

# Rivers and Dams

An aerial photograph of a large dam and reservoir. The dam is a long concrete structure with several spillways. The reservoir is a large body of water that fills a valley. In the background, there are rolling hills and mountains. The foreground shows a road and some buildings near the dam.

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Colorado State University

**USBR Lectures – Part III**

Denver, Colorado

January 18, 2024

# USBR Short Course

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1. Watersheds and Climate
2. Sedimentation Engineering
3. **Rivers and Dams**
4. River Environment



# Rivers and Dams

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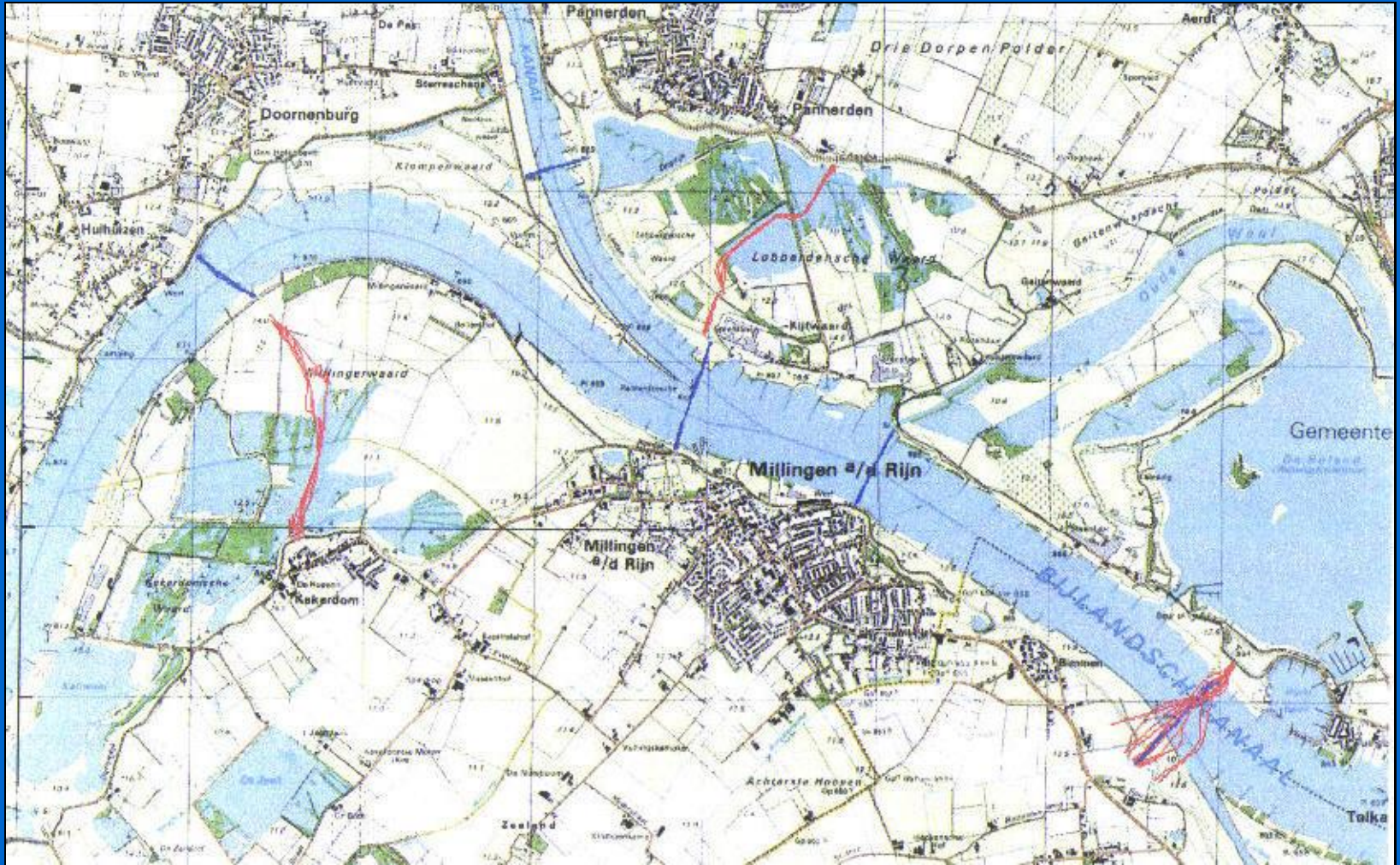
- 1. River Equilibrium**
- 2. Aggradation**
- 3. Degradation below Dams**
- 4. Case Study Gupo Bridge**
- 5. Case Study Dam Break**



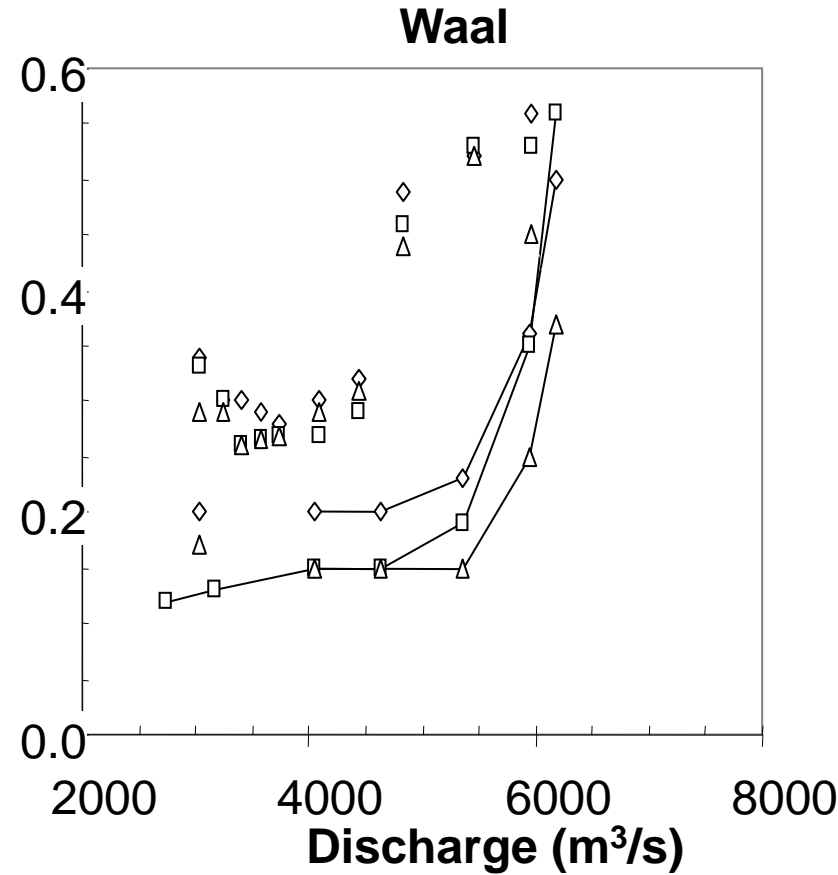
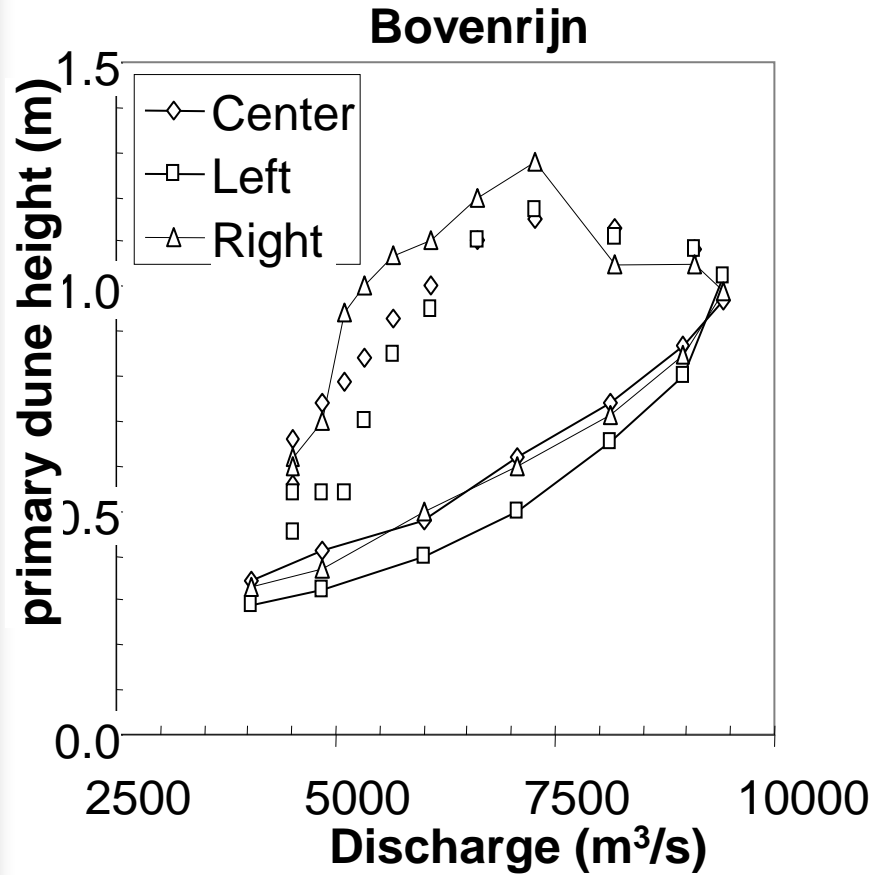
# 1a. Manning n

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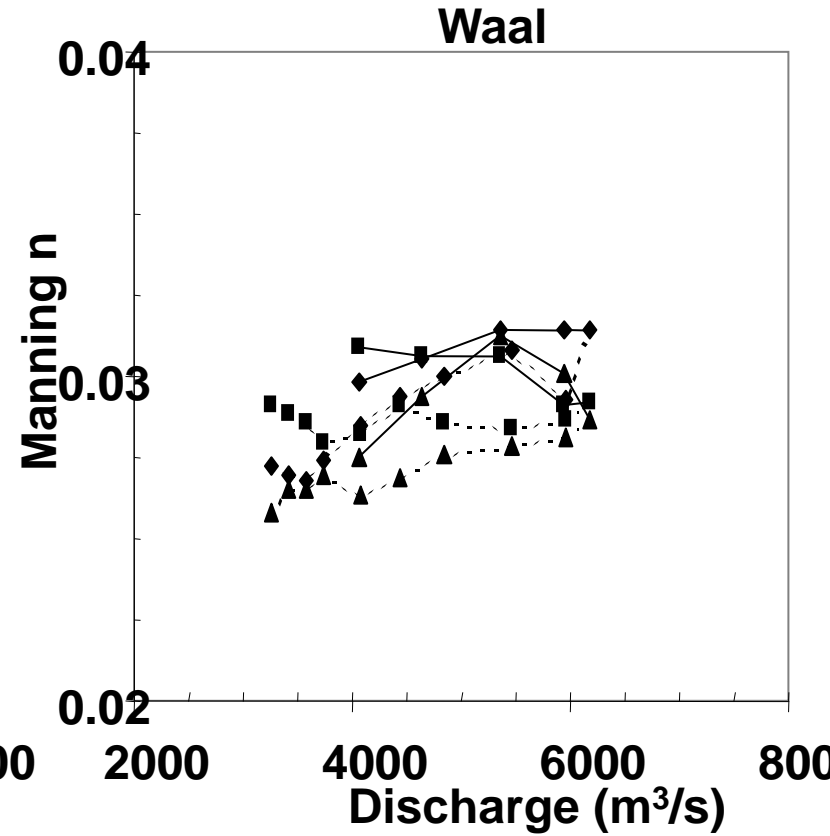
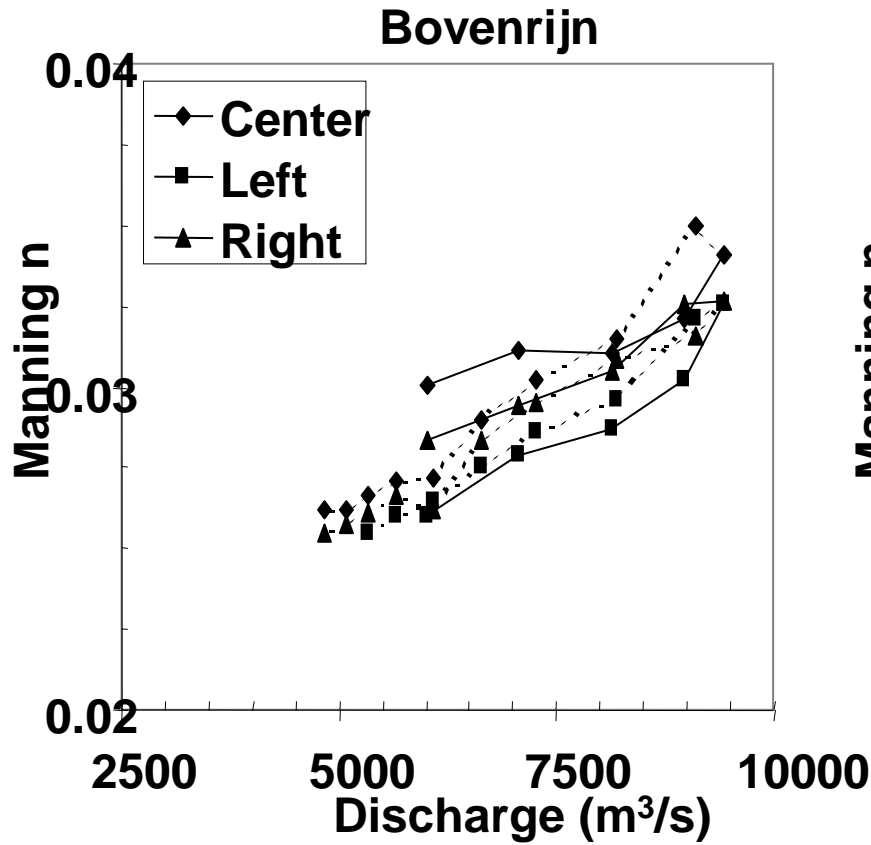
# Rhine River flood in 1998



# Primary dune height vs discharge



# Manning n vs discharge

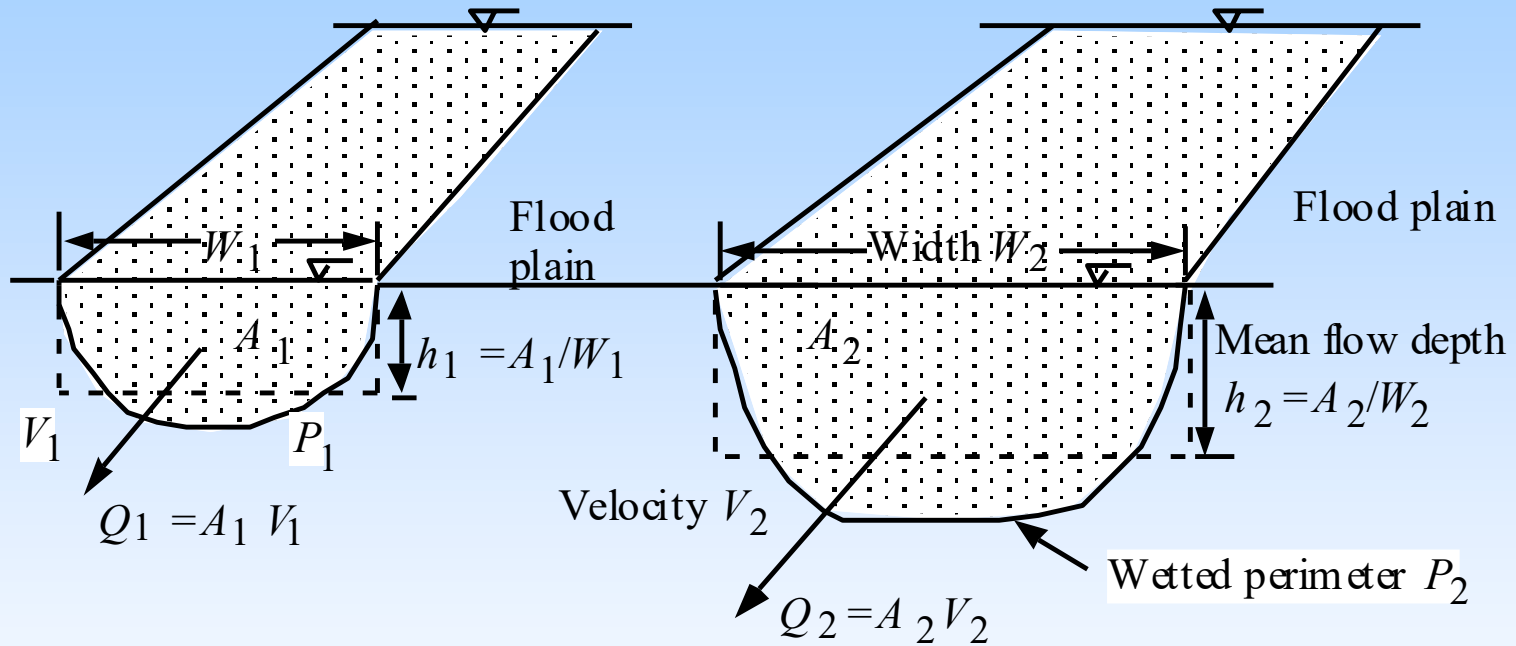


# 1b. Downstream Hydraulic Geometry

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# Downstream Hydraulic Geometry



# Julien-Wargadalam (J-W) Equations

When the Manning-Strickler approximation is applicable, i.e.  $m = 1/6$ , a simplified form of Eqs. (10.19) is obtained in SI as

$$h \approx 0.133 Q^{0.4} \tau_*^{-0.2} \quad (10.20a) \blacklozenge$$

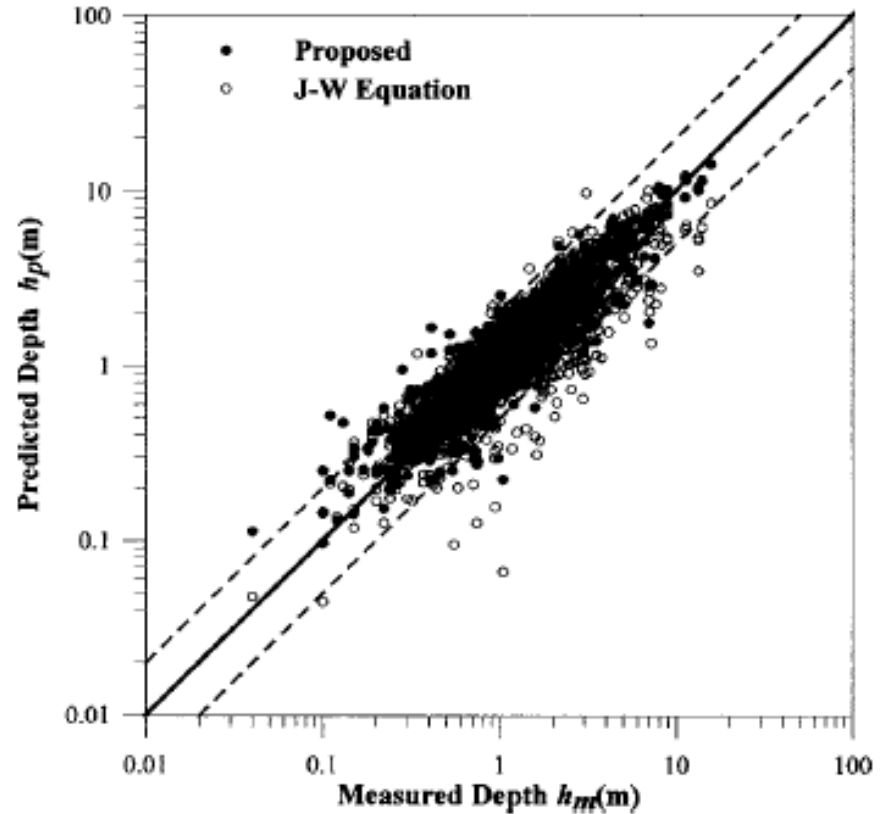
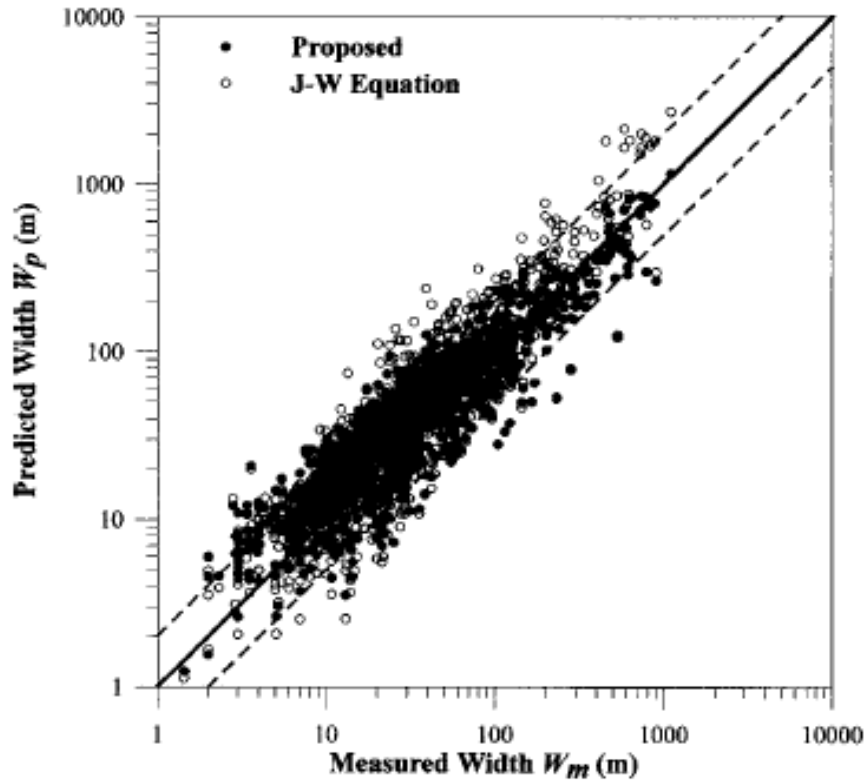
$$W \approx 0.512 Q^{0.53} d_s^{-0.33} \tau_*^{-0.27} \quad (10.20b) \blacklozenge$$

$$V \approx 14.7 Q^{0.07} d_s^{0.33} \tau_*^{0.47} \quad (10.20c) \blacklozenge$$

$$S \approx 12.4 Q^{-0.4} d_s \tau_*^{1.2} \quad (10.20d) \blacklozenge$$

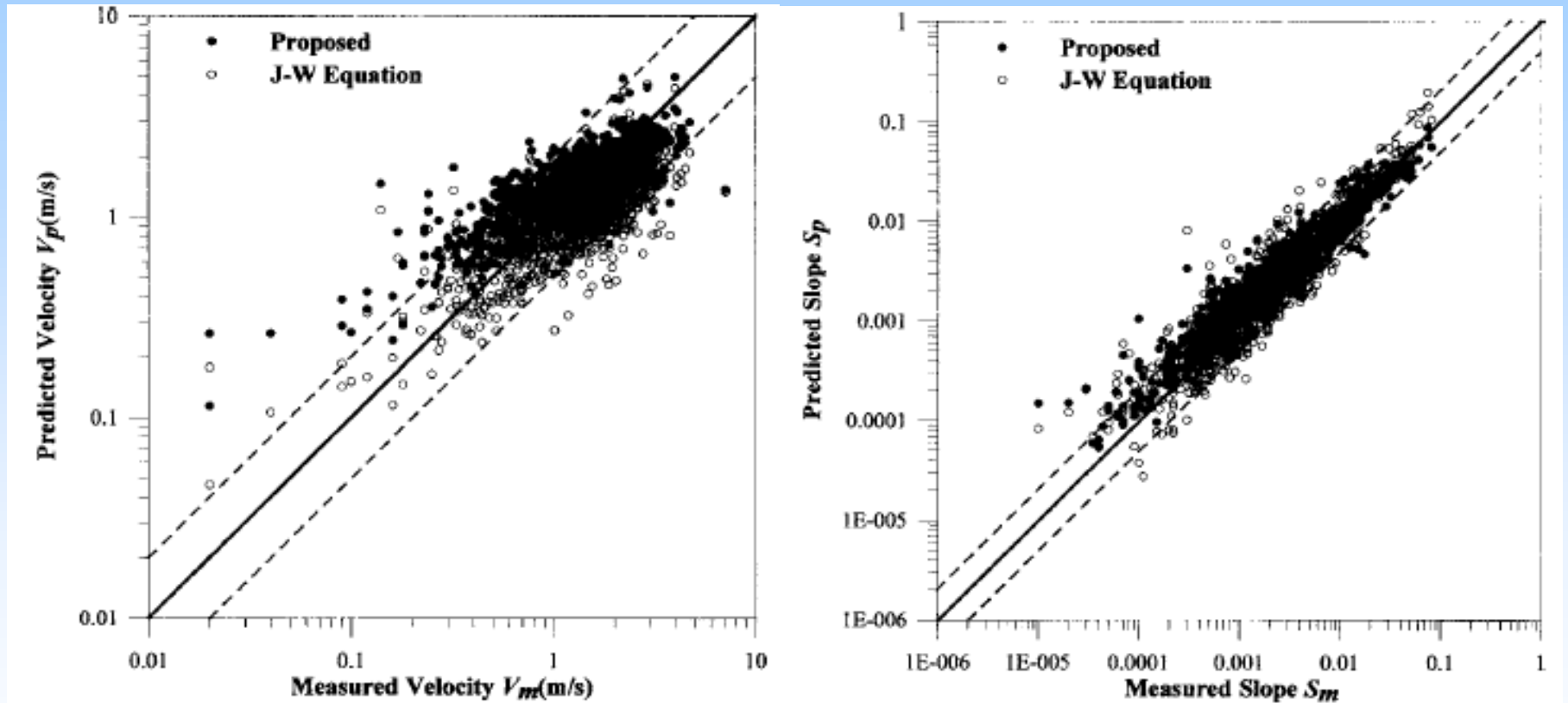
The hydraulic geometry of stable channels is obtained from Eqs. (10.20) when  $\tau_* \cong 0.047$ . Higher sediment transport rates require higher velocity and slope, and reduced width and depth.

# Bankfull width and depth



from Julien and Wargadalam (ASCE-JHE, 1996)

# Bankfull velocity and slope



from Julien and Wargadalam (ASCE-JHE, 1996)

# 1c. Meandering

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# Sediment Transport in Sharp Bends

Laboratory experiments show that fine sand can deposit where coarse sand cannot, i.e. point bars

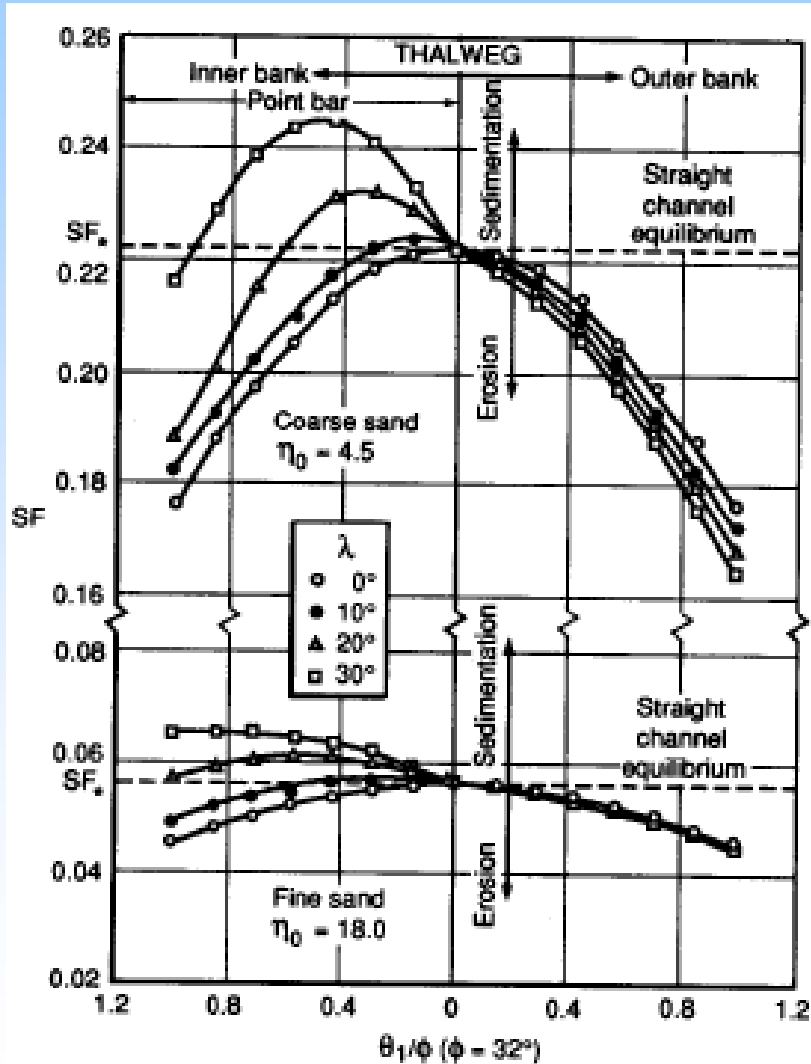
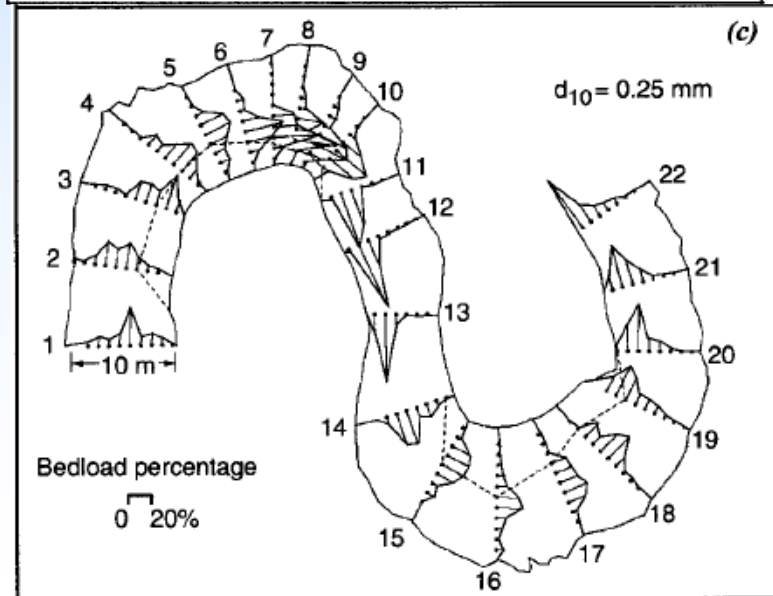
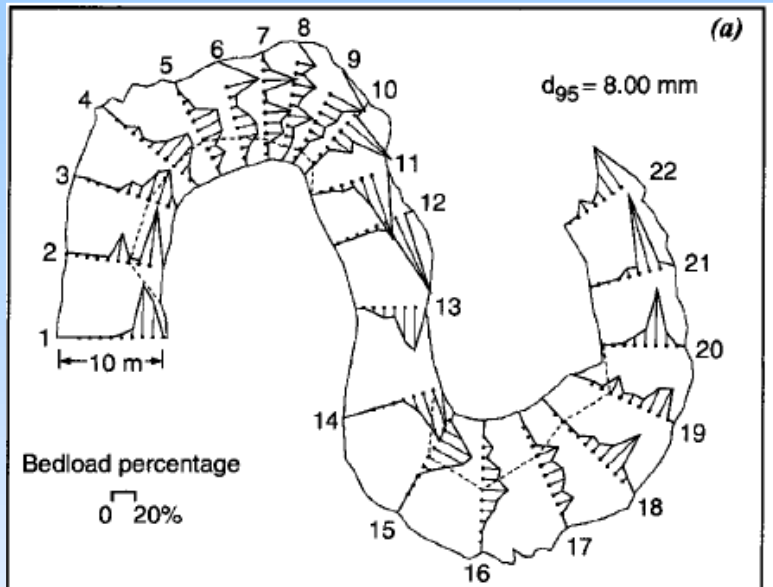


Fig. 3. Relation between  $SF$  and  $\theta_1/\phi$  ( $M/N = 1$ ).



from Kawai and Julien (JHR-IAHR, 1996)

# Sediment Transport in Sharp Bends



Field measurements in the sharp bends of the Fall River, Colorado demonstrate that particles of different sizes move in different directions.

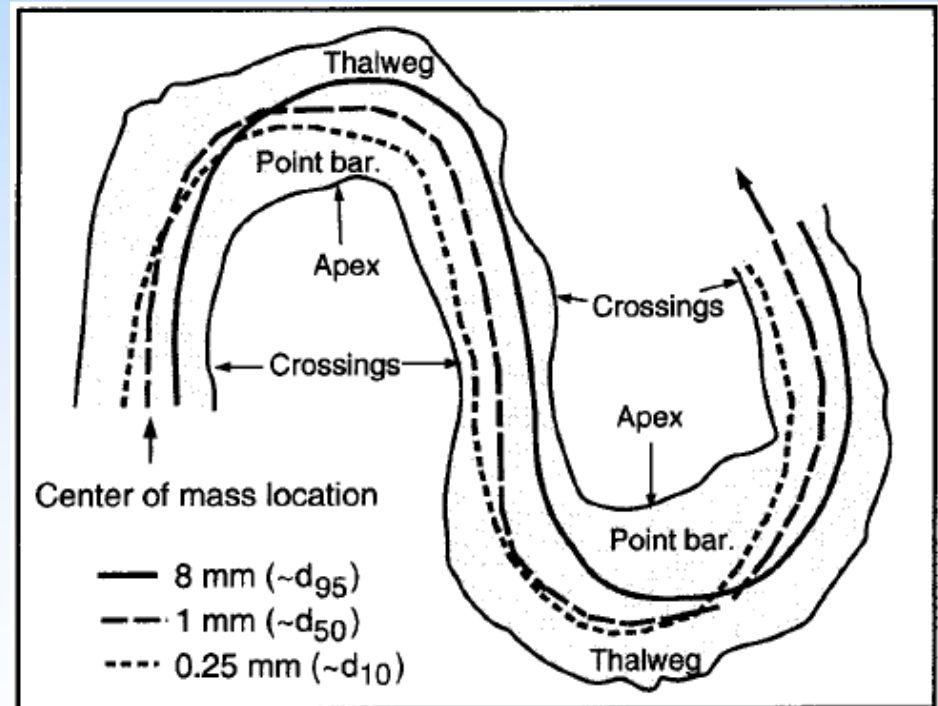


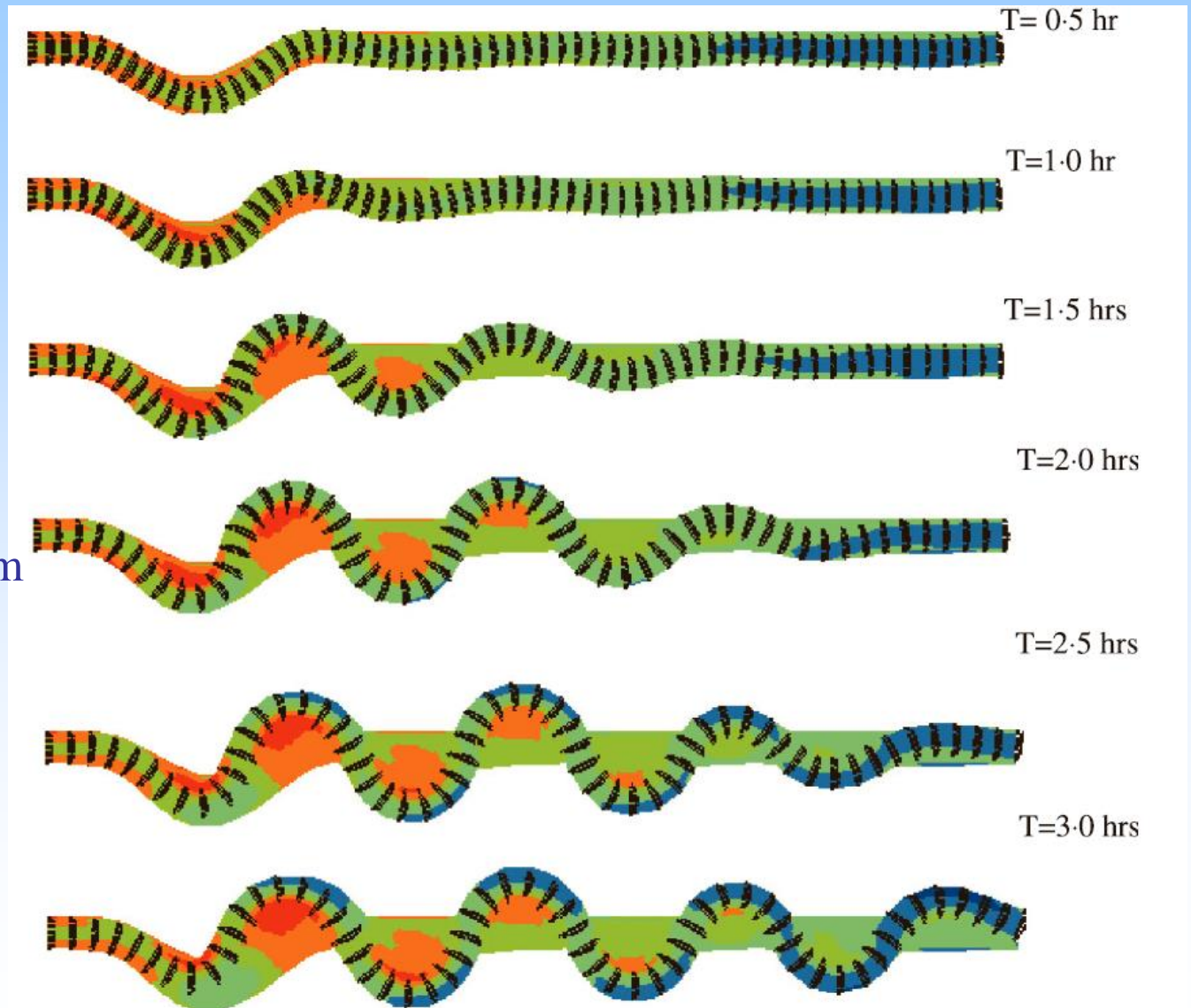
Fig. 5 Center of mass curves for three bedload size fractions

from Julien and Anthony (JHR-IAHR, 2002)

# Meandering Simulations

## Initial Conditions

- sine-generated
- deflection angle  $30^\circ$
- discharge  $2.1 \text{ l/s}$
- width  $0.4 \text{ m}$
- length  $13.2 \text{ m}$
- sediment size  $0.45 \text{ mm}$



Model from Duan and Julien (ESPL, 2005)



# Meandering Evolution

Example starting from a straight channel  
on the Rio Puerco, New Mexico



Rio Puerco, New Mexico

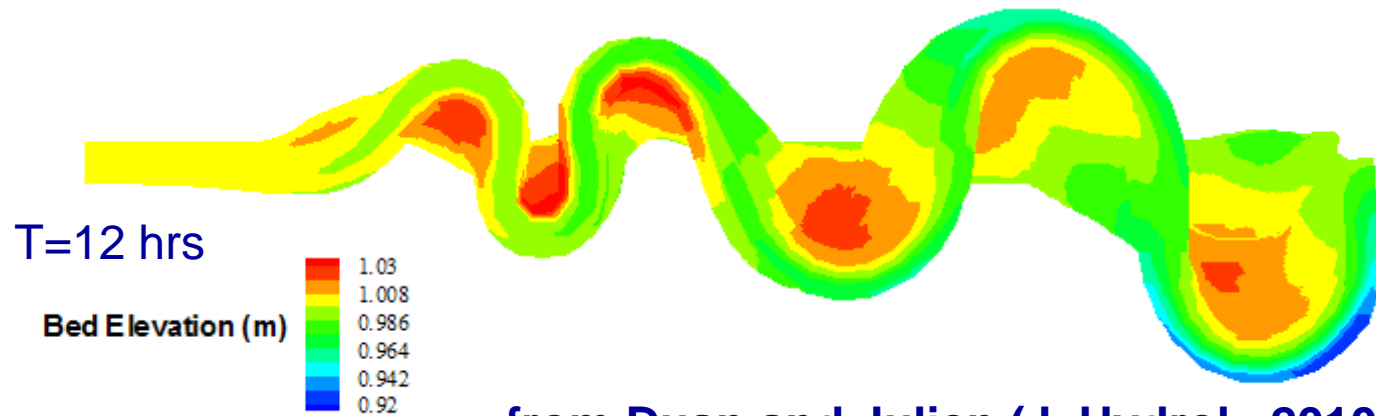
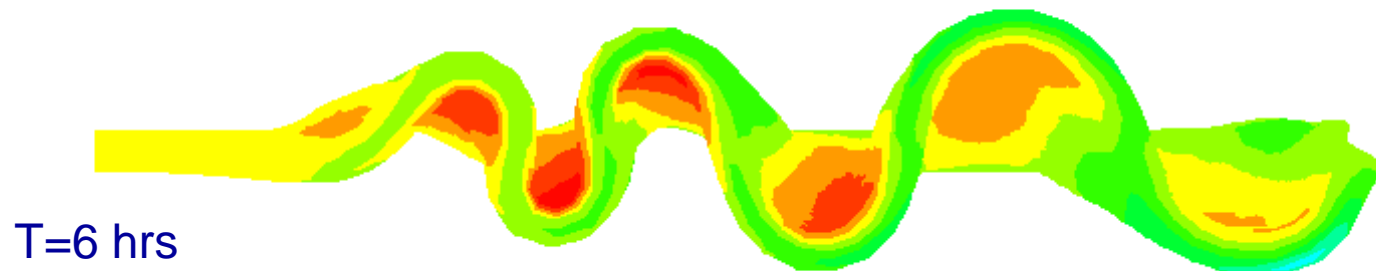
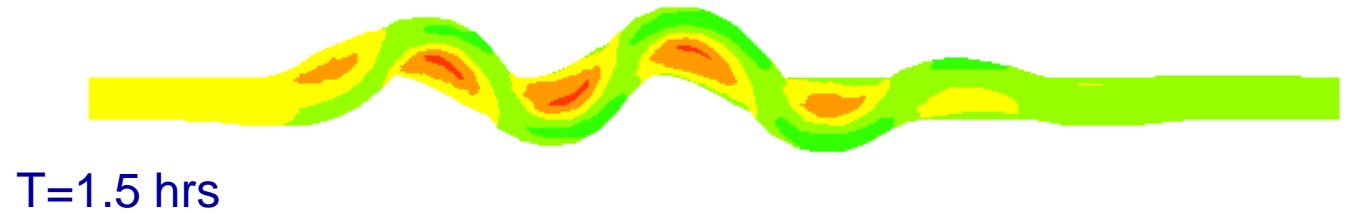


Model from Duan and Julien (ESPL, 2005)

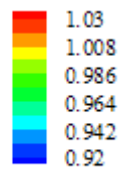


Rio Puerco, New Mexico

# Meandering Simulations



Bed Elevation (m)



from Duan and Julien (J. Hydrol., 2010)

# Lateral Migration in a Meandering Channel



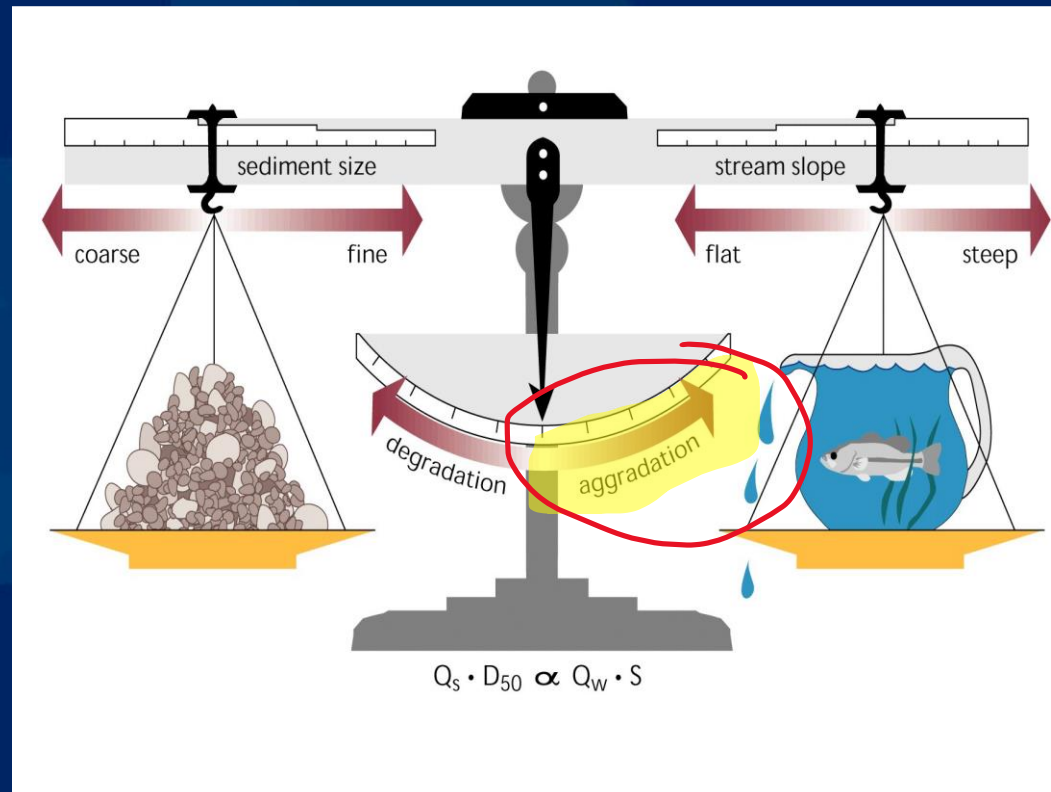
# Rivers and Dams

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1. River Equilibrium
2. **Aggradation**
3. Degradation below Dams
4. Case Study Gupo Bridge
5. Case Study Dam Break



# 2a. Meandering to Braiding (sediment overload)



# Natural Chute Cutoffs

- Often in response to an increase in sediment load



- Chute cutoffs on Williams River, AK  
(Photo by N.D. Smith)



# Oxbow Lake



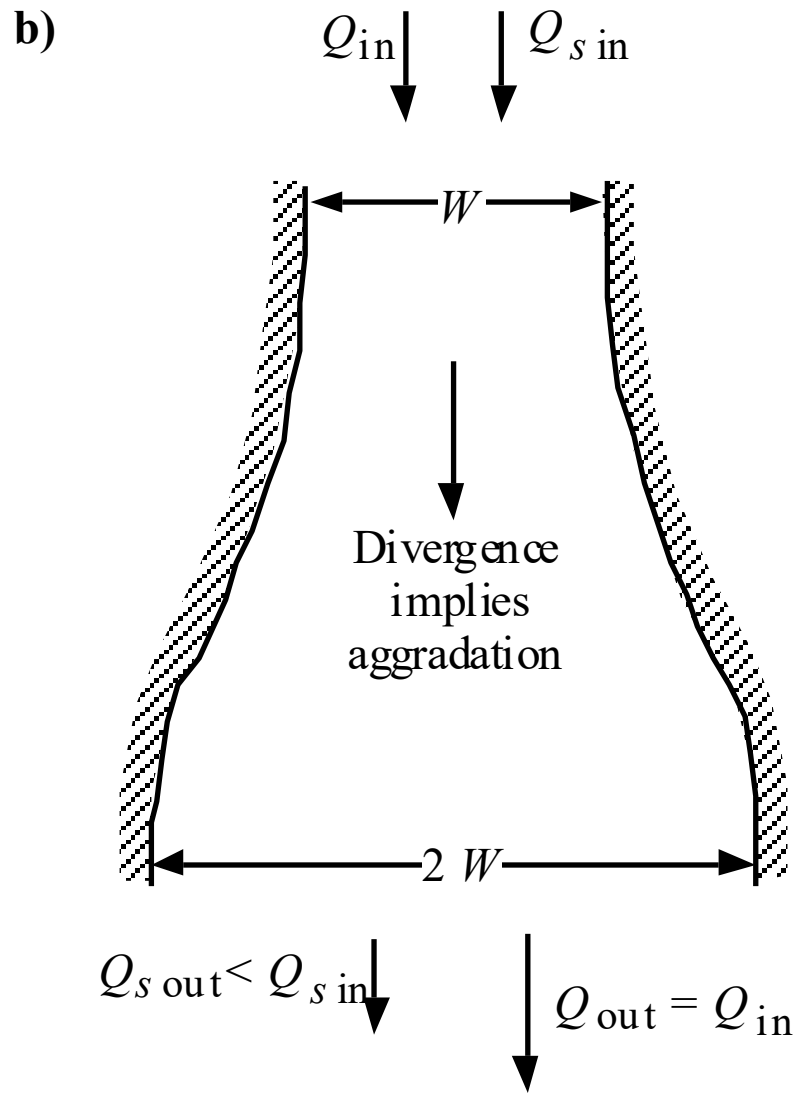
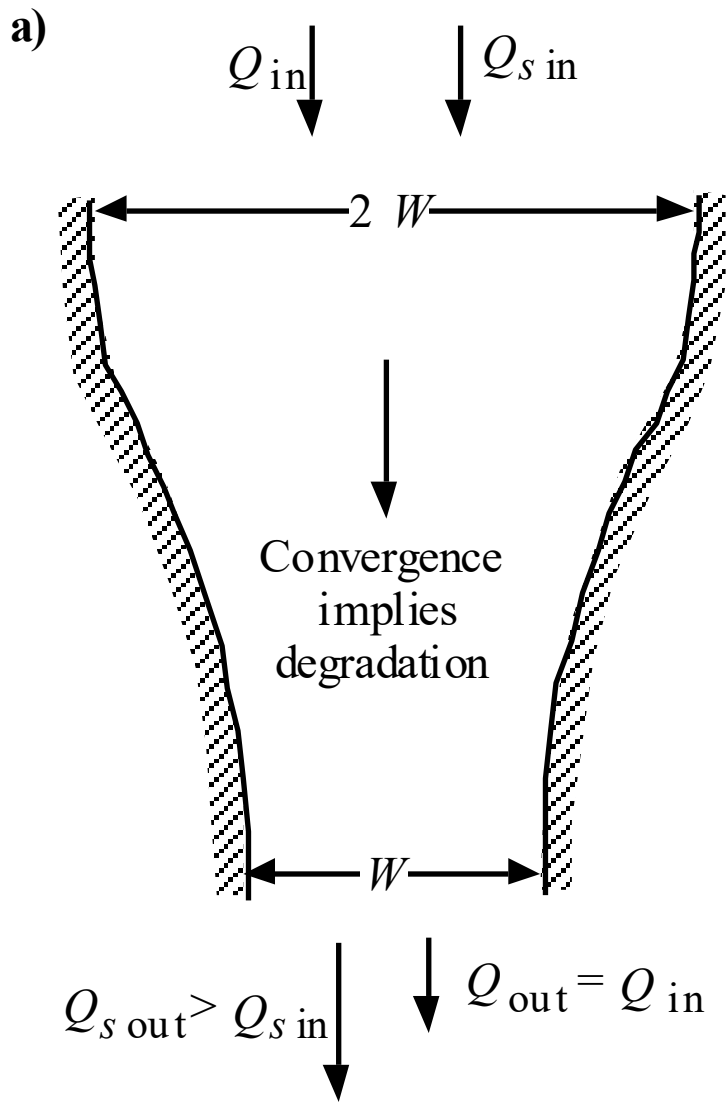


Riverbed rising forces  
river overbank



## 2b. Channel width variability

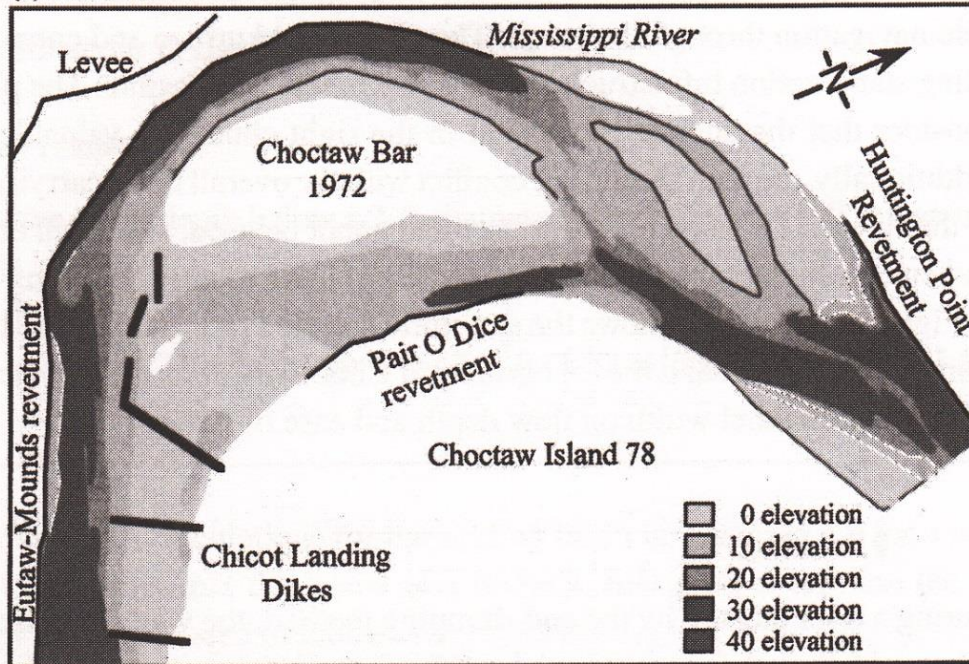
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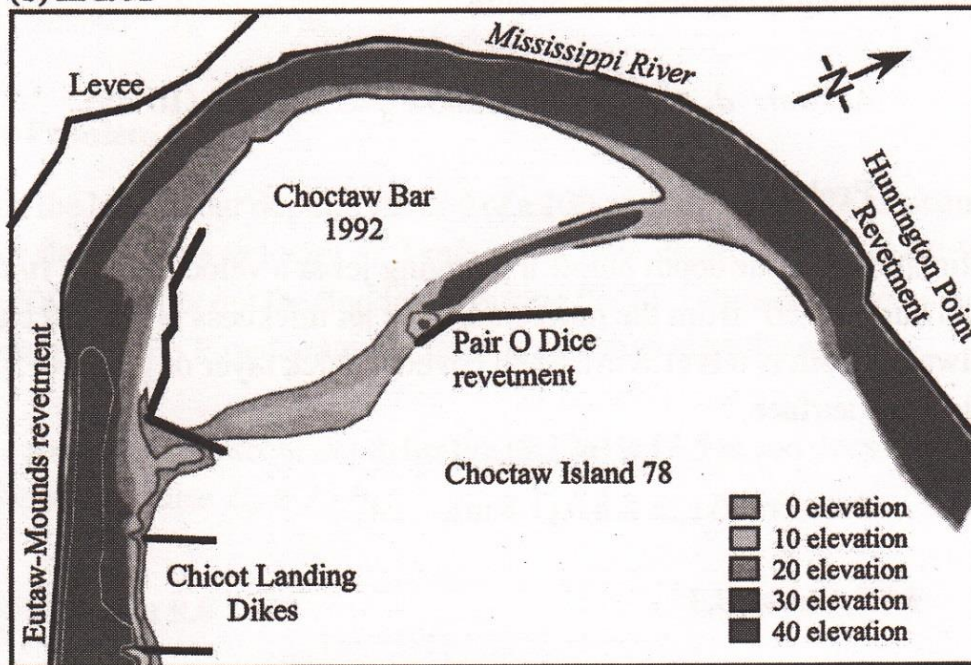
# Dykes



(a) In 1972

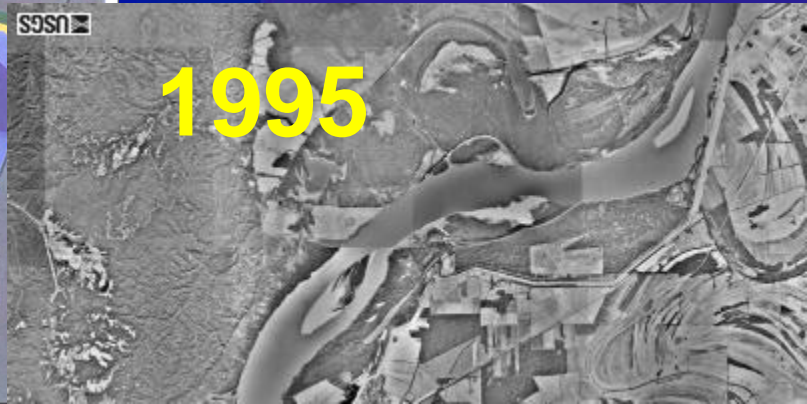
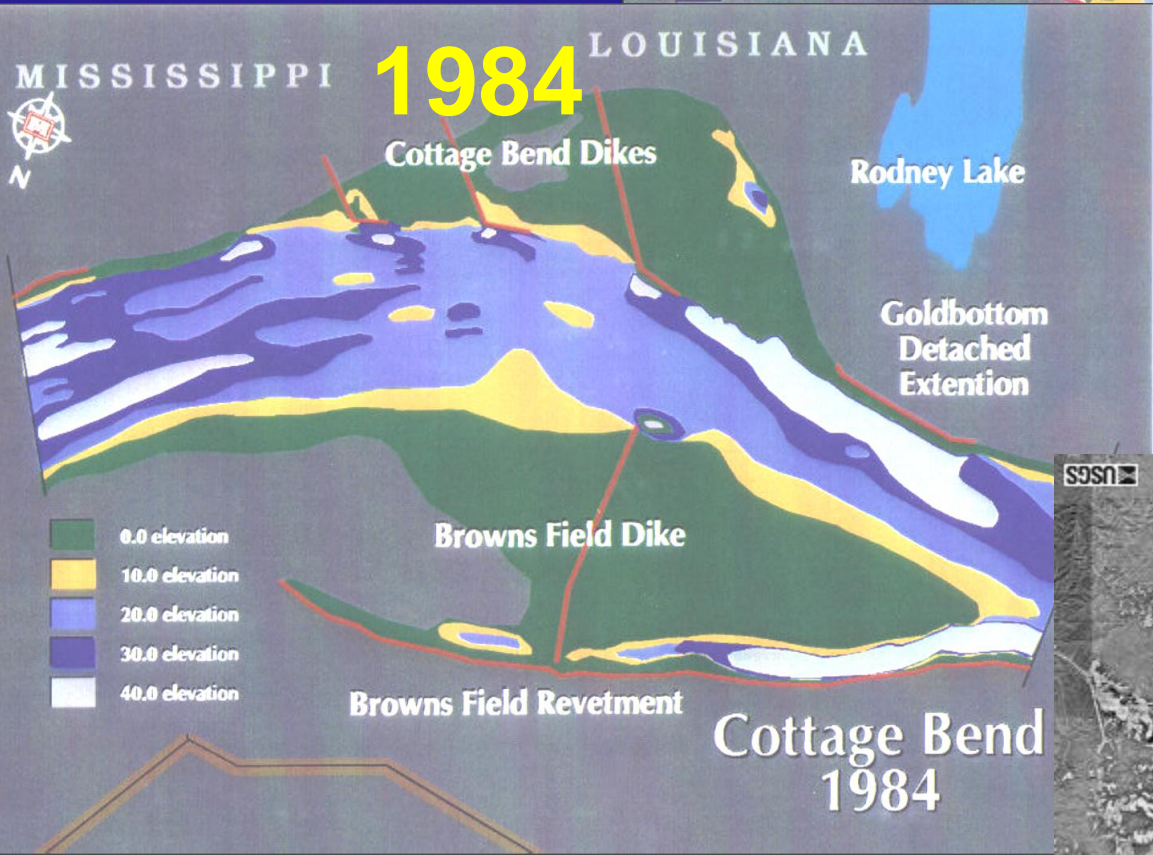
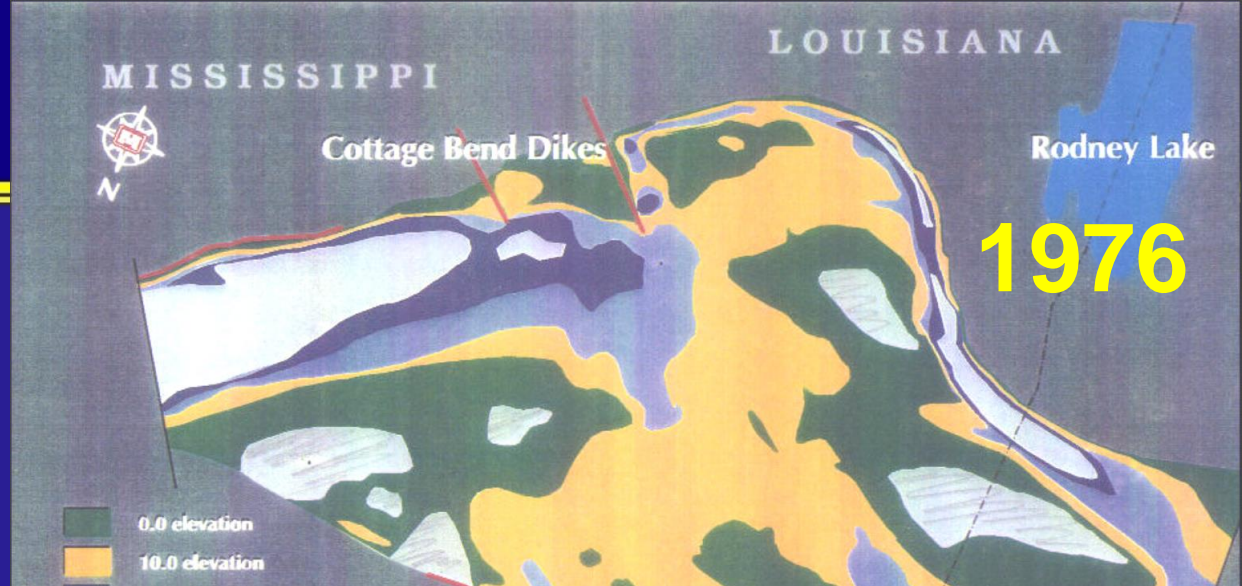


(b) In 1992



From Julien  
River Mechanics  
CUP 2018

# Cottage Bend



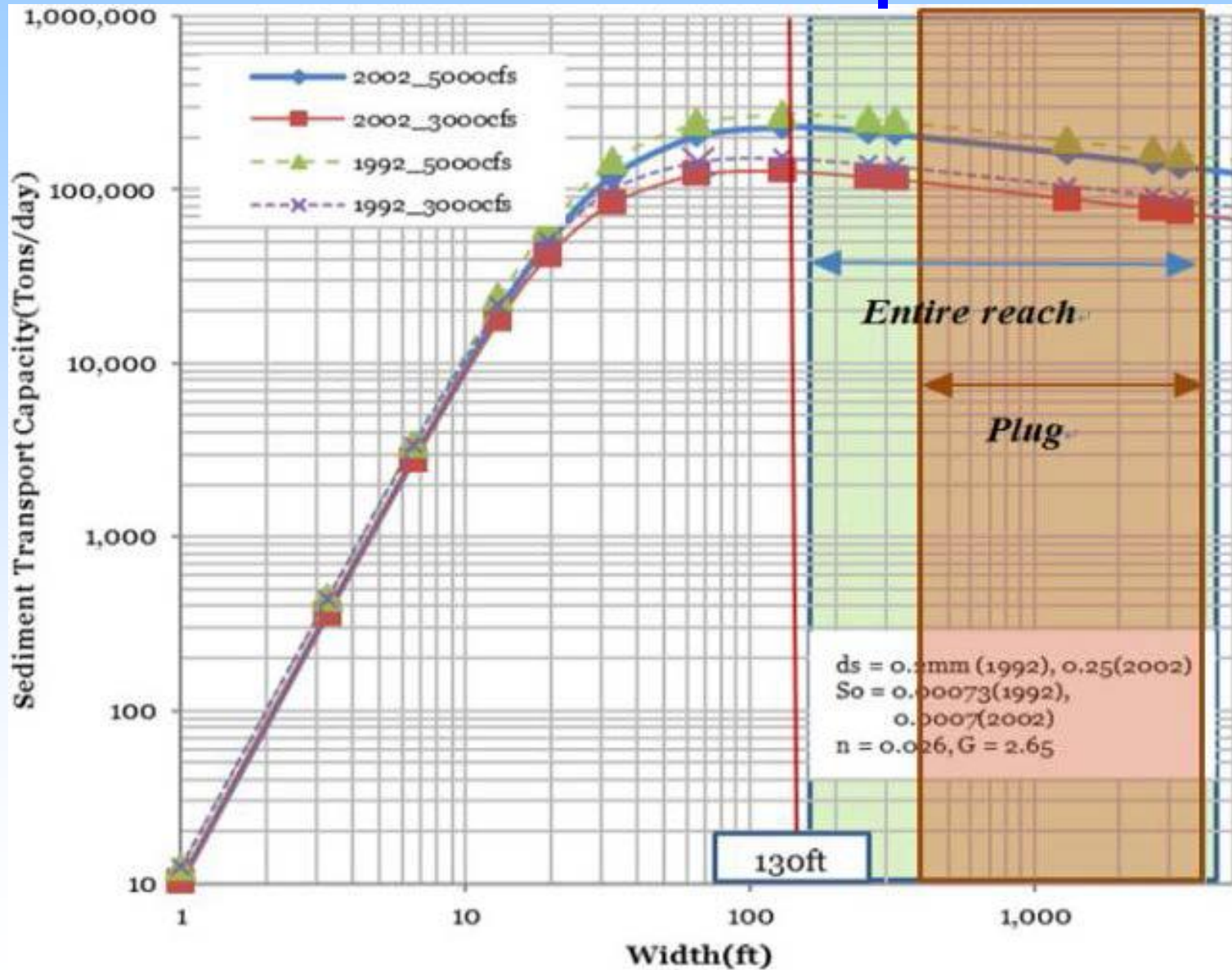
## 2c. Width-slope trade-offs

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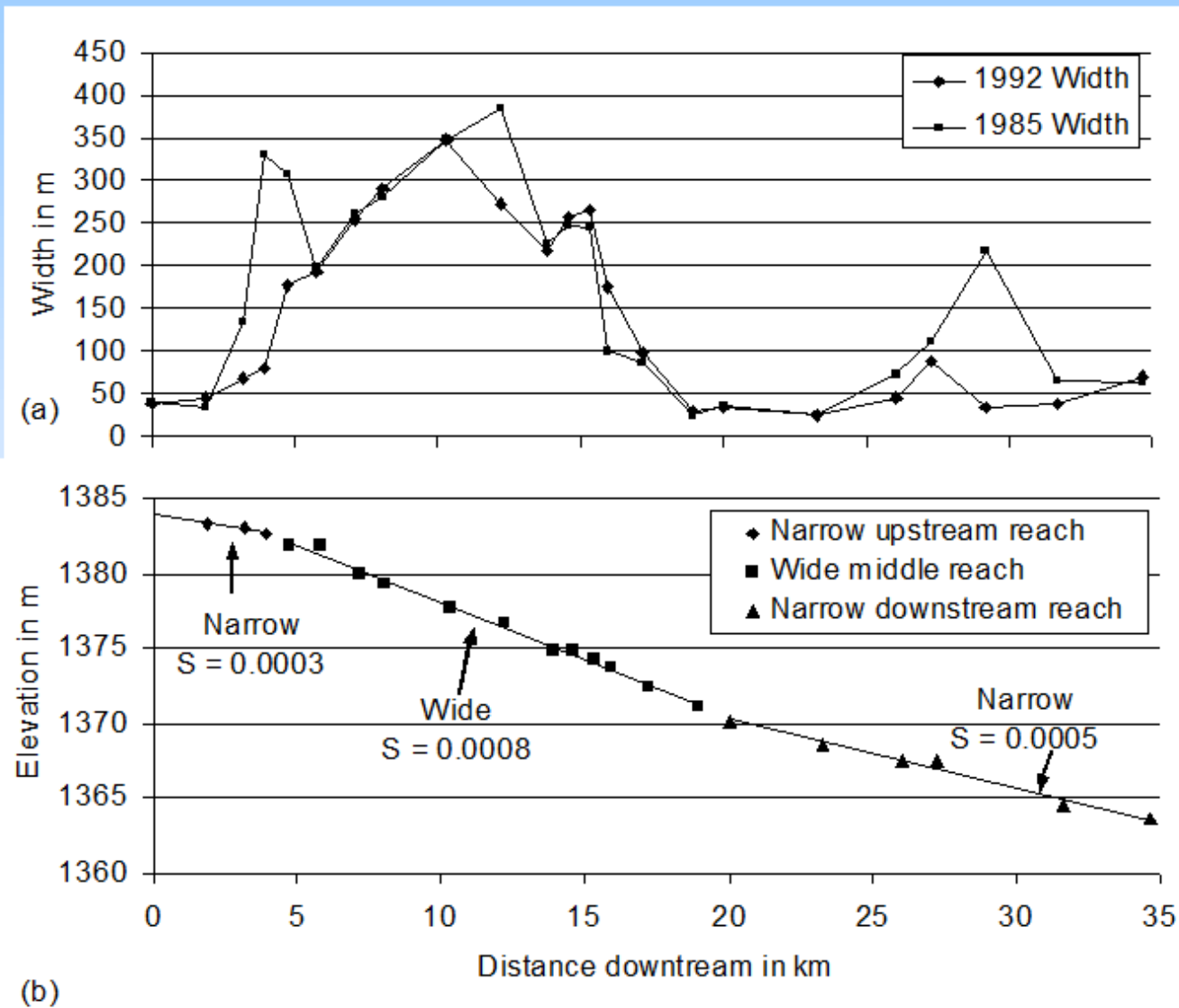




# Relationship between channel width and sediment transport



# Wider reaches are steeper!



# Rivers and Dams

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2. Aggradation
3. **Degradation below Dams**
4. Case Study Gupo Bridge
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# 3a. Degradation Problems

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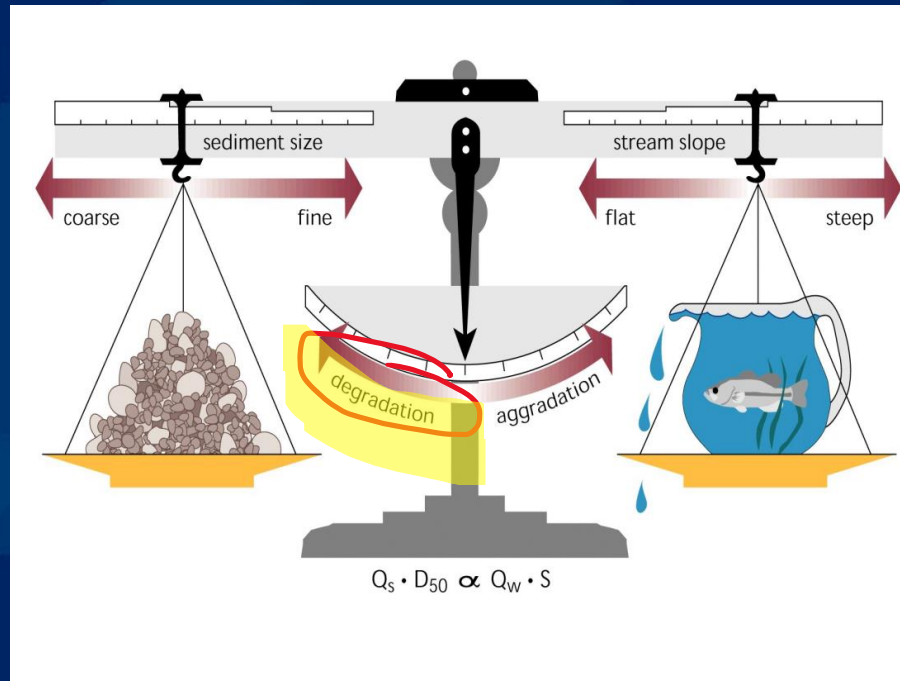








# 3b. Braiding to meandering (sediment starved)





Cochiti  
Dam



Rio Grande

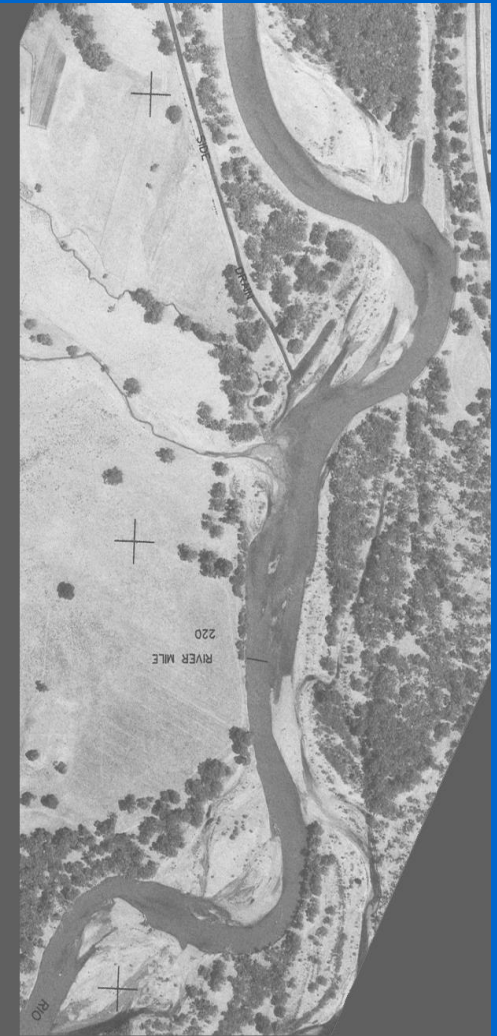
Santa Fe River

# Planform geometry

1935

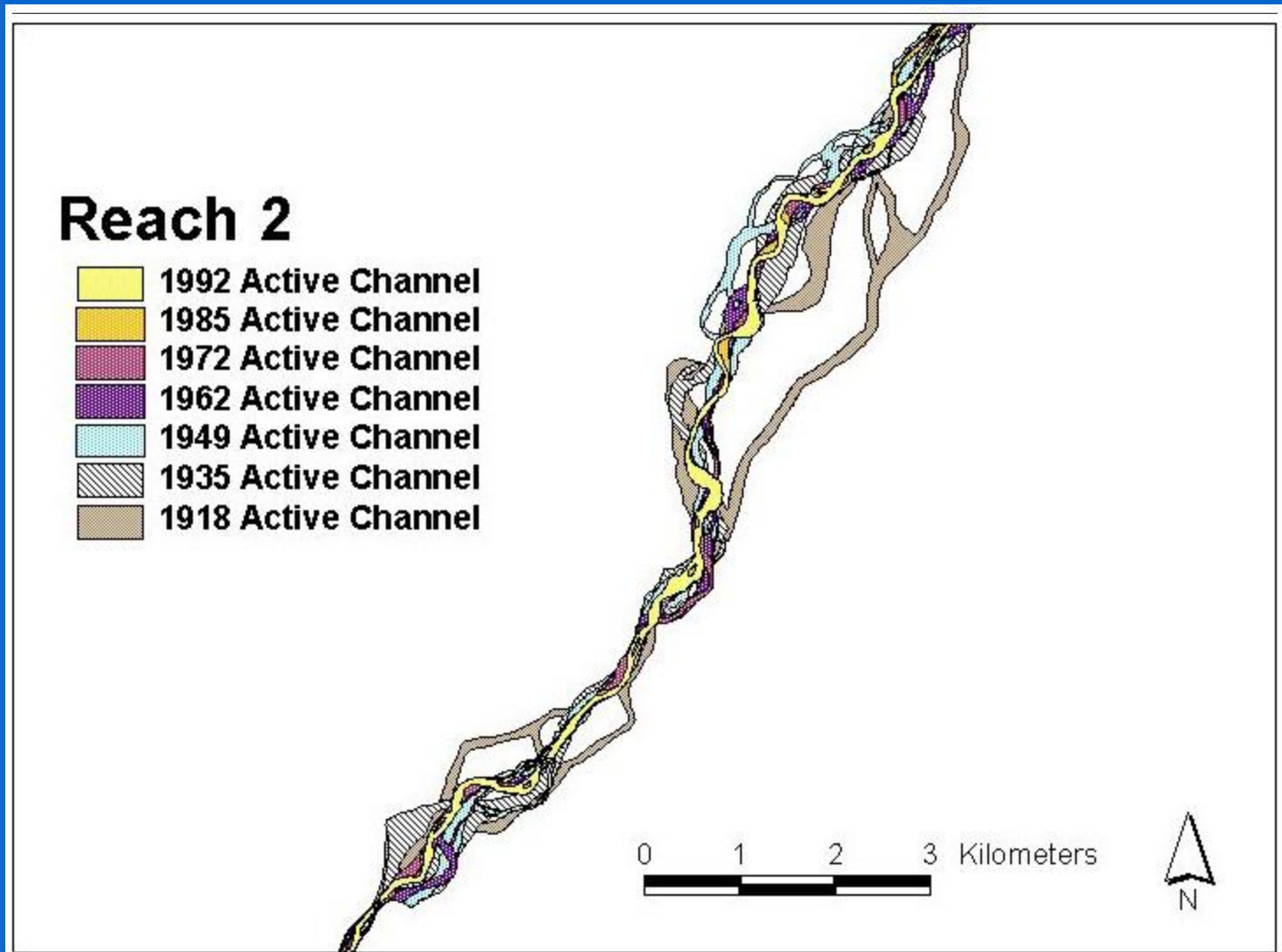
1972

1992

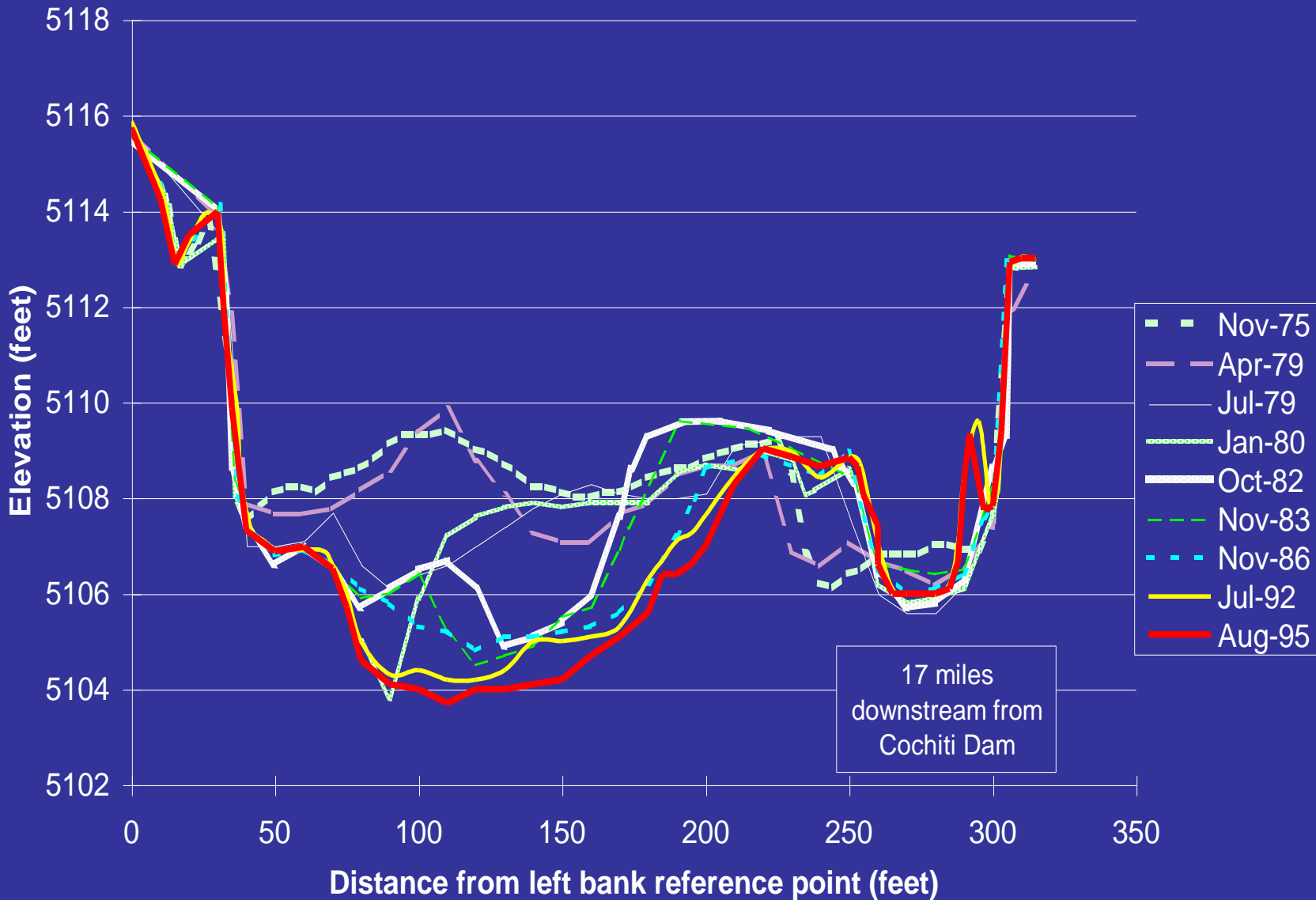


0 600 m

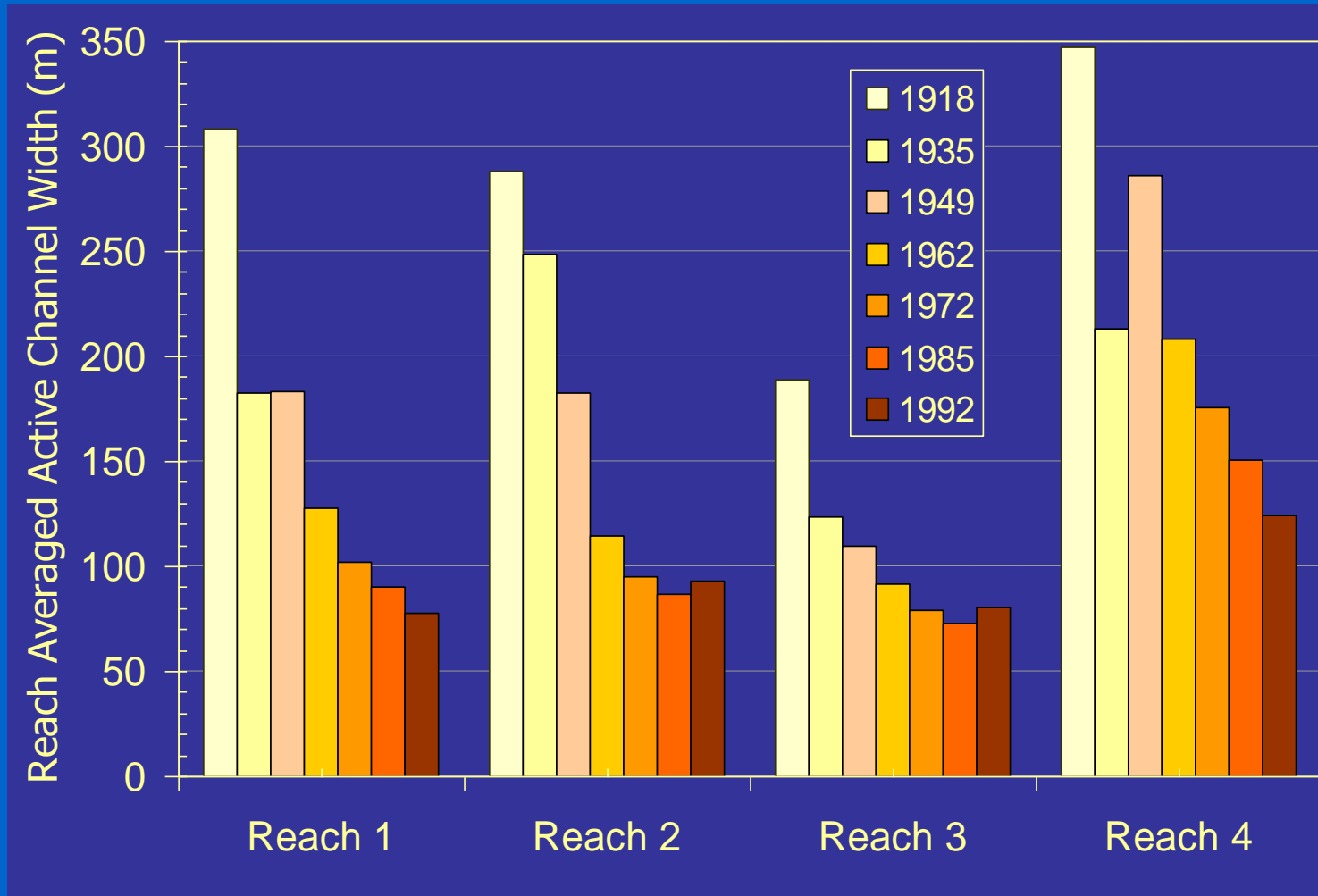
# Lateral Adjustments



# Cross section CO-18



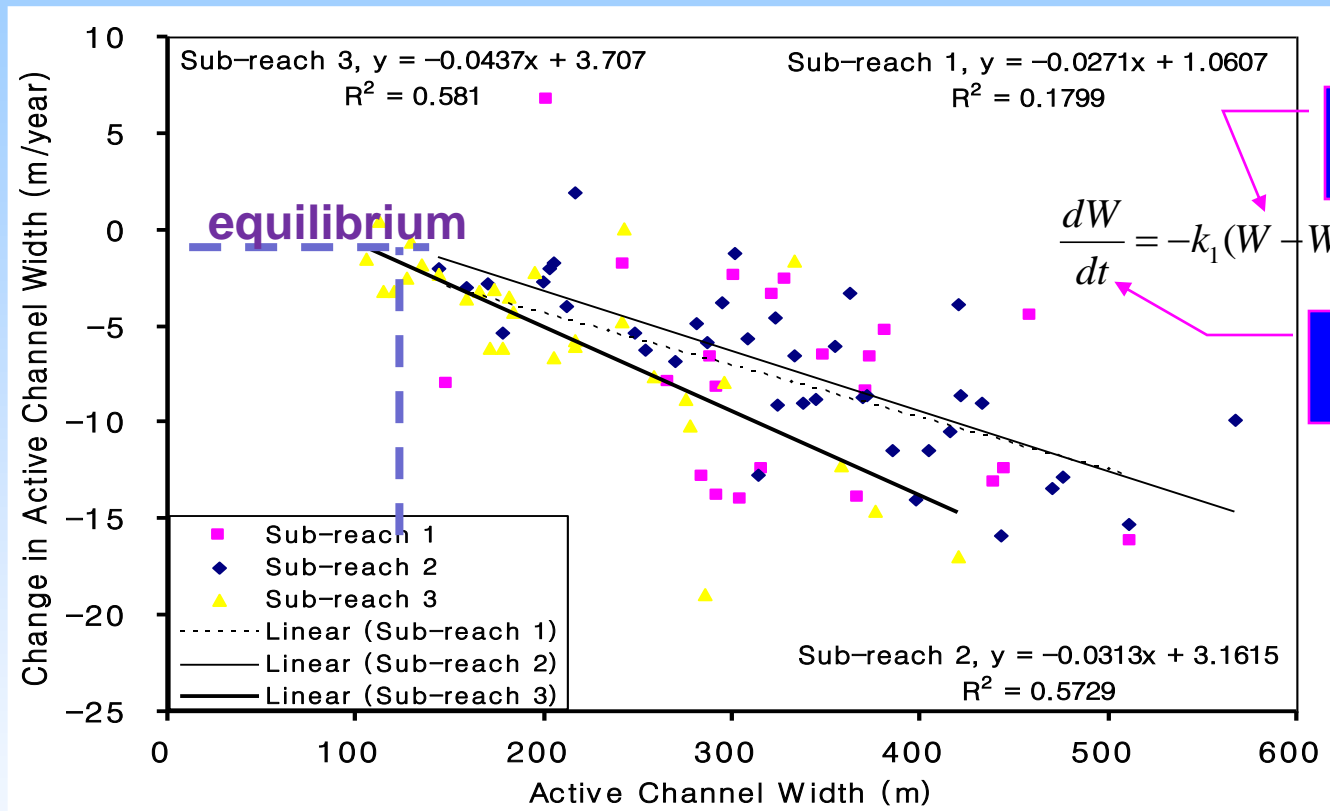
# Active channel width





# Changes in active channel width

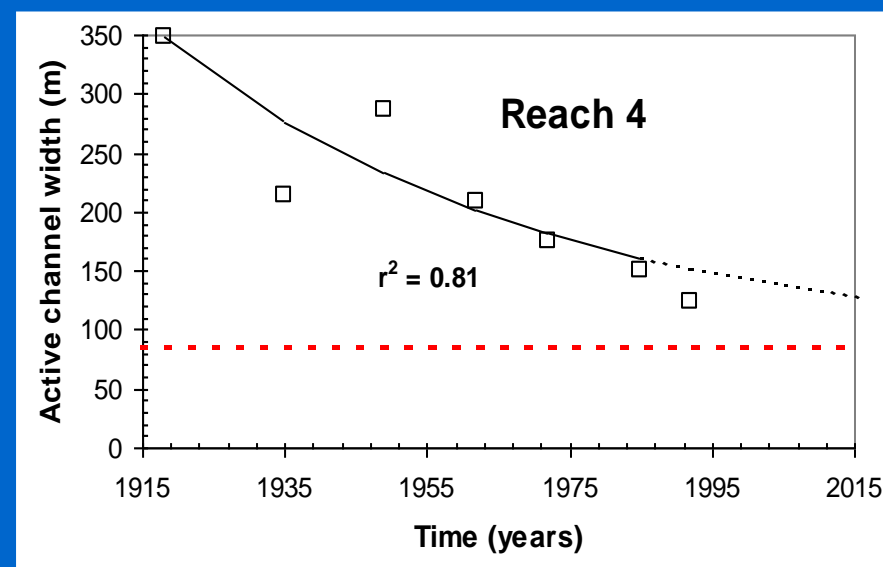
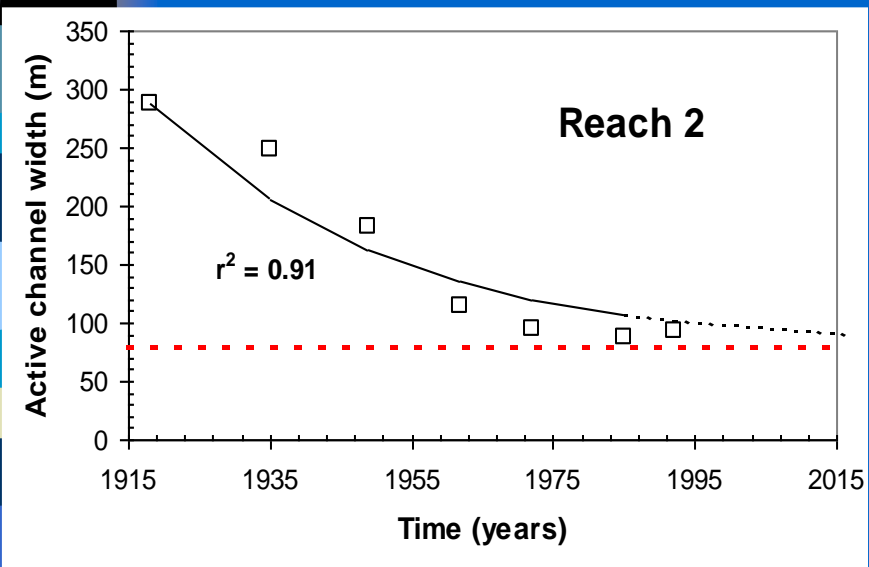
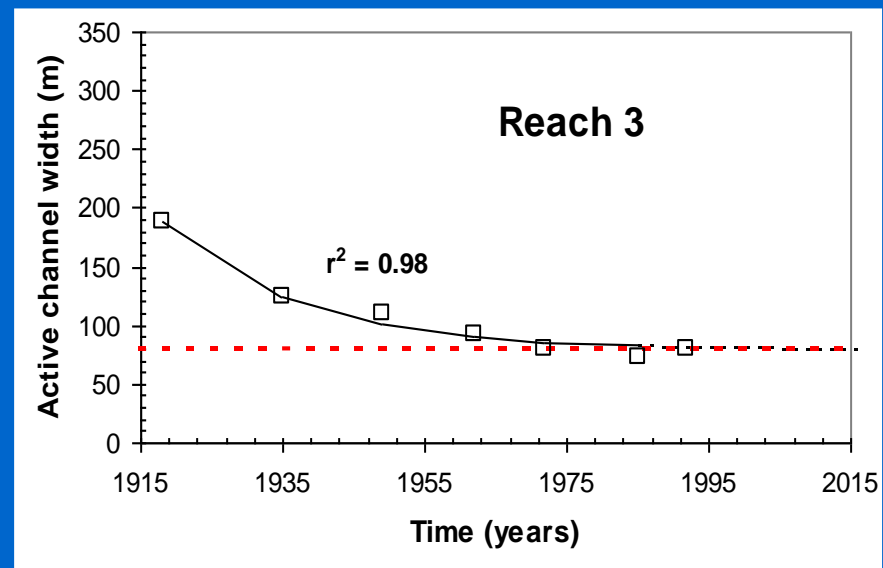
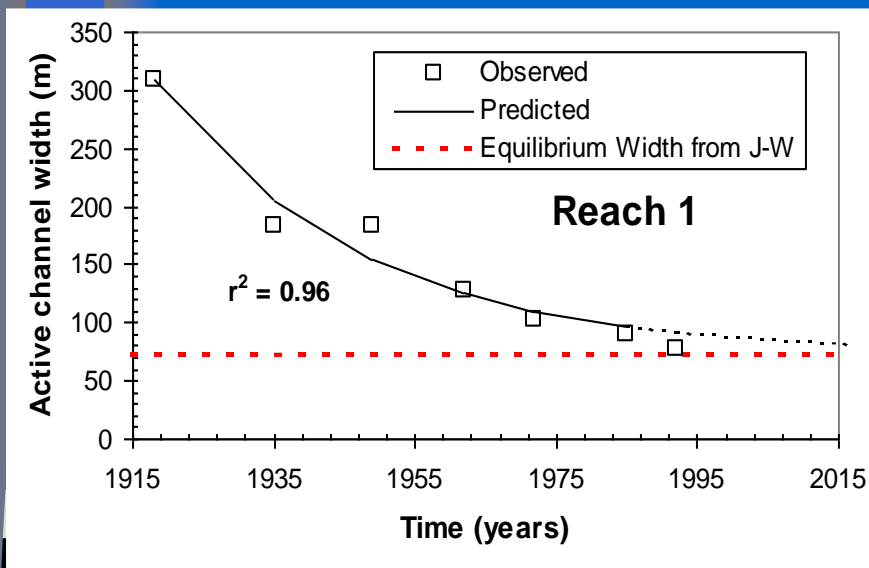
## Rio Grande, NM (after Richard et al., 2005)



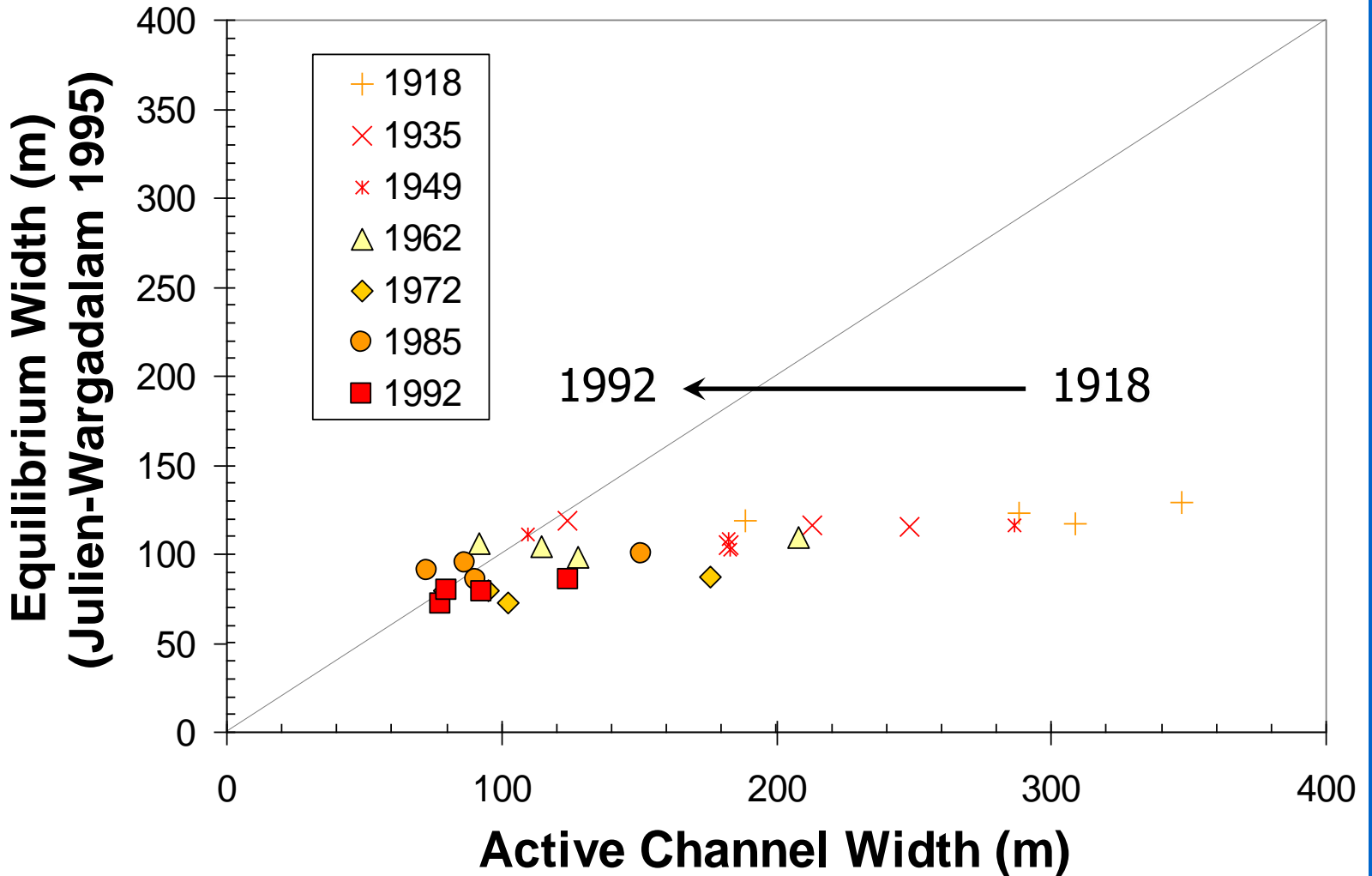
$$\frac{dW}{dt} = -k(W - W_e)$$

$$W = W_e + (W_o - W_e) \cdot e^{-kt}$$

# Exponential Model Results



# Hydraulic Geometry Equations (Julien & Wargadalam 1995)



# 3c. River Problems in Estuaries

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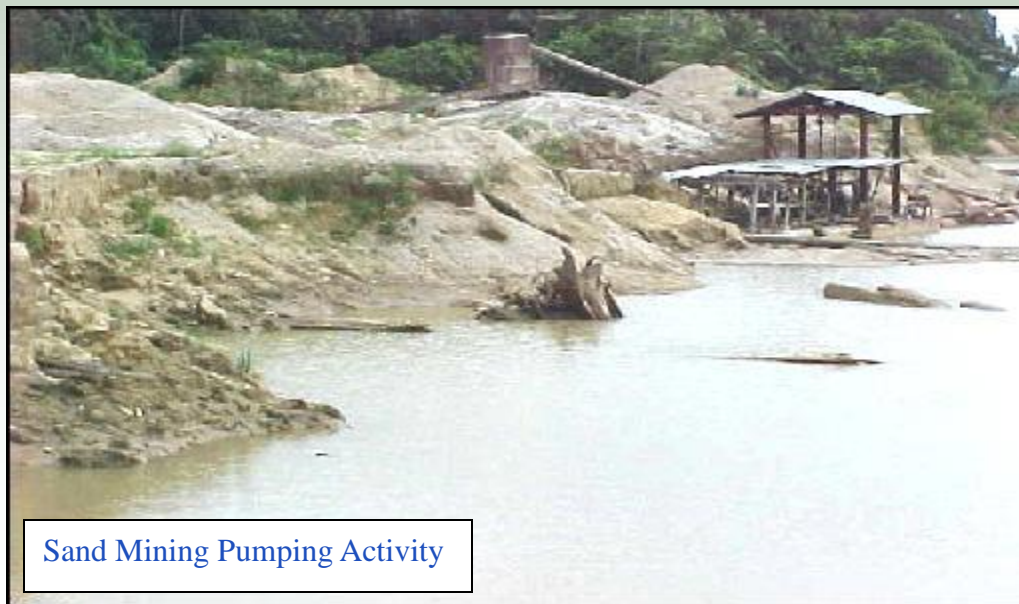
# Sand and Gravel Mining



Kampong Kubang Bedengong



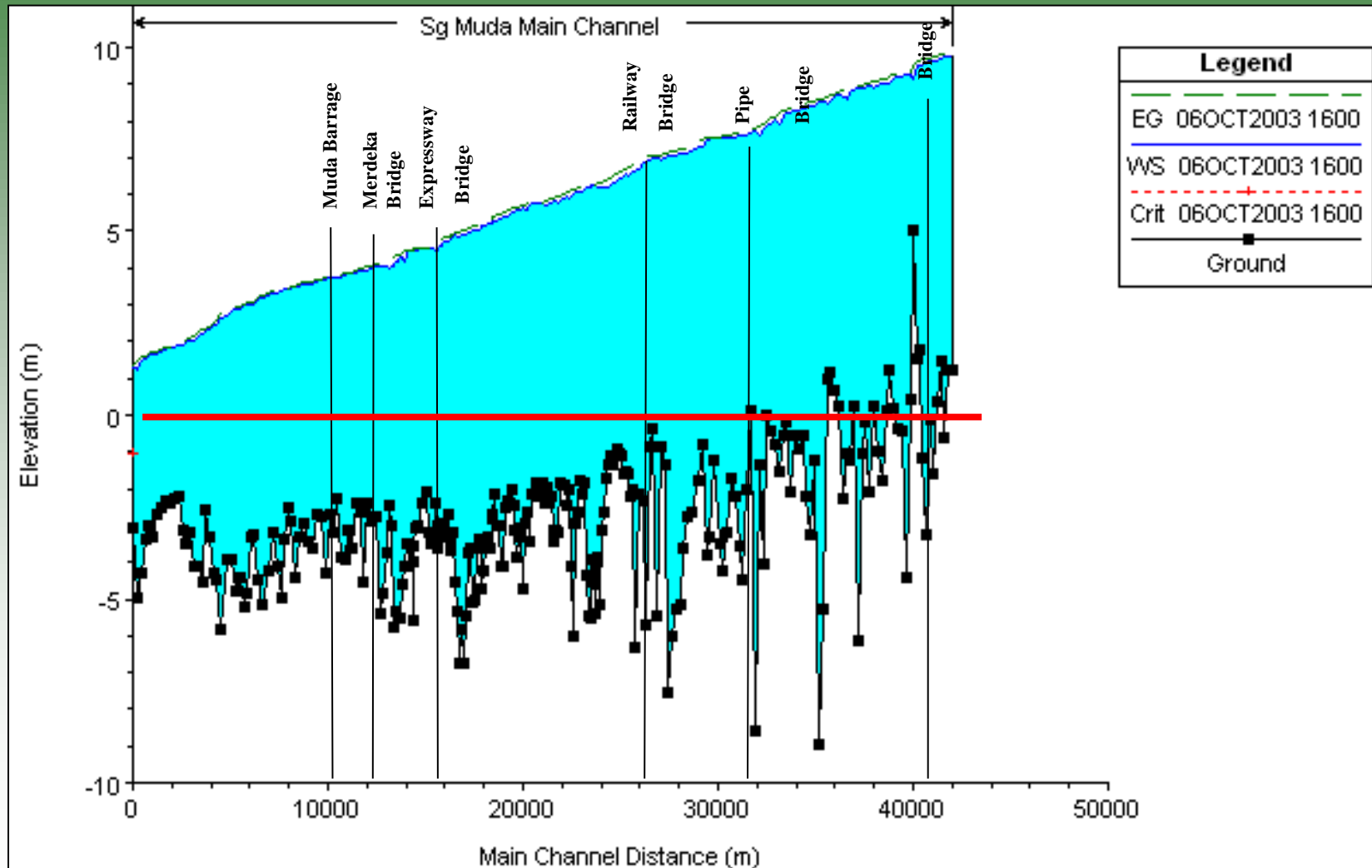
Kampong Lubok Segintah



Sand Mining Pumping Activity

River Sand  
Mining

# Longitudinal Flood Profile for Sg Muda ( $Q=1340\text{m}^3/\text{s}$ )



# Wentim and Ren-fitting

Wentim River near Pusan, South Korea

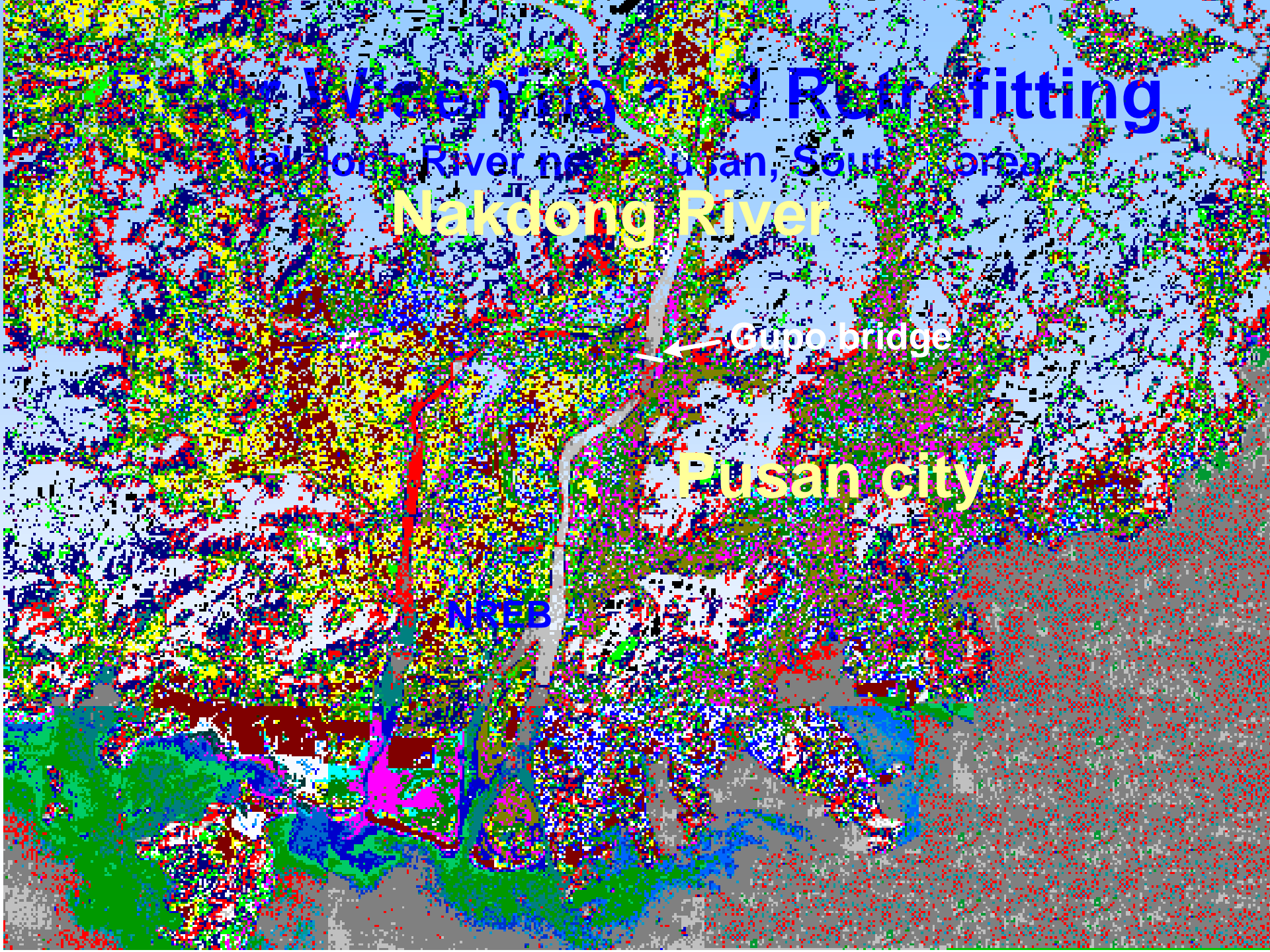
## Nakdong River

Gupo bridge

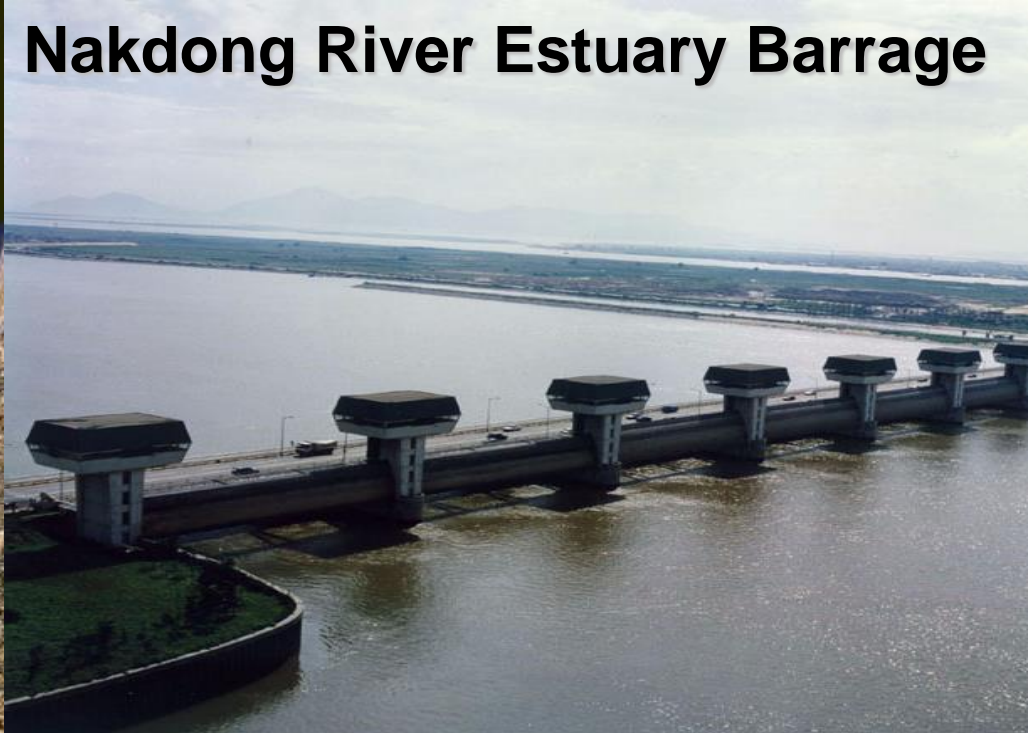
## Pusan city

NREB

Wentim River



# Nakdong River Estuary Barrage



•from Ji et al. ASCE-JHE, Nov. 2011



# Rivers and Dams

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1. River Equilibrium
2. Aggradation
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4. **Case Study Gupo Bridge**
5. Case Study Dam Break

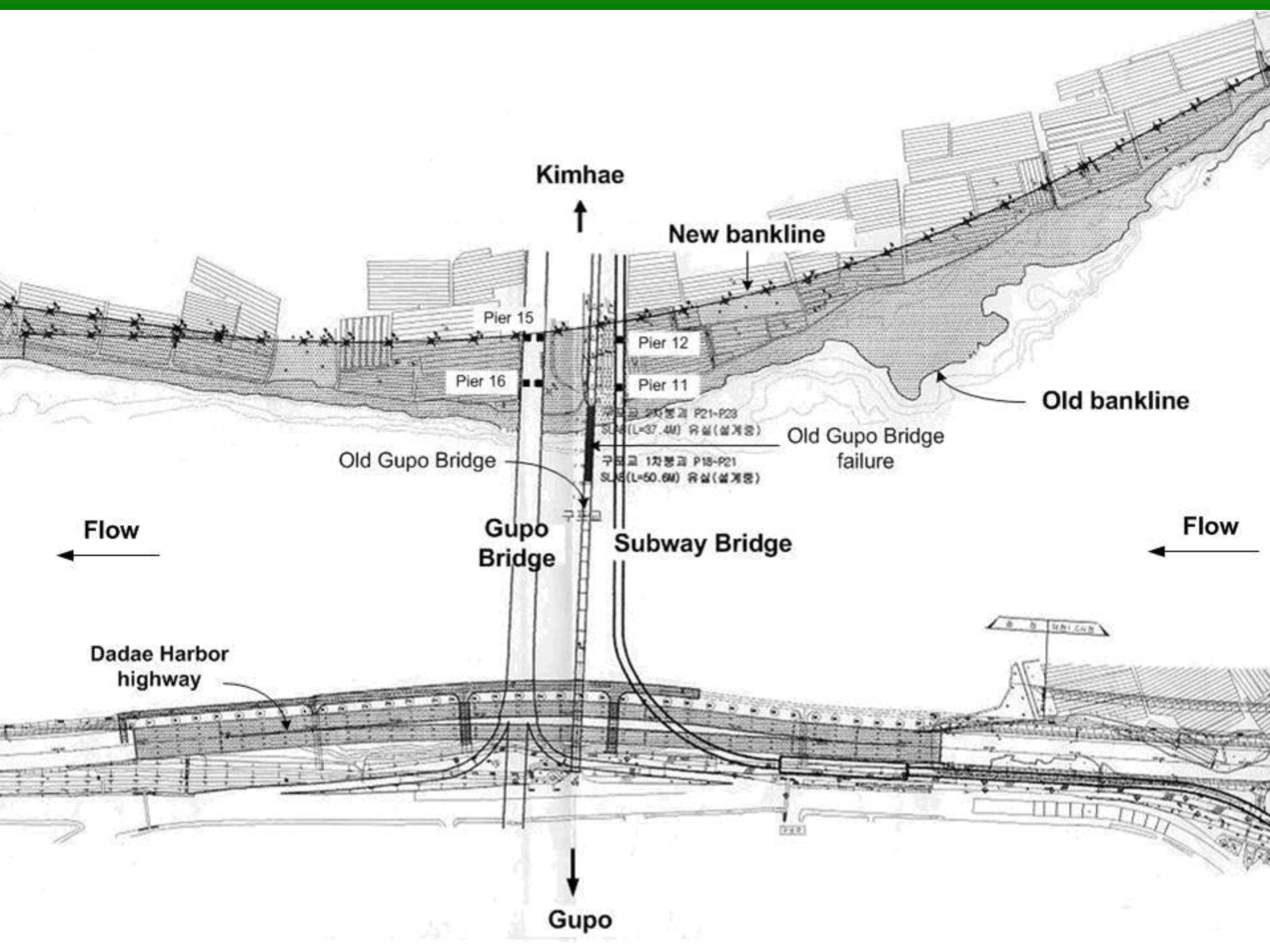


# Case-Study: Gupo Bridge during Typhoon Maemi in 2003





P10



Kimhae

New bankline

Pier 15

Pier 12

Pier 16

Pier 11

Old bankline

Old Gupo Bridge

Old Gupo Bridge failure

Flow

Gupo Bridge

Subway Bridge

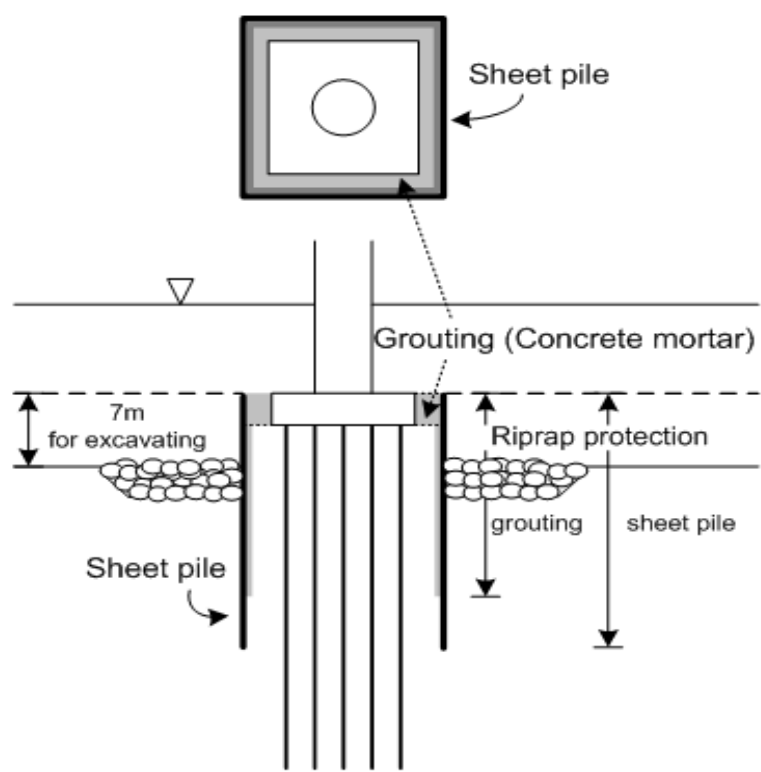
Flow

Dadae Harbor highway

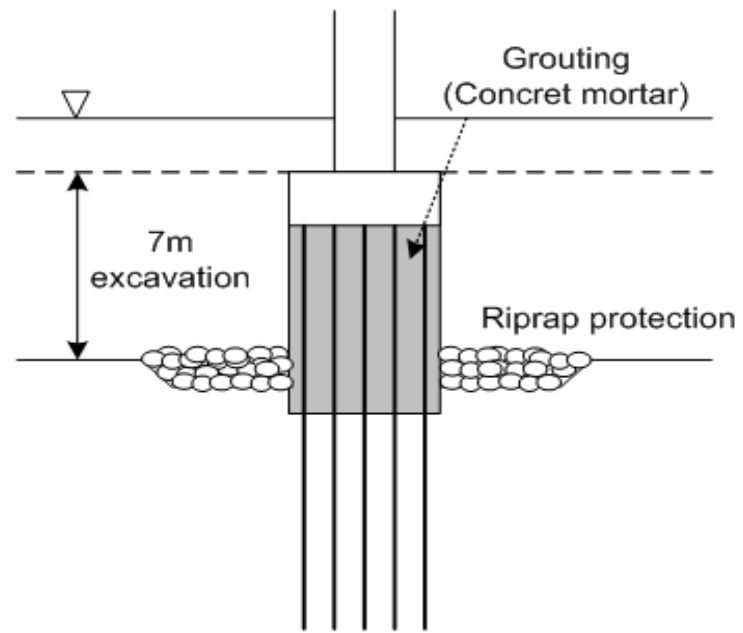
Gupo



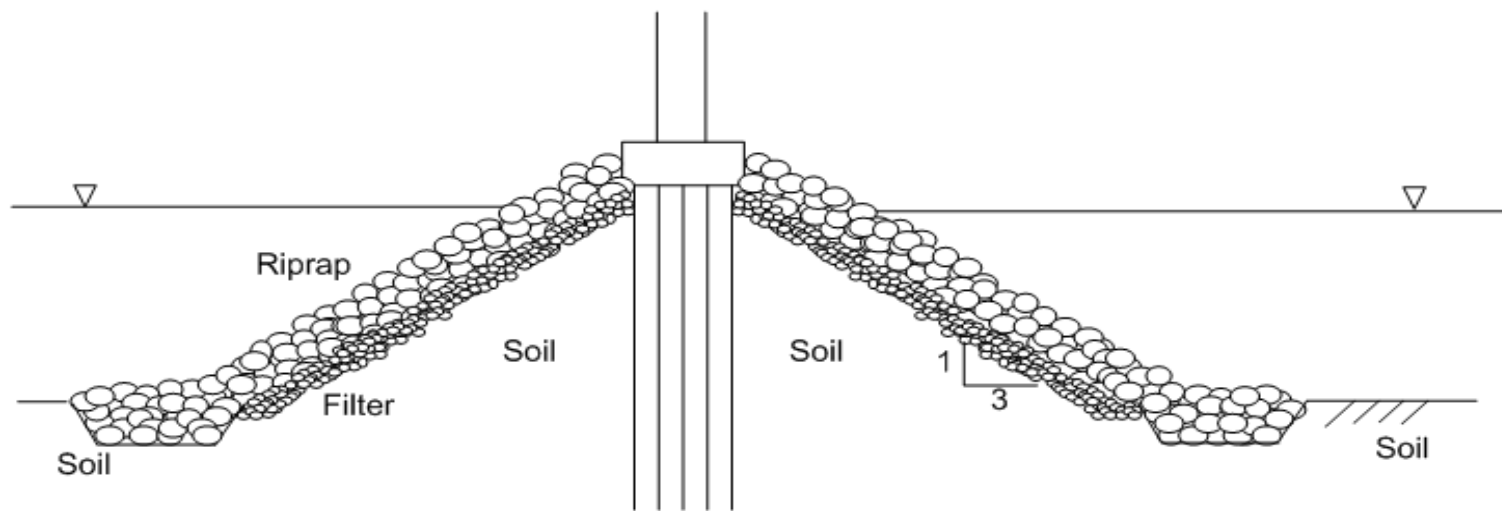
P15



**Alternative plan I**



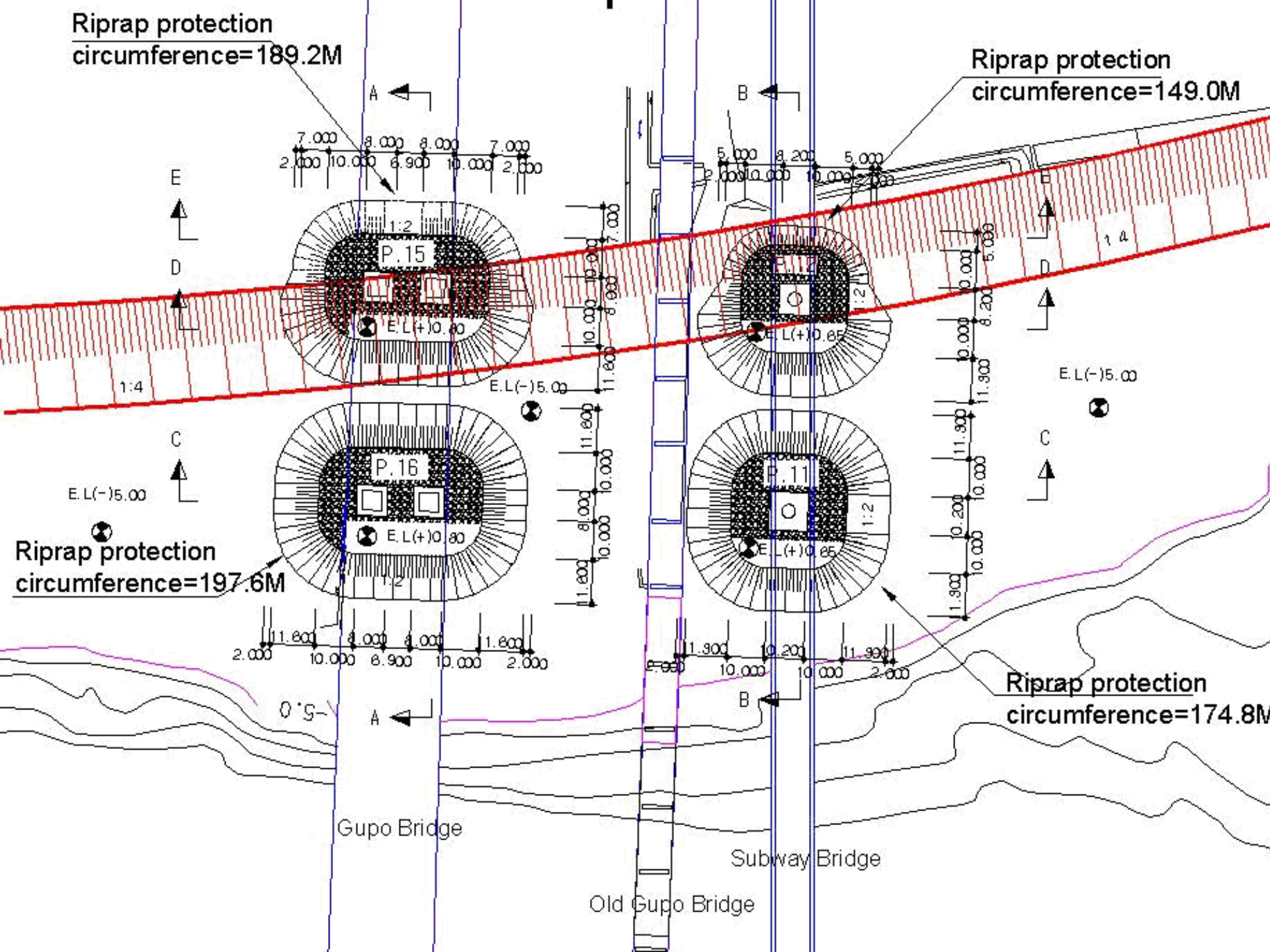
**Alternative plan II**



**Alternative plan III**

Riprap protection  
circumference=189.2M

Riprap protection  
circumference=149.0M



Riprap protection  
circumference=197.6M

Riprap protection  
circumference=174.8M

Gupo Bridge

Subway Bridge

Old Gupo Bridge

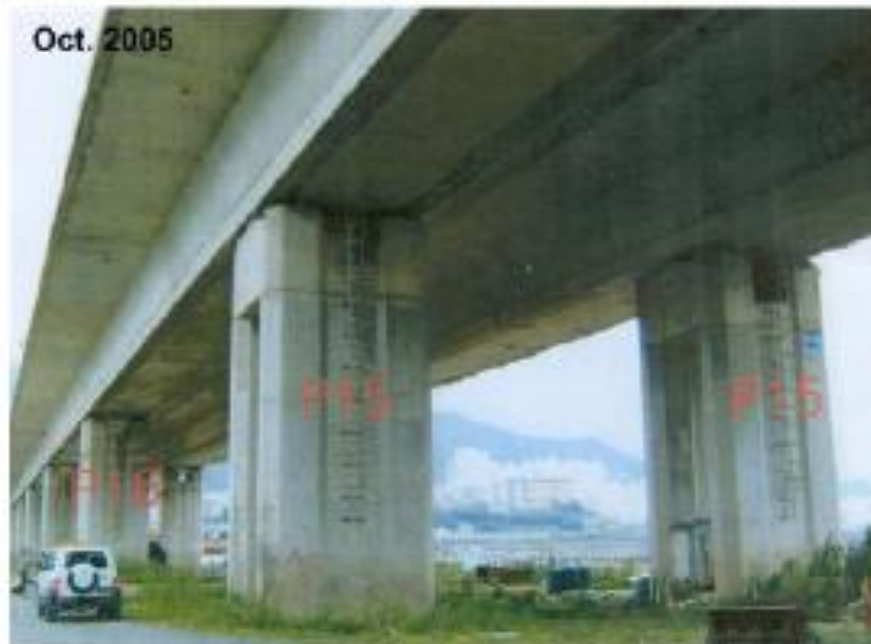
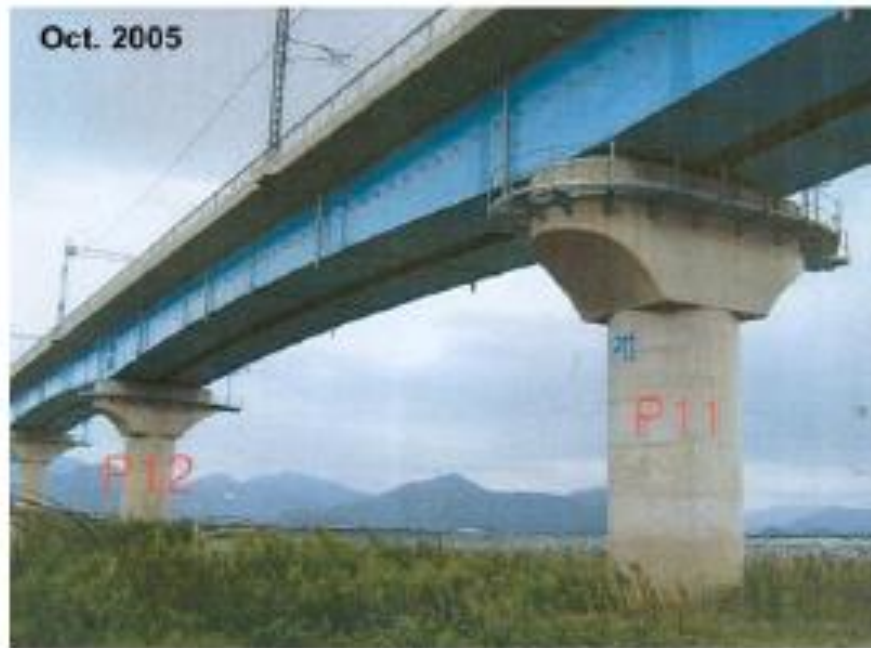


Figure 14. Gupo and Subway Bridge Piers before and after retrofitting construction



# Rivers and Dams

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1. River Equilibrium
2. Aggradation
3. Degradation below Dams
4. Case Study Gupo Bridge
5. **Case Study Dam Break**





**How does the flood wave propagate downstream?**

**21 Mile Dam, Elko County, NV, Feb 8, 2017**

25/01/2019 12:28:2



M1 - Barragem



# The Fundão Dam Collapse

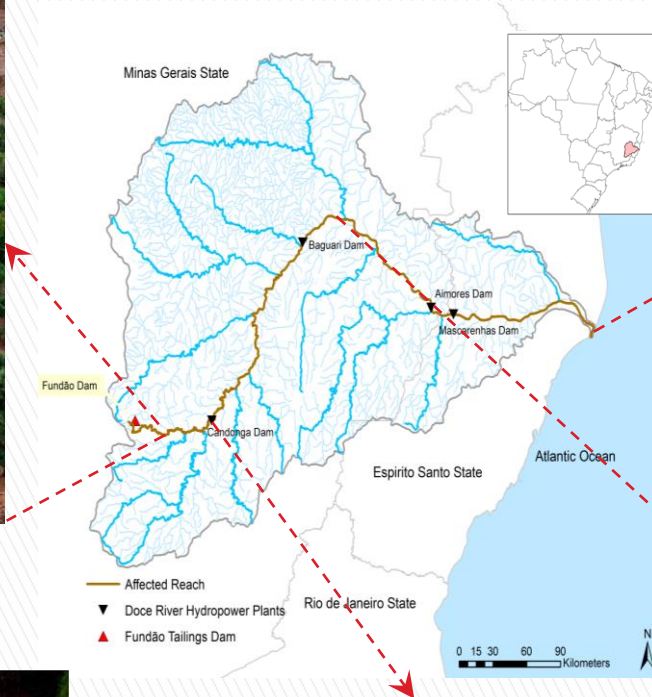
**Bento Rodrigues Town,  
6 November 2015**



**Gesteira Town  
6 November 2015**



from Marcos Palu (2018)



**Coast, 21 November 2015  
C ≈ 1,500 mg/l**



**Doce River at  
Governador Valadares City  
11 November 2015,  
C ≈ 30,000 mg/l**

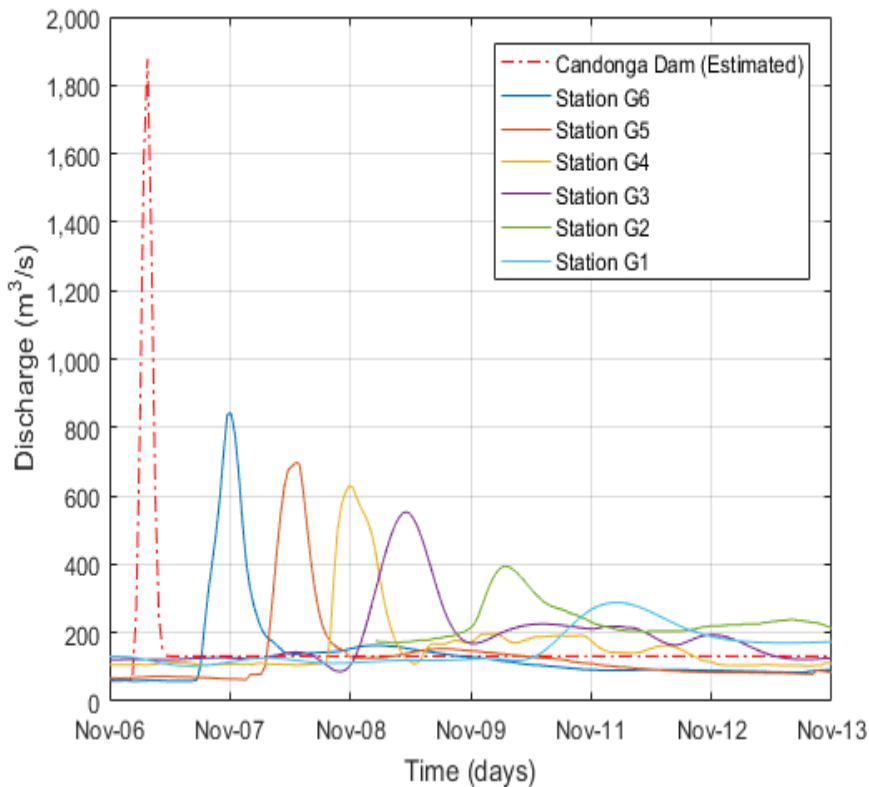


**Candonga Dam, 6 November 2015  
C ≈ 700,000 mg/l**

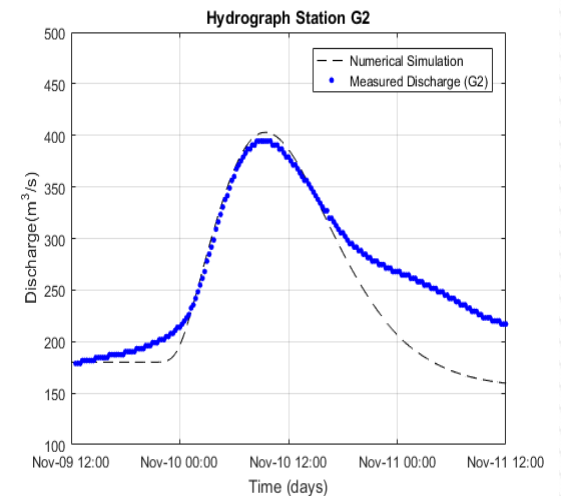
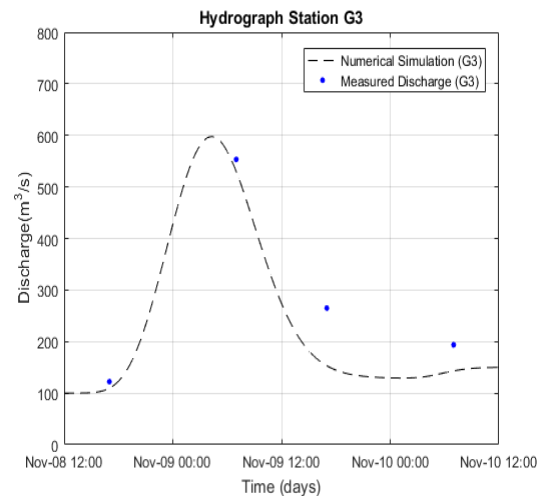
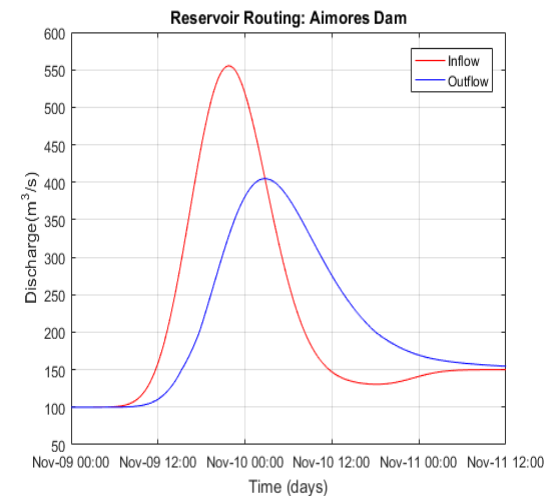
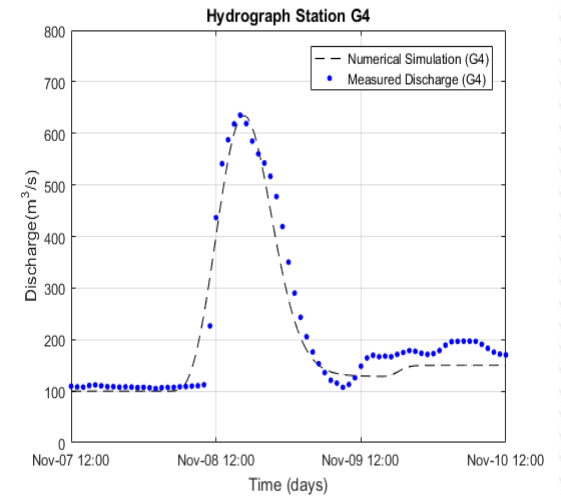
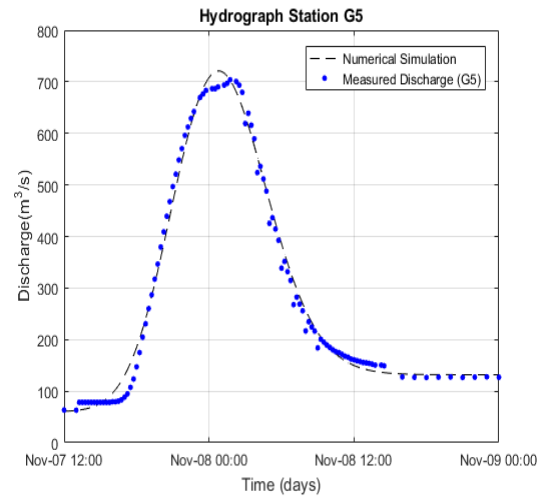
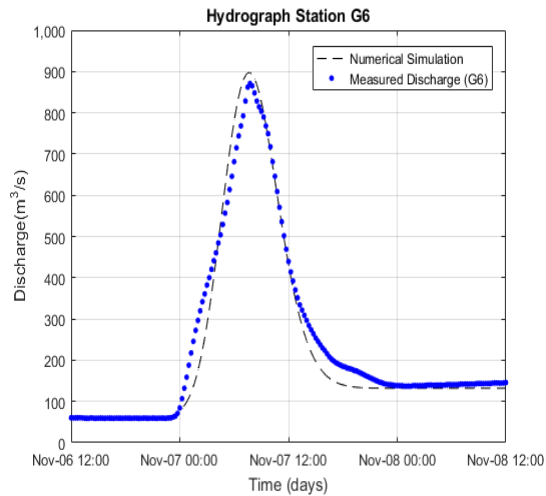


# Hydrographs

Observed hydrographs in Doce River after the Fundão Dam break (ANA, 2015).



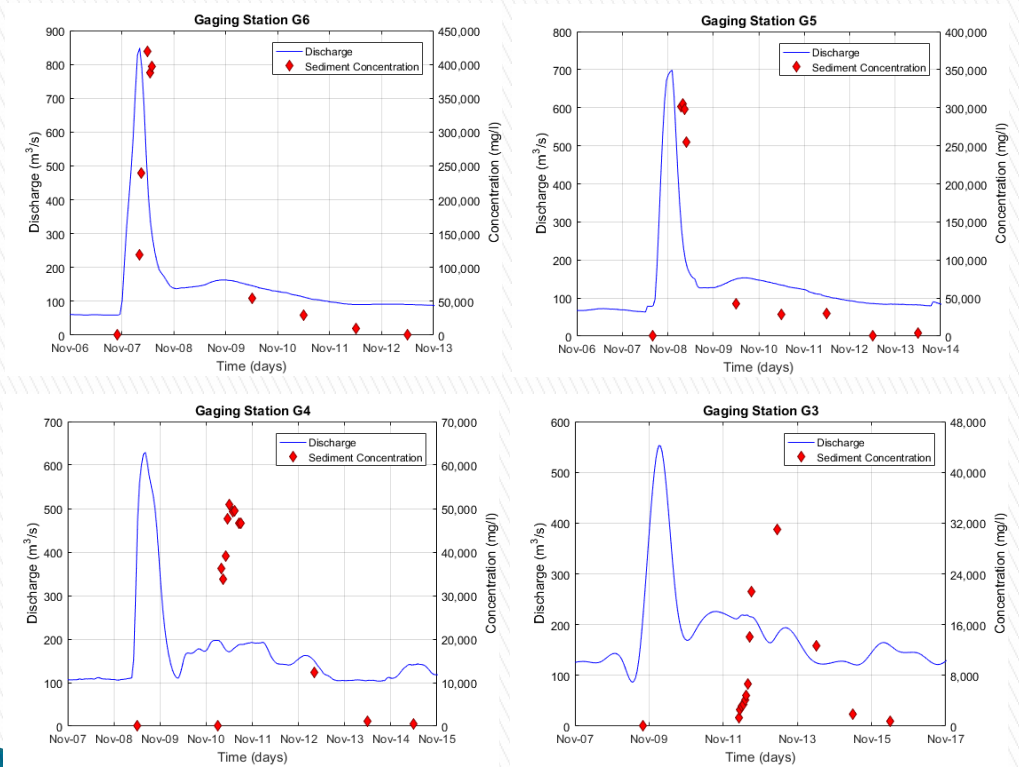
# Floodwave Propagation Modeling



from Marcos Palu and Julien ASCE-JHE (2020)

# Sediment Concentration Measurements

Observed suspended sediment concentration (CPRM & ANA, 2015)



# Sediment Routing NEW Development!

The one-dimensional advection-dispersion equation with settling is applied on the evaluation of transport of suspended load in open channels (Fischer et al., 1979; Julien, 2010).

$$\frac{\partial C}{\partial t} + U \frac{\partial C}{\partial x} = K_d \frac{\partial^2 C}{\partial x^2} - kC$$

$C$  is the concentration;  
 $U$  is the flow averaged velocity;  
 $K_d$  is the longitudinal dispersion coefficient;  
 $k = \omega/h$  is the settling rate.

Analytical solution for a constant spill of finite duration  $\tau$  is:

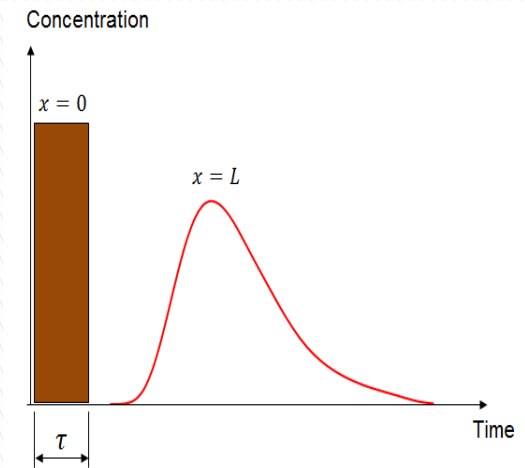
$$C(x, t) = \frac{C_0}{2} \left\{ \begin{aligned} & e^{\frac{Ux}{2K_d}(1-\Gamma)} \left[ \operatorname{erfc} \left( \frac{x - Ut\Gamma}{2\sqrt{K_d t}} \right) - \operatorname{erfc} \left( \frac{x - U(t - \tau)\Gamma}{2\sqrt{K_d(t - \tau)}} \right) \right] \\ & + e^{\frac{Ux}{2K_d}(1+\Gamma)} \left[ \operatorname{erfc} \left( \frac{x + Ut\Gamma}{2\sqrt{K_d t}} \right) - \operatorname{erfc} \left( \frac{x + U(t - \tau)\Gamma}{2\sqrt{K_d(t - \tau)}} \right) \right] \end{aligned} \right\}$$

Where:  $\Gamma = \sqrt{1 + 4\eta}$  and  $\eta = \frac{kK_d}{U^2}$

The complementary error function  $\operatorname{erfc}$  is equal to:

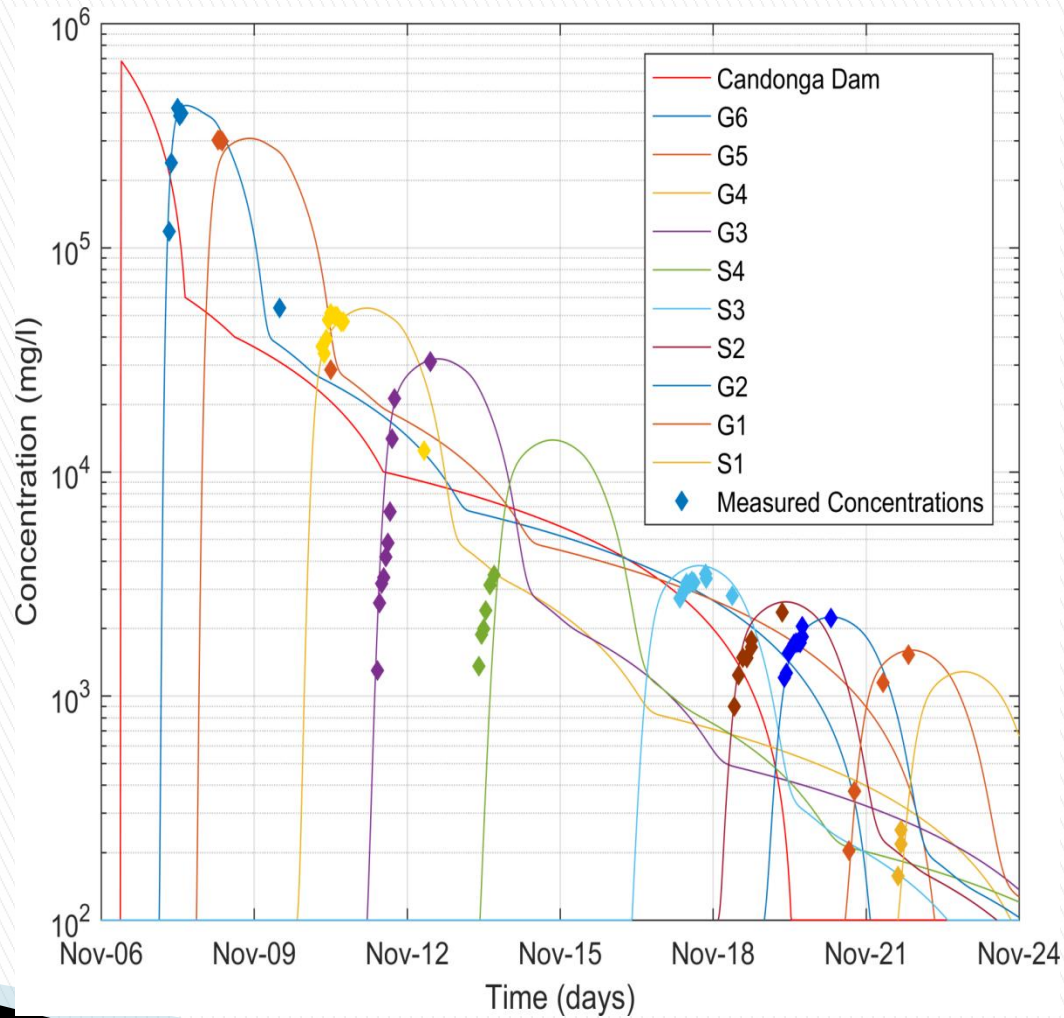
$$\operatorname{erfc}(b) = 1 - \operatorname{erf}(b) = 1 - \frac{2}{\sqrt{\pi}} \int_0^b e^{-\beta^2} d\beta$$

`erfc.precise` in Xcel





# Sediment Concentration Modeling



# Summary and Conclusions

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## 1. River Equilibrium

*Rivers can reach equilibrium after several years.*

## 2. Aggradation

*Aggradation forces out-of-banks rivers and braiding.*

## 3. Degradation below Dams

*Degradation causes incision and narrowing with possible impact on structures.*

## 4. Case-study Gupo Bridge

*Retrofitting based on stability, not equilibrium.*

## 5. Case-study Dam Break

*Numerical modeling of flood and sediment waves.*





# Thank You!

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## ACKNOWLEDGMENTS

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Dr. Jenifer Duan, UArizona  
Dr. Phil Combs, USACE  
Dr. Kiyong Park, K-Water S. Korea  
Dr. Claudia Leon, USBR  
Dr. Azazi Zakaria, USM, Malaysia  
Dr. Amin Ab. Ghani, USM, Malaysia  
Dr. Ev. Richardson, CSU  
Dr. Gigi Richard, FLC, Colorado  
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Dr. Sang-kil Park, PNU, S. Korea  
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# River Mechanics

Second Edition