^{j2\pi f T})$$

Working forwards pictorially in frequency

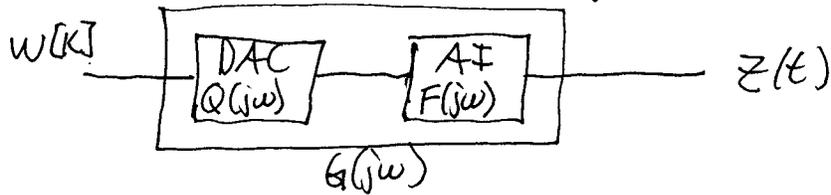
Digital Interpolation



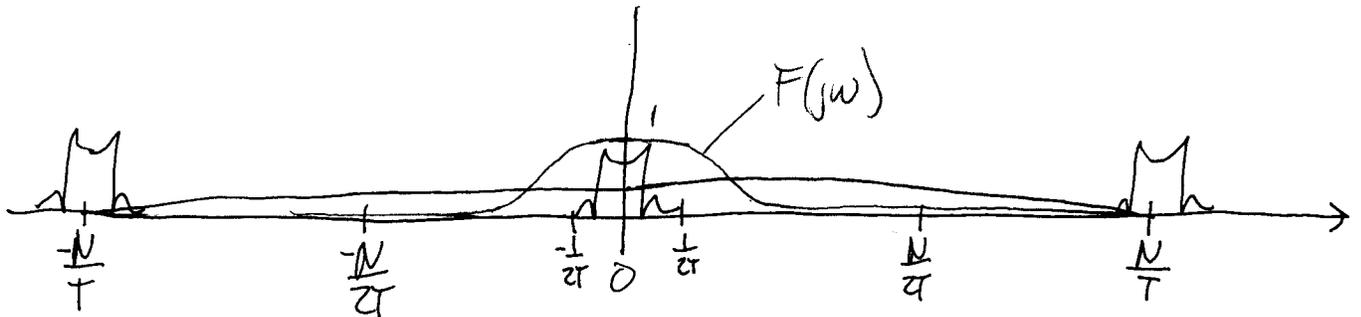
$P(e^{j2\pi f T})$  is linear phase (digital) FIR filter, which means that there will be no "phase distortion" from this filter. (Later in Lab 4)

## Analog Interpolation

Note  $G(j\omega)$  is actually two filters



$$G(j\omega) = F(j\omega)Q(j\omega) \longleftrightarrow g(t) = (f * q)(t)$$

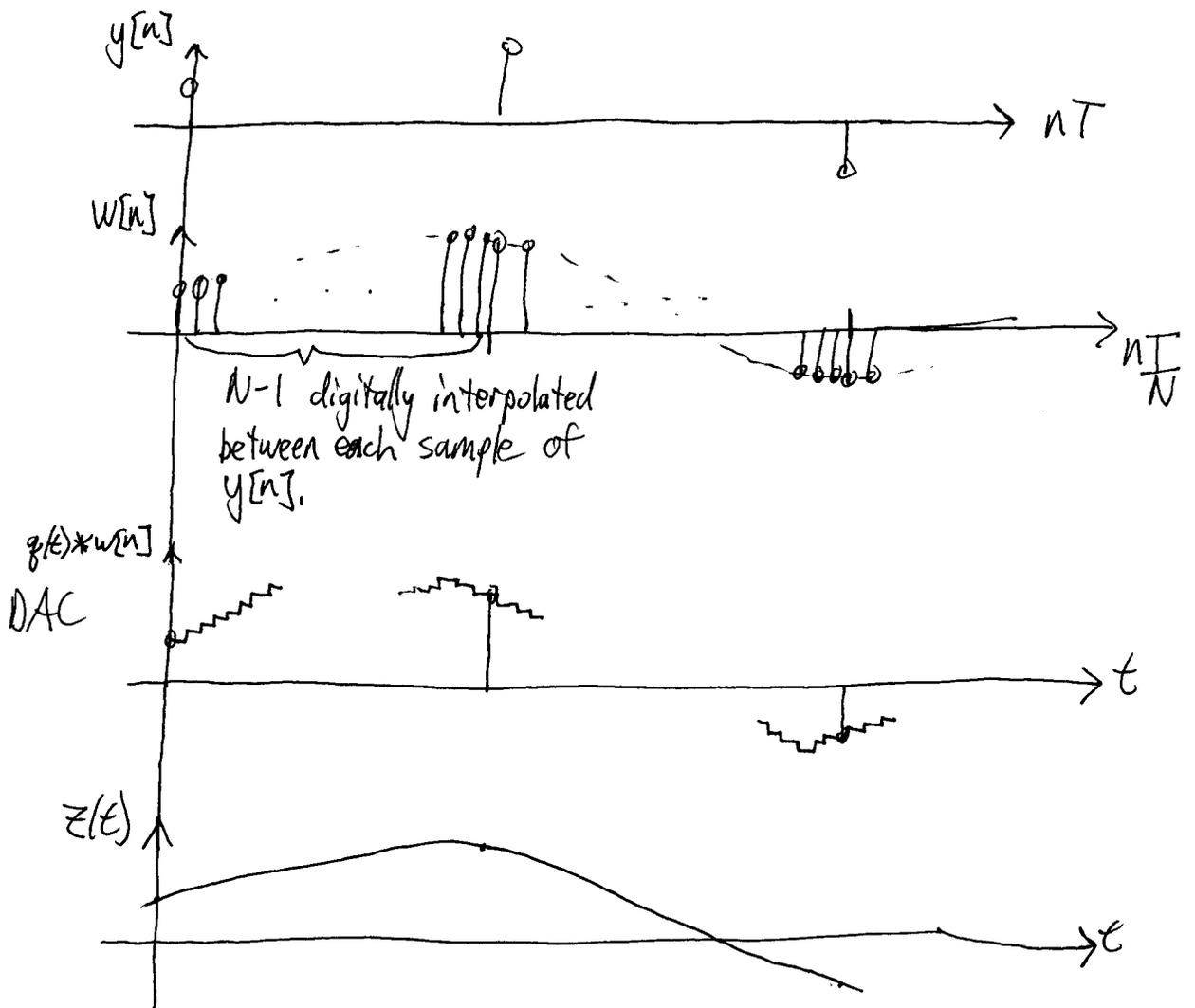


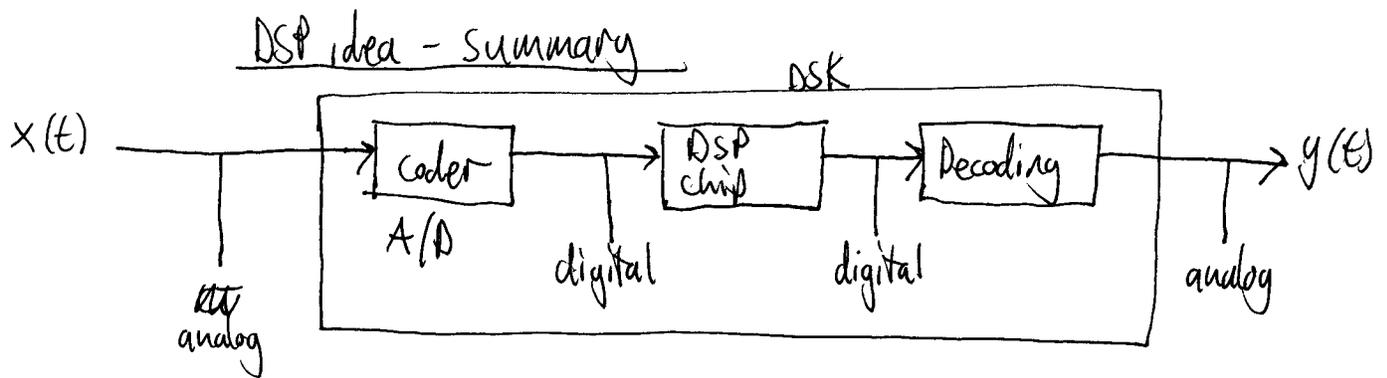
$$q(t) = \begin{cases} 1 & 0 \leq t \leq \frac{N}{T} \\ 0 & \text{o.w.} \end{cases} \longleftrightarrow Q(j\omega) = \frac{T}{N} e^{j2\pi f \frac{N}{2}} \text{sinc}\left(\pi f \frac{T}{N}\right)$$

zero-order hold (zoh)

$$F(j\omega) \approx 1, \quad |f| < \frac{1}{2T}$$

In the time domain





Comments:

- A/D & D/A (coding & decoding) done by the codec (a single chip located on the DSK board)
- $y(t) \approx \hat{y}(t)$  (from before) when  $x(t)$  is approximately bandlimited to the half sampling frequency.
  - In real applications,  $f_s$  would be a design parameter. However, in this class,  $f_s$  will be fixed.
- DSP chip implements the ~~algorithm~~ digital algorithm. This algorithm may be
  - LTI ( $H(z)$ ), or
  - NLTV (non-linear time varying)
- In Lab 2, when F0 is performed, the DSP chip will be used as a straight wire (i.e.  $H(z)=1$ ). For Labs 4-6, the DSP chip will be an LTI filter  $H(z)$ . In Lab 7, the DSP chip will be used to implement general NLTV ~~eg~~ communication systems